

Hydrogeological Assessment

FINAL REPORT

Auburn Developments

Project Name:

Hunter Farm Development Marion Street Dorchester, Ontario

Project Number:

LON-21008138-A0

Prepared By:

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Date Submitted:

June 14, 2022

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Date Submitted:

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Executive Summary

EXP Services Inc. (EXP) was retained by **Auburn Developments** to conduct a hydrogeological assessment of the proposed development to be located south of Marion Street and to the east and west of Richmond Street in Dorchester, Ontario, hereinafter referred to as the 'Site'.

The objective of the hydrogeological assessment was to examine the hydrogeological characteristics of the Site by reviewing the Ministry of the Environment, Conservation and Parks (MECP) Water Well Records (WWR), reviewing the soils and groundwater information provided from a series of sampled boreholes and monitoring wells at the Site, compiling a site wide monthly water balance, collecting a full year of groundwater elevations to identify any seasonal variations, and assess the natural heritage features on the property. It is understood that the hydrogeological assessment will be submitted for review and approval by the County of Middlesex (Thames Centre) and the Upper Thames River Conservation Authority (UTRCA).

Based on the results of the hydrogeological assessment, the following findings are presented:

- There are several mapped surface water features across the Site including the Sandusky Drain, the Porter Subdivision Drain and the Hunter Branch which all drain to the south into the Hunt Drain. In addition, three
 (3) unmapped wetlands are located on the Site which are all considered regulated lands of the UTRCA (Wetland A to the west of the Sandusky Drain and Wetlands B and C in the northeast portion of the Site);
- Surface drainage follows Site topography and generally flows towards the Drains to the southwest and eventually south to Thames River;
- The stratigraphy at the Site is heterogenous with silt, sandy silt/silty sand clayey silt/till at surface overlying sand/ sand and gravel which is discontinuous in nature. The sand is present mostly in the western portion of the Site and becomes exposed at surface in the southwest corner of the Site. Based on borehole logs, the sand layer is up to 4.5 m thick. Surficial organic deposits were noted in the vicinity of Wetland A west of the Sandusky Drain;
- Overall, groundwater levels across the Site are relatively high and near ground surface with groundwater levels measured within 1 meter below ground surface (bgs). Groundwater elevations in the majority of the wells were elevated in the spring and showed a direct response to precipitation events;
- Portions of the Site are mapped as a significant groundwater recharge area and a highly vulnerable aquifer;
- Single Well Response Tests (SWRT) were completed on four (4) of the monitoring wells. Based on the test results, the estimated hydraulic conductivities are 8.2×10^{-4} m/s for sand and between 3.2×10^{-8} m/s and 9.0×10^{-7} m/s for silt;
- Three (3) grain size analyses were carried out on samples of the sand and gravel till, silt till and sand. The hydraulic conductivity ranged from 3.1 x 10⁻⁷ m/s in silty sand till, to 4.5 x 10⁻⁵ m/s in sand (BH9);
- Groundwater chemistry results did not exceed the Ontario Drinking Water Quality Standards, Objectives and Guidelines (ODWQS) for any of the analyzed parameters with the exception of uranium which exceeded the



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ODWQS of 20 ug/L with a concentration of 35 ug/L at BH7/MW-A on March 17, 2022. The Ontario Provincial Water Quality Objectives (PWQO) guidelines were exceeded for several analyzed parameters in surface water;

- The monitoring wells on Site have been maintained for ongoing study past the completion of this report. When the wells are no longer required, they should be decommissioned in accordance with O. Reg. 903;
- The post development infiltration target of 80%, as suggested by the Conservation Ontario Guidelines, can be achieved by redirecting runoff for infiltration using secondary infiltration and run-off reduction techniques;
- Preliminary dewatering calculations suggest a Category 3 Permit to Take Water will be required for construction dewatering, specifically in the southwest portion of the Site, where a shallow saturated sandy aquifer was observed;
- During construction, short term impacts to the shallow groundwater may occur, where excavations crossing the shallow groundwater require construction dewatering; and,
- A total of 45 domestic, one (1) livestock, and one (1) public groundwater supply wells are located within a 500 m radius of the Site. Four of the domestic wells and the public well were installed into the shallow overburden (<10 m bgs). Based on the results from the door-to-door survey, it has been confirmed that a number of residences within 500 m of the Site utilize private well water.

A full year of groundwater elevation monitoring (May 2021 to May 2022) and water quality monitoring was completed in support of the hydrogeological investigation. Based on the hydrogeological data collected from the property, a good understanding has been captured regarding the groundwater conditions related to site development. It is our hope that this Final Report will be sufficient for Site Plan Submission.



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1. Introduction and Background

1.1 Background

EXP Services Inc. (EXP) was retained by Auburn Developments to conduct a hydrogeological study and water balance assessment on the proposed development to be located south of Marion Street and east and west of Richmond Street, in Dorchester, Ontario, hereinafter referred to as the 'Site' (Appendix A, Drawing 1).

The proposed development consists of low and medium density residential homes with open space and park areas, as well as stormwater management (SWM) facilities. The preliminary conceptual development plan is included in **Appendix B**.

The objective of the hydrogeological study was to examine the hydrogeological characteristics of the Site by reviewing the Ministry of the Environment, Conservation and Parks (MECP) Water Well Records (WWR), reviewing the soil and groundwater information provided from a series of sampled boreholes and monitoring wells at the Site, compiling a Site wide monthly water balance, collecting a full year of groundwater elevations to identify any seasonal variations; and assess the natural heritage features on the property. The assessment provides comments pertaining to potential impacts on hydrogeological conditions at the Site and provides recommendations and design/construction measures, where applicable, to mitigate this potential for impact. This final report includes a full year of data collection thus fulfilling the requirements in support of the Site Plan Submission.

It is understood that the hydrogeological study and water balance assessment will be submitted for review and approval by the County of Middlesex (Thames Centre) and the Upper Thames River Conservation Authority (UTRCA) as part of the Draft Plan Approval for the proposed development. The study design and report have been compiled in accordance with the City of London Design Specification & Requirements Manual (2019) as well as the Conservation Authority Guidelines for Hydrogeological Assessments (2013).

The Site is located north of the Thames River and contains multiple mapped Drains (Sandusky Drain, the Porter Subdivision Drain, and the Hunter Branch which all drain to the south into the Hunt Drain) as well as unmapped wetlands. EXP staff confirmed the Porter Subdivision Drain does not exist on Site. Wetland A is defined as the wetland west of the Sandusky Drain, Wetland B is defined as the small wetland in the northeast portion of the Site, and Wetland C is defined as the larger wetland in the northeast portion of the Site (**Drawing 2**). These surface water features have been assessed based on their impact to, and dependence on, groundwater resources.

The UTRCA administers a regulation made under Section 28 of the Conservation Authorities Act, known as Development, Interference with Wetlands and Alterations to Shorelines and Watercourses (O.Reg. 157/06). The regulation was approved by the Minister of Natural Resources and Forestry on May 4, 2006. This regulation allows the UTRCA to ensure that proposed development and other activities have regard for natural hazard features. The UTRCA implements the regulation by issuing Section 28 permits for works in or near watercourses, valleys, wetlands, or shorelines, when required.

Property owners must obtain permission and/or a letter of clearance from the local Conservation Authority before beginning any development, site alteration, construction, or placement of fill within the regulated area. Permits are also required for any wetland interference, or for altering, straightening, diverting or interfering in any way with the existing channel of a creek, stream or river. It is EXP's understanding that the Site is subject to this regulation, and requires a Section 28 permit, as the Site contains a water feature.



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1.2 Terms of Reference and Scope of Work

The investigation was completed in accordance with the scope of work outlined through email correspondence provided in **Appendix C**. An official scoping meeting with the UTRCA was not completed, however, the study followed standard UTRCA study guidelines as completed for similar projects. An Authorization to proceed with this investigation was received from Mr. Steve Stapleton of **Auburn Developments Inc.** through email correspondence in May 2021.

A geotechnical investigation is also being conducted by EXP for the Site and will be submitted under separate cover. This investigation included excavation of 38 test pits across the Site. Test pit logs from the geotechnical investigation are included in **Appendix D**. Information from the geotechnical study will be incorporated into this report, wherever appropriate.

The purpose of the assessment was to examine the subsoil and groundwater conditions at the Site by advancing a series of boreholes at the locations chosen by EXP and illustrated on the Field Investigation Location Plan (**Drawing 2**).

The scope of work for the Hydrogeological Assessment consisted of the following tasks:

- 1. <u>Desktop Study</u>: This task consisted of a review of existing information including Site plans, previous reports, geological maps, geological cross sections, groundwater level information, borehole logs, and MECP WWR.
 - EXP has completed several Geotechnical Investigations and Hydrogeological Assessments in the vicinity of the Site and relevant details from those studies have been incorporated, where appropriate.
- 2. <u>Field Program</u>: Installation of ten (10) monitoring wells in nine (9) locations was carried out as part of the field program with one of the locations being completed with a set of nested wells (BH7/MW A/B). A total of five (5) surface water stations were installed within surface water bodies found across the Site. Water levels have been measured monthly since installation for a twelve (12) month period to identify seasonal fluctuations in the groundwater and surface water features on Site. Single well response tests (SWRT) were completed for the purposes of characterizing the hydrogeological conditions at the Site. Two (2) rounds of groundwater and surface water quality samples were collected and submitted for laboratory analysis. In addition, a door-to-door well survey was completed to confirm whether shallow wells are in use in the vicinity of the Site.
- 3. <u>Data Evaluation</u>: Evaluation of the available field and laboratory data, assessment of the dewatering requirements and potential dewatering effects on the surrounding environment, as applicable.
- 4. <u>Water Balance</u>: Preparation of a water balance assessment of the subject Site evaluating pre- and post-development conditions.
- 5. Reporting: This task consisted of preparing this hydrogeological assessment report. In preparing this report, EXP has considered the guidance material available in the Conservation Ontario Guidelines for Hydrogeological Assessments (Conservation Ontario, 2013) and City of London Design Specification & Requirements Manual (2019).



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Reference is made to **Appendix N** of this report, which contains further information necessary for the proper interpretation and use of this report.

1.3 Proposed Development and Stormwater Management Strategies

The proposed development will contain mixed single family and medium density residential properties with local servicing installed to standard depths of approximately 2 to 4 m below grade. The Draft Plan of Subdivision is provided in **Appendix B**. The residential development will also include park and open space areas, two (2) stormwater management (SWM) facilities, as well as interior roadways and sidewalks.

A Stormwater Management Report was completed by Stantec Consulting Ltd. (Stantec) on May 16, 2022 (Stantec, 2022). A map of the proposed storm drainage areas is provided in **Appendix B**. West of Richmond Street, runoff will be directed to the Sandusky Drain with no quantity controls proposed. Additionally, runoff conveyance from external areas (EXT-1 and EXT-2) to the Sandusky Drain will be maintained. East of Richmond Street two (2) SWM facilities are proposed located in block A209 in the north portion of the Site (dry pond) and in block A208b in the southern portion of the Site (wet pond). Runoff east of Richmond Street will be directed partly to the Sandusky Drain, the SWM facilities which ultimately drain west into the Sandusky Drain, Wetland C and to Ida Street southeast of the Site to mitigate peak flows to the Sandusky Drain. Implementation of Low Impact Development (LID) techniques will be considered in the final design stage.



2. Methodology

2.1 Borehole Drilling and Monitoring Well Installations

On May 11 and 12, 2021, ten (10) boreholes were advanced at nine (9) locations at the Site with installation of monitoring wells in all ten (10) boreholes. One (1) location was completed as 'nested' wells to allow for a hydrogeological gradient evaluation (BH7/MW – A/B). The locations of the boreholes are all presented on **Drawing 2**. Borehole drilling and monitoring well installation was completed under the technical supervision of EXP. The location and depth of the boreholes was based on the proposed development plan which was provided to EXP. Boreholes were advanced to depths ranging from 5.0 to 11.1 m below ground surface (bgs).

The boreholes were advanced using a track-mounted drill rig and standard 21 cm (8") OD hollow stem auger drilling techniques with split spoon sampling. During the drilling, the stratigraphy in the boreholes was examined and logged in the field by EXP technical personnel. Representative samples of the soils found in the boreholes were submitted for laboratory testing that included moisture content and gradation. Copies of the field borehole logs are provided in **Appendix D**. Copies of the soil gradation analyses are included in **Appendix E**.

All wells were constructed from 5.1 cm (2") diameter, schedule 40, polyvinyl chloride (PVC), flush-threaded casing. The appropriate number of risers were coupled with screen sections via threaded joints to construct the well. The well screens consisted of PVC pipe with 0.010-inch factory-generated slots. A summary of the well installation details is provided in **Table 1**, with the well locations shown on **Drawing 2**.

A primary filter pack consisting of silica sand was placed around the well screen in the borehole and extended above the top of the well screen. Hole Plug, a swelling bentonite clay that forms an effective barrier to the vertical movement of fluids when installed in a borehole, was used as a seal above the filter pack.

The ground surface and top of well pipe elevations were collected by a Sokkia GPS unit, capable of collecting accurate location and elevation measurements to the mm scale.



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Table 1 – Monitoring Well Construction Details

| Well ID | Ground Surface Elevation* (m amsl) | Top of Standpipe Elevation* (m amsl) | Completion Depth (m bgs) | Screen Length (m) | Screened Strata |
|----------|--|--|--------------------------------|-------------------------|---|
| BH1/MW | 260.80 | 261.60 | 9.1 | 1.52 | Sand and Gravel; Sand |
| BH2/MW | 256.00 | 256.90 | 4.6 | 1.52 | Silt |
| BH3/MW | 256.04 | 256.89 | 5.3 | 1.52 | Sand; Sandy Silt |
| BH4/MW | 256.03 | 256.85 | 4.6 | 1.52 | Sand |
| BH5/MW | 257.64 | 258.57 | 3.8 | 1.52 | Sandy Silt; Sand; Silt Lamination; Silt Till |
| BH6/MW | 268.06 | 268.90 | 10.7 | 1.52 | Sand; Clayey Silt |
| BH7/MW-A | 264.30 | 265.08 | 6.1 | 1.52 | Silt; Silt Till |
| BH7/MW-B | 264.28 | 265.11 | 3.0 | 1.52 | Silt; Clayey Silt |
| BH8/MW | 257.53 | 258.43 | 3.8 | 1.52 | Sand; Sandy Silt Till |
| BH9/MW | 266.14 | 266.96 | 4.6 | 1.52 | Sand |

Notes:

- 1. m amsl denotes metres above mean sea level.
- 2. m bgs denotes metres below ground surface.
- * elevations were collected by a Sokkia GPS unit

2.2 Piezometer and Staff Gauge Installations

A total of five (5) surface water stations were installed throughout the Site on May 27, 2021, in a combination of surface Drains and wetland features. Each surface water station was installed with a shallow groundwater piezometer and surface water staff gauge. Surface water Station 1 was installed in Wetland A west of the Sandusky Drain and Richmond Street. Surface water Station 2 was installed downstream at the south end of the Sandusky Drain and surface water Station 3 was installed upstream within the northern end of the Sandusky Drain. Surface water stations 4 and 5 were installed within the two (2) wetlands located in the northeast corner of the Site in Wetland B and Wetland C, respectively. The locations of each station are shown on **Drawing 2**. The following **Table 2** outlines the surface water station details.

The piezometers were installed with a 6-inch Solinst drive point end (6-inch screen length). The Solinst drive point piezometer ends have a stainless steel, 50 mesh cylindrical filter screen, within a ¾" (20mm) stainless steel drive-point body.

A staff gauge was installed at each surface water station within the surface water body in order to capture monthly surface water elevations. This staff gauges are referred to as SG1 to SG5.

Each piezometer and staff gauge was surveyed using a Sokkia GPS unit, capable of collecting accurate location and elevation measurements to the mm scale.



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Table 2 - Surface Water Station Details

| Station ID | Piezometer ID | Ground Surface Elevation (m amsl) | Top of Piezometer Elevation (m amsl) | Completion Depth (m bgs) | Screen Length (m) | Screened Strata | Staff Gauge Installed |
|------------|------------------|--|---|--------------------------------|-------------------------|---|--------------------------|
| Station 1 | P-1 | 255.52 | 256.56 | 1.02 | 0.15 | Soft Soil (likely organic) | Yes (SG1) |
| Station 2 | P-2 | 254.58 | 255.88 | 0.7 | 0.15 | Soft Soil (likely organic); Sand and Gravel | Yes (SG2) |
| Station 3 | P-3 | 256.21 | 257.55 | 1.08 | 0.15 | Sand and Gravel | Yes (SG3) |
| Station 4 | P-4 | 263.57* | 264.67 | 1.03 | 0.15 | Silt/Clay | Yes (SG4) |
| Station 5 | P-5 | 264.43 | 265.68 | 1.03 | 0.15 | Soft Soil (likely organic) | Yes (SG5) |

- Notes: 1. m amsl denotes metres above mean sea level.
 - 2. m bgs denotes metres below ground surface.
 - 3. * assumed elevation based on SG elevation

2.3 Well Development and Groundwater Sampling

Monitoring wells were developed following installation. The wells were developed to:

- remove fine soil particles adjacent to the well screen that may otherwise interfere with water quality analyses;
- restore the groundwater properties that may have been disturbed during the drilling process;
- improve the hydraulic communication between the well and the geologic materials; and,
- remove water, if any, added during the drilling process.

Wells were generally developed by removing a minimum of ten times the volume of water contained in the well casing (casing volume) where possible using rigid high-density polyethylene (HDPE) tubing fitted with Waterra™ inertial pumps.

Groundwater samples were collected from four (4) selected monitoring wells on September 28, 2021 and March 17, 2022 for analysis of groundwater quality. Groundwater chemistry results are presented and discussed in **Section 4.4**.

2.4 Surface Water Sampling

Surface water samples were collected from four (4) selected surface water stations on September 28, 2021 and March 17, 2022 in order to establish baseline surface water quality. Surface water chemistry results are presented and discussed in Section 4.4.



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2.5 Long-Term Groundwater Elevation Monitoring

Water level monitoring in all monitoring wells and piezometers installed on Site has been completed on a monthly basis (with the exception of the month of June) since installation in May 2021 until the end of April 2022 for a one-year period. Measurements were manually collected using a battery-signal water level tape.

Water level dataloggers were installed in four (4) monitoring wells (BH3/MW, BH7/MW-A, BH7/MW-B, BH9/MW) and within the shallow groundwater piezometers at surface water stations SW1, SW2, SW4 and SW5 to assist in the evaluation of seasonal water level fluctuation, groundwater/surface water interactions, and the influence of precipitation on surface water and groundwater levels across the Site. An additional logger was placed at surface and used for barometric compensation. The dataloggers were installed in the monitoring wells on May 18, 2021 and in the piezometers on May 27, 2021 and remained in place for continued monitoring until the monitoring period was completed at the end of April, 2022. Water level measurements were logged every 24 hours.

2.6 Hydraulic Conductivity Testing

Hydraulic conductivity estimates for the soils were determined using two methods. The first method is applicable to saturated soils at depth and involves single well recovery tests (SWRT) within the installed monitoring wells. The second method involves a calculated estimation of hydraulic conductivity based on soil sample particle size analysis.

2.6.1 Single Well Response Tests (SWRTs)

Single Well Response Tests (SWRTs) were completed in monitoring wells BH2/MW, BH4/MW, BH7/MW-A and BH8/MW on May 17, 2021 to estimate hydraulic conductivity of the subsurface soils. The test method consisted of an initial purging of the well and subsequent monitoring of the rise in the water level in the well over time. This method is applicable to saturated soils at depth.

The results from the SWRTs were analyzed using the mathematical solution by Hvorslev (1951) for unconfined aquifer as provided in the software AQTESOLV TM Pro v. 4.5 and involved matching a straight-line solution to water-level displacement data collected during the recovery test. The following equation was used to estimate the hydraulic conductivity (K);

 $K (m/s) = [r^2 ln(L/R)] / [2 L T_o]$

where: (T_o) is the initial change

r is the radius of the well casing; R is the radius of the well screen; and, L is the length of the well screen.

2.6.2 Grain Size Analyses

A total of three (3) soil samples were selected for grain size distribution analysis testing. Due to the nature of the Site soils, estimated hydraulic conductivity (K) values were determined using different methods depending on the soil sample characteristics including the Kaubisch, Kozeny-Carman, and Beyer methodologies.



3. Site Description and Geologic Setting

3.1 Site Location and Description

The Site is located south of Marion Street, and to the east and west of Richmond Street in Dorchester, Ontario. The Site is currently occupied by agricultural fields and farming structures to the east side of Richmond Street. The Site is irregular in shape and measures approximately 45.31 hectares in total area. The site is bounded by Canadian National Railway tracks to the south, undeveloped land/residential development to the east, and residential development to the north and west (**Drawing 1**).

The proposed development consists of low and medium-density residential homes with open space and park areas, as well as two (2) stormwater management (SWM) facilities. The conceptual development plan is included in **Appendix B**.

3.2 Topography and Drainage

Based on topographic mapping, the area is generally hilly with a topographic high of approximately 275 m above mean sea level (amsl) located at the northeast corner of the Site and a topographic low of 256 m amsl located in the western portion of the Site associated with a surface water feature.

There are several surface water features across the Site which flow south towards the Thames River. These features include the Sandusky Drain, the Porter Subdivision Drain and the Hunter Branch which all drain south into the Hunt Drain. EXP staff noted that the mapped Porter Subdivision Drain does not exist on Site. According to MTE Consultants Inc. who completed the ecology study for the Site, the unnamed drain south of TP15 and TP16 does not exist as well. Additionally, there are unmapped wetlands including wetland A west of the Sandusky Drain and Wetland B and Wetland C in the northeast portion of the Site. Maps of the surface water features and drainage on Site are provided in **Drawing 2** and **Drawing 3**.

The Site is located in the Dorchester watershed. The areas surrounding the drains and Wetlands B and C in the northeast portion of the Site are regulated by the UTRCA, as shown on **Drawing 4**. Surface runoff from the Site generally flows toward the drains to the southwest and eventually south to Thames River. A detailed description of the drainage areas on Site is provided in Section 5.2.

3.3 Wetlands and Ecology

A detailed ecology study for the Site was completed by MTE Consultants Inc. A map of the ecological land classification and vegetation communities is provided in **Appendix B**. Below is a brief description of the vegetation communities on Site:

- Community 1 is a Mineral Cultural Meadow (CUM1) consisting of Sugar Maple, Manitoba Maple with some Black Locust and Eastern Cottonwood. The regionally-rare species Cockspur Hawthorn was also observed in Community 1.
- Community 2 (Wetland C) is an Organic Shallow Marsh (MAS3) consisting of Tamarack with Goldenrod and Dogwood, Sedge, Cattail, Reed Canary Grass, Skunk Cabbage (a medium sensitivity groundwater indicator plant) and Common Boneset (a low sensitivity groundwater indicator plant).



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- Community 3 (Wetland C) is a White Cedar Organic Coniferous Swamp (SWC3) consisting of Eastern White
 Cedar. Groundwater indicators observed in Community 3 include Jack-in-the-Pulpit (medium sensitivity),
 Spotted Joe-Pye weed (low sensitivity), Skunk Cabbage (medium sensitivity), Great Blue Lobeila (medium
 sensitivity), Naked Mitrewort (medium sensitivity) and Sensitive Fern (medium sensitivity). Regionally-rare
 species observed in Community 3 include Evergreen Wood Fern, Downy Willowherb, Bristly Dewberry and
 Purple Meadow-rue.
- Community 4 is a Mineral Cultural Woodland (CUW1) consisting of Apple and Manitoba Maple with some occasional Ash and Skunk Cabbage (a medium sensitivity groundwater indicator).
- Community 5 (Wetland B) is a Shallow Marsh (MAS) consisting of Willow, Eastern Cottonwood, White Elm Bitter Nightshade, Willow and Manitoba Maple.
- Community 6 is a combination of a Mineral Meadow Marsh (MAM2) and a Mineral Cultural Meadow (CUM1). Groundwater indicators observed in Community 6 include Spotted Joe-Pye weed (low sensitivity), Skunk Cabbage (medium sensitivity), Common Boneset (low sensitivity) and Great Blue Lobeila (medium sensitivity). Regionally-rare species observed in Community 6 include Downy Willowherb and Purple Meadow-rue.
- Community 7 is a Mineral Cultural Meadow (CUM1) consisting of Eastern Cottonwood, Ash, Manitoba Maple,
 Freeman Maple, Willow, Norway Maple, Eastern Redcedar, Spirea and Dogwood. Skunk Cabbage and
 Turtlehead medium sensitivity groundwater indicator plants were also observed in Community 7.
- Community 8 (Wetland A) is a Mineral Meadow Marsh (MAM2) consisting of groundwater indicators including Tussock Sedge (medium sensitivity), Spotted Joe-Pye weed (low sensitivity), Skunk Cabbage (medium sensitivity), Common Boneset (low Sensitivity), Great Blue Lobeila (medium sensitivity) and Sensitive Fern (medium sensitivity). Regionally-rare species in Community 8 include Water Sedge, Downy Willowherb and Purple Meadow-rue.
- Community 9 is a Mineral Cultural Meadow (CUM1) consisting of Manitoba Maple, Willow and Trembling
 Aspen with occasional European White Poplar. Spotted Joe-Pye weed a low sensitivity groundwater indicator
 plant and Great Blue Lobeila a medium sensitivity groundwater indicator plant were also observed in
 Community 9. Regionally-rare species observed in Community 6 include Downy Willowherb and Purple
 Meadow-rue.
- Community 10 is a Residential Farmyard. Northern Catalpa, Hackberry, Silver, Freeman and Manitoba Maple, Ailanthus, Willow and Norway Spruce are found within this Community.

Wetland B (Community 5) is proposed to be removed and may be either compensated on-site, adjacent to Wetland C (community 2), or may be compensated off-site. Wetland A (Community 8) will be predominantly retained as Park space. Buffer areas to be implemented around Wetlands A and C are still in discussion and will be finalized in the final design stage.



3.4 Site Geology

3.4.1 Bedrock Geology

The Site is underlain by limestone, dolostone and shale of the Dundee Formation (OGS, 2011). This formation consists of 60 to 160 feet (18 to 49 m) of light brown, medium-grained with some minor chert (Hewitt, 1972), and is part of the Algonquin Arch, which forms a ridge along the southwestern Ontario peninsula between the Michigan Basin (to the northwest) and the Appalachian Basin (to the southwest). Bedrock is generally not exposed in the area.

Review of bedrock topography mapping (**Drawing 5**; OGS, 1978) indicates the bedrock surface is found at an elevation of approximately 236 m amsl in the vicinity of the Site. The bedrock surface generally slopes to the south in this area. Review of MECP Well records within 1000 m from the centre of the Site (**Appendix F**) indicates an overburden thickness of approximately 11 to 37 m. Bedrock was not encountered during the drilling program completed as part of this investigation.

3.4.2 Overburden Geology

The physiography of Southwestern Ontario was altered significantly by the glacial and interglacial periods that took place throughout the Quaternary period. The overburden deposits which are present in the study area were formed by numerous glacial events during the late Wisconsinan glacial stage approximately 10,000 to 23,000 years before present. There were two distinct glacial lobes present in Southwestern Ontario during this period. The Huron Lobe advanced from Lake Huron southwards, and the Erie Lobe advanced from the northeast, receding to the east.

During the advancement of the glacial ice sheets, bedrock and unconsolidated sediments were eroded. During the recession of the glaciers, the eroded materials were deposited in lakes, rivers and along spillways, contributing to the present configuration of moraines, abandoned spillways, drumlins, eskers, abandoned shorelines, and various still-water sediment deposits.

Deposits in the area can be contributed to the Port Bruce Stadial period. In the London area, a series of east-west recessional and end moraines were formed, along with the Port Stanley Till Plain. Deposition of the basal portion of the Port Stanley Till was formed during the initial advance of the Erie Lobe. Overlying till was deposited during subsequent cycles of advance and retreat, resulting in silt and sand layering within the till plain.

The surficial deposits were mapped and categorized into a number of physiographic regions by Chapman and Putnam (1984). The northern portion of the Site is part of a physiographic region known as the Oxford Till Plain and is also mapped as an undrumlinized till plains landform. The physiographic region in the southern portion of the Site is part of a physiographic region known as Mount Elgin Ridges and is also mapped as a spillway landform. Mapping of the physiographic regions and landforms at the Site is provided in **Drawing 6** and **Drawing 7**, respectively.

Quaternary mapping indicates that the Site consists of the Catfish Creek Till characterized by sandy silt to silt (OGS, 2000).

A review of surficial geological mapping by the Ontario Geological Survey (OGS, 2010) shows the northern portion of the Site is mapped primarily as sandy silt to silty sand textured till on Paleozoic terrain and the southern portion of the Site is primarily mapped as glaciofluvial deposits. Modern alluvial deposits of clay, silt sand and gravel with minor organic remains are mapped west of Richmond Street and are associated with the mapped drains. Minor coarse



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textured glaciolacustrine deposits of sand, gravel, minor silt and clay are mapped along the eastern Site boundary (**Drawing 8**).

3.4.3 Site Specific Surficial Geology

Ten (10) boreholes were completed by EXP in nine (9) locations across the Site, with installation of monitoring wells in all borehole locations. One (1) of the locations was completed as a 'nested' well set to allow for hydrogeological evaluation of potential vertical gradients. The locations of the boreholes are provided in **Drawing 2**. The boreholes were terminated at a maximum depth of between 5.0 and 11.1 m bgs. Borehole logs are provided in **Appendix D**.

Generalized stratigraphic cross sections through the Site, as shown in **Drawing 9**, are provided in **Drawings 10** to **12**. The following is a general description of the stratigraphy at the Site as shown in the cross sections.

As shown in cross section A-A' (**Drawing 10**), the northwest portion of the Site consists of surficial silt and clayey silt/till overlying a discontinuous layer of sand and gravel. The silt layer is also discontinuous and truncates the clayey silt/till layer in the area of BH2/MW. Further to the east, silty sand to sandy silt is found at surface overlying silt and clayey silt/till with a localized sand layer noted in BH9/MW.

As shown in cross section B-B' (**Drawing 11**), the southwest portion of the Site consists of surficial discontinuous sand and sand and gravel overlying silty sand to sandy silt. Further to the east the stratigraphy is more homogenous characterized by predominantly clayey silt/ till with a discontinuous sand lens noted at BH8/MW.

As shown in cross section C-C' (**Drawing 12**), the western portion of the Site consists of surficial silt, silty sand/sandy silt and silt clayey/till overlying sand and sand and gravel. This sand layer becomes exposed at surface at the southwest portion of the Site around BH3/MW. Based on borehole logs, the sand layer is up to 4.5 m thick (BH3/MW). Surficial organic deposits were noted in the vicinity of Wetland A.



4. Hydrogeologic Setting

In addition to the groundwater information collected from the monitoring wells installed at the Site, the following documents were reviewed to gain an understanding of the hydrogeological conditions in the area:

- Goff, K and D.R. Brown, 1981. Ground-Water Resources Summary. Thames River Basin Water Management Study Technical Report. Ontario Ministry of the Environment, Water Resources Report 14;
- Thames-Sydenham and Region Source Protection Committee. 2011. Upper Thames River Source Protection Area, Approved Updated Assessment Report. 12 August; and,
- MECP WWR within 1000 m of the centre of the Site.

4.1 Regional Aquifer

Goff and Brown (1981) described the potential for four regional aquifers in the study area; shallow unconfined overburden aquifer, intermediate and deep confined aquifers and a bedrock aquifer.

4.1.1 Overburden Aquifers

The uppermost shallow and unconfined overburden aquifer was described as consisting of lacustrine or glacio-fluvial sands that may, in some locations, be overlain by lower permeability silts and clays. Regionally, the shallow aquifer is generally associated with the Stratford Till Plain and glacial deposits and are typically less than 15 m in thickness. Shallow overburden aquifers are discontinuous in nature and are expected to be linked more directly to precipitation and recharge compared to the intermediate and deep overburden aquifers.

Intermediate depth (15 to 30 m bgs) and deep overburden aquifers (>30 m bgs) aquifers generally consist of saturated sand and gravel deposits in the overburden and are very discontinuous in nature due to the heterogeneous nature of glacial deposits. Sand and gravel layers are present in the Port Stanley and Catfish Creek glacial till sheets. The intermediate depth and deep overburden aquifers are generally confined by overlying silt, clay and glacial till deposits which limit vertical migration of shallow groundwater.

Locally, shallow groundwater flow is expected to follow the local topography, and generally drain southwest towards the Thames River. Similarly, on a regional scale, the deep overburden aquifer flow direction is reported to be towards the south-southwest (Dillon and Golder, 2004).

4.1.2 Bedrock Aquifer

The bedrock aquifer is contained within limestone of the Dundee Formation. The water quality is generally good with elevated levels of iron, sodium and chloride in some wells. As with the intermediate and deep overburden aquifers, the bedrock aquifer is confined by the overlying till material, which generally ranges in thickness up to 37 m in the vicinity of the Site. Wells extending into the shallow fractured bedrock (up to about 3 m) are typically considered to be hydraulically connected to the overlying sand and gravel deposits that are present at the bedrock-overburden interface.

Flow direction in the deeper confined aquifer(s) and regional groundwater system has not been assessed as part of this investigation. However, as part of the Middlesex-Elgin Groundwater Study (Dillon and Golder, 2004), groundwater flow within the deeper aquifer is generally in a south-southwest direction towards Lake Erie.



4.2 Site Specific Groundwater Elevations and Flow

4.2.1 Monitoring Wells

Manual water levels in the monitoring wells have been collected monthly from May 2021 until the end of April 2022. Details of the monthly water levels are summarized in **Appendix G**.

Overall, shallow groundwater levels of less than 1 m bgs were noted in monitoring wells BH2/MW and BH5/MW. These are shallow wells located along the Sandusky Drain. Shallow groundwater levels were also noted in BH7/MW-A/B located in the vicinity of Wetland B and BH8/MW located at the southern portion of the Site. The deepest groundwater levels were noted in BH1/MW (ranging from 4.21 m to 4.83 m bgs) and in BH6/MW (ranging from 8.68 m to 9.67 m bgs). These are the deepest wells onsite installed to depths of 9.1 m bgs and 10.7 m bgs, respectively.

Dataloggers were installed in monitoring wells BH3/MW, BH7/MW-A, BH7/MW-B, BH9/MW and within the shallow groundwater piezometers at surface water stations SW1, SW2, SW4 and SW5 to provide continuous water elevation monitoring. Dataloggers were installed in the monitoring wells on May 18, 2021, and within the piezometers on May 27, 2021, and have been collecting daily measurement since. Results collected to date are presented in **Appendix G** with precipitation data from weather station London CS (ID 6144478) located approximately 7.7 km northwest of the Site.

The hydrograph for monitoring well BH3/MW, screened in sand/sandy silt from 3.8 m to 5.3 m bgs, shows a gradual decline from May to September 2021 with groundwater elevation increasing as a direct response to significant precipitation events on September 22, 2021 (67 mm) and again on February 17, 2022 (38 mm). Static groundwater levels remained relatively stable between September 2021 and April 2022. Overall, groundwater elevation ranged from 254.21 m to 255.45 m amsl. These groundwater elevations correspond with groundwater levels of 1.83 m and 0.59 m bgs, respectively. Discrepancies between the datalogger and the manual measurements were noted between November 2021 and January 2022 and in April 2022.

Monitoring well BH7/MW-A (deep) is screened in silt/silt till from 4.6 m to 6.1 m bgs and monitoring well BH7/MW-B (shallow) is screened in silt/clayey silt from 1.5 m to 3.0 m bgs. The hydrographs for these nested monitoring wells are nearly identical indicating they are screened within hydraulically connected soils. Groundwater elevations within these wells declined from May to September 2021, increased from September to October 2021 following the September 2021 significant precipitation event and remained relatively stable from October 2021 to April 2022. Overall, groundwater elevations in these wells ranged from 262.74 m to 264.62 m amsl. These groundwater elevations correspond with groundwater levels of 1.54 m bgs and 0.32 m above grade, respectively. Direct responses to precipitation events were noted throughout the monitoring period.

The hydrograph for monitoring well BH9/MW, screened in sand from 3.0 m to 4.5 m bgs, shows a minor decline in groundwater elevations between May and September 2021, followed by an increase in September as a direct response to the September 2021 significant precipitation event. Groundwater elevations remained relatively stable between September 2021 and April 2022. Overall, groundwater elevations ranged from 264.50 m to 265.69 m amsl. These groundwater elevations correspond with groundwater levels of 1.64 m bgs and 0.45 m bgs, respectively. Direct responses to precipitation events were noted throughout the monitoring period.

A decrease in groundwater elevations during the monitoring period from May to September was noted in all the monitoring wells. This observation is consistent with groundwater trends observed in southern Ontario in which higher groundwater levels in early spring correspond with spring freshet. Seasonal fluctuations with elevated



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groundwater elevations as a result of significant rain events were observed in all the monitoring wells. Significant precipitation events during the monitoring period were noted on June 25, 2021 (33 mm), August 26, 2021 (57 mm), September 22, 2021 (67 mm) and February 17, 2021 (38 mm).

4.3 Shallow Groundwater and Surface Water Stations

Surface water (SW) Stations 1 to 5 were established across the Site. Dataloggers were installed in four (4) of the shallow groundwater piezometers (P-1, P-2, P-4 and P-5) in order to capture readings on a daily basis. Results from the dataloggers are presented in hydrographs presented in **Appendix G**.

Surface water Station 1 is located within Wetland A west of the Sandusky Drain. The hydrograph for piezometer P-1 shows a gradual increase in groundwater elevations between May and September 2021. Levels remained relatively stable between September 2021 and April 2022 with fluctuations of approximately 0.25 m. Overall, groundwater elevations in P-1 ranged from 254.73 m to 256.03 m amsl. These groundwater elevations correspond with groundwater levels of 0.79 m bgs and 0.51 m above grade, respectively. The gradual increase in groundwater elevations between installation to roughly September 2021 is likely due to slow recovery following piezometer installation. Above ground water levels in P-1 were observed between October 2021 and April 2022. Surface water readings from the staff gauge, SG1 were generally higher than the piezometer reading indicating downward vertical gradient and recharge conditions. Little to no direct response to precipitation events were observed in piezometer P-1.

Surface water Station 2 is located within the Sandusky Drain west of Richmond Street. The hydrograph for piezometer P-2 shows relatively consistent groundwater elevations throughout the monitoring period with fluctuations of about 0.25 m. Groundwater elevations in P-2 ranged from 254.47 m to 255.49 m amsl. These groundwater elevations correspond with groundwater levels of 0.11 m bgs and 0.91 m above grade, respectively. Above ground water levels and direct responses to precipitation events in P-2 were observed throughout the monitoring period. Surface water readings at the staff gauge, SG2, were found to be generally similar to the shallow groundwater measured within the piezometer, suggesting a close interaction between the surface water and groundwater at this location.

Surface water Station 3 is located within the Sandusky Drain east of Richmond Street. The hydrograph shows consistent water levels in both piezometer P-3 and the staff gauge SG3. Water levels in piezometer P-3 were consistently above grade and higher than the readings at staff gauge SG3. These conditions suggest an upward gradient and groundwater discharge conditions to surface water at this location. Groundwater elevations in P-3 ranged from 256.25 m to 256.71 m amsl corresponding to water levels of 0.04 m to 0.5 m above grade.

Surface water Station 4 is located within Wetland B. Similar to the hydrograph of BH7/MW, groundwater elevations in piezometer P-4 declined from May to September 2021, increased from September to November 2021 following the September 2021 significant precipitation event, and remained relatively stable from November 2021 to March 2022. Groundwater elevations in P-4 fluctuated by approximately 0.25 m and ranged from 262.70 m amsl to 264.16 m amsl. These groundwater elevations correspond with groundwater levels of 0.87 m bgs and 0.60 m above grade, respectively. Dry surface conditions were noted at the staff gauge SG4 between July and October 2021. Between October 2021 and April 2022 water levels at SG4 were consistently above groundwater levels in P-4 indicating downward vertical gradient and recharge conditions at this location.

Surface water Station 5 is located within Wetland C. Similar to piezometer P-1, the hydrograph for piezometer P-5 shows a gradual increase in groundwater elevations between May and June 2021 due to slow recovery following piezometer installation. Water levels in P-5 remained relatively stable between June 2021 and September 2021.



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Following the September 2021 significant precipitation event, water levels in P-5 stabilized with fluctuations of approximately 0.25 m and increases as direct responses to precipitation events. Overall, groundwater elevations in P-5 ranged from 263.91 m to 265.11 m amsl. These groundwater elevations correspond with groundwater levels of 0.52 m bgs and 0.68 m above grade, respectively. Above ground water levels in P-5 were observed throughout the monitoring period. Surface water readings from the staff gauge, SG5 were generally similar to the piezometer levels indicating a close interaction between the surface water and groundwater at this location.

4.4 Hydroperiod and Recharge

Data Reference is made to the TRCA document Stormwater Management Criteria, Appendix D: Water Balance for Protection of Natural Features (August 2012). By definition, the hydroperiod is the seasonal pattern of water level fluctuation. It is the result of inflow and outflow, surface contours of the landscape, substrate and groundwater conditions. Defining the existing surface water and groundwater conditions in the area is essential in order to provide recommendations, mitigation strategies and contingency measures during the development of the property.

The range in water elevations measured across the Site (a measurable component of a hydroperiod) throughout the monitoring period is shown in **Table 3** below.



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Table 3 – Hydroperiod as defined by Groundwater and Surface Water Elevations

| Location ID | Minimum Water Elevation (m amsl) | Maximum Water Elevation (m amsl) | Range (m) |
|-------------|-------------------------------------|-------------------------------------|-----------|
| BH1/MW | 255.97 | 256.59 | 0.62 |
| BH2/MW | 254.99 | 255.46 | 0.47 |
| BH3/MW* | 254.21 | 255.45 | 1.24 |
| BH4/MW | 254.59 | 255.09 | 0.5 |
| BH5/MW | 256.82 | 257.27 | 0.45 |
| BH6/MW | 258.38 | 259.37 | 0.99 |
| BH7/MW-A* | 262.75 | 264.62 | 1.87 |
| BH7/MW-B* | 262.74 | 264.60 | 1.86 |
| BH8/MW | 256.95 | 257.25 | 0.3 |
| BH9/MW* | 264.50 | 265.69 | 1.19 |
| P-1* | 254.73 | 256.03 | 1.3 |
| SG1 | 255.59 | 255.75 | 0.16 |
| P-2* | 254.47 | 255.49 | 1.02 |
| SG2 | 254.71 | 254.94 | 0.23 |
| P-3 | 256.25 | 256.71 | 0.46 |
| SG3 | 256.01 (Dry) | 256.48 | 0.47 |
| P-4** | 262.70 | 264.16 | 1.46 |
| SG4 | 263.57 (Dry) | 264.50 | 0.93 |
| P-5 | 263.91 | 265.11 | 1.2 |
| SG5 | 264.56 | 265.06 | 0.5 |

Note: * - Measurements obtained from datalogger

As shown in **Table 3**, the largest variation in water elevations occurred at BH7/MW-A and BH7/MW-B with a range of 1.87 m and 1.86 m respectively.

Typically, groundwater recharging conditions occur on Site from approximately October to April, as observed in the hydrographs. Based on available logger data the most notable significant recharge surges were in monitoring wells BH7/MW-A/B, located adjacent to Wetland B. There were approximately three significant (3) separate surges of recharge. The maximum magnitude of groundwater increase during these surges was as follows:

June 25 to June 26, 2021, recharge of 0.8 m in a day;



^{** -} Measurements collected from May 2021 to March 2022

- September 22 to September 23, 2021, recharge of 1.12 m in a day;
- February 17 to February 23, 2022, recharge of 0.5 m over 6 days (average of 0.08 m per day);

Therefore, during recharging events, the aquifer is found to recharge on the order of 0.08 m to 1.12 m per day.

Groundwater recharge did not occur from approximately May to September 2021 in monitoring wells BH7/MW-A/B, as the groundwater table was decreasing during this time period.

4.5 Hydraulic Gradients and Flow

The horizontal hydraulic gradient across the Site will vary due to the range in topography and resulting range in groundwater elevations. The hydraulic gradient is found to be approximately 0.01 m/m across the Site.

Groundwater elevations collected in nested monitoring wells BH7/MW-A/B were very similar and a vertical hydraulic gradient could not be determined.

Shallow groundwater flow across the Site is affected by hydraulic conductivity, topography, drainage, and geology. Based on the groundwater elevations across the Site it is determined that shallow groundwater is generally flowing in a southwesterly direction. Groundwater elevations and flow direction are presented in **Drawing 13.** The groundwater flow direction map represents seasonal high groundwater elevations from February, 2022. Groundwater discharging conditions are observed within the Sandusky Drain and are represented in the Groundwater Flow map in **Drawing 13**.

4.6 Hydraulic Conductivity

Single well recovery tests (SWRT) were performed on four (4) selected monitoring wells on Site (BH2/MW, BH4/MW, BH7/MW-A and BH8/MW) to evaluate the hydraulic characteristics of the soil on Site. The results of the tests are summarized in **Table 4**, and the calculations are presented in **Appendix H**. The results provide information regarding the hydraulic conductivity of the soils surrounding the well screen.

Based on these tests, the estimated hydraulic conductivities are 8.2×10^{-4} m/s for sand and between 3.2×10^{-8} m/s and 9.0×10^{-7} m/s for silt. These results agree with literature values of hydraulic conductivities for sand ranging from 10^{-5} to 10^{-2} m/s and silt ranging from 10^{-9} to 10^{-5} m/s (Table 2.2, Freeze and Cherry; 1979).

Grain size analyses were carried out on select soil samples collected from the boreholes, with results summarized in **Table 4**, and shown graphically in **Appendix E**. A total of three (3) soil samples from Site were selected for grain size distribution analysis testing. Based on the grain size analyses, the hydraulic conductivity ranged from 3.1×10^{-7} m/s in silty sand till (BH1) to 4.5×10^{-5} m/s in sand (BH9). A hydraulic conductivity of 1.1×10^{-6} m/s was estimated for the silt till (BH8). The results of all hydraulic conductivity testing are compiled in the table below.



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Table 4 – Hydraulic Conductivity Results

| Sample ID | Lithology | Hydraulic Conductivity (m/s) | |
|---------------------|---------------------------|------------------------------|--|
| BH2/MW | Silt | 7.3 x 10 ⁻⁸ | |
| BH4/MW | Sand | 8.2 x 10 ⁻⁴ | |
| BH7/MW-A | Silt; Silt Till | 9.0 x 10 ⁻⁷ | |
| BH8/MW | Sand; Silt Till | 3.2 x 10 ⁻⁸ | |
| Grain Size Analyses | | | |
| BH1, SA7 | Silty Sand Till, Gravelly | 3.1 x 10 ⁻⁷ | |
| BH8, SA4 | Silt Till, sandy | 1.1 x 10 ⁻⁶ | |
| BH9, SA5 | Sand | 4.5 x 10 ⁻⁵ | |

4.7 Groundwater and Surface Water Quality

Groundwater and surface water sampling was completed on September 28, 2021 and March 17, 2022. A total of four (4) groundwater monitoring wells (BH3/MW, BH7/MW-A and BH7/MW-B and BH9/MW) and four (4) surface water locations (SW Station 1, Station 2, Station 4 and Station 5) were selected for sampling. Water quality tables are presented in **Appendix I** and complete laboratory chain of custody results are provided in **Appendix J**.

Groundwater quality was compared to the Ontario Drinking Water Quality Standards, Objectives and Guidelines (ODWQS) (O.Reg. 169/03). Although the groundwater on Site is not planned for use as drinking water, these guidelines are used for comparison's sake only. As demonstrated in the tabulated results in **Appendix I**, no parameters exceeded the ODWQS guidelines for any sampled monitoring wells with the exception of uranium which exceeded the ODWQS of 20 ug/L with a concentration of 35 ug/L at BH7/MW-A on March 17, 2022.

Surface water quality was compared to Ontario Provincial Water Quality Objectives (PWQO) (MOEE 1994). The PWQO guidelines for several parameters were exceeded in the surface water stations. The following table summarizes the detected exceedances (**Table 5**). Total aluminum exceeded the PWQO guideline of 75 ug/L in all surface water stations. Total arsenic exceeded the PWQO guideline of 5 ug/L in surface water Station 1. The metals cobalt, iron and zinc concentrations exceeded the PWQO guideline in surface water Stations 1 and 5 and the PWQO guideline for copper was exceeded only in surface water Station 5.



Table 5 - Surface Water Quality Exceedances

| Parameter | PWQO Guideline | Station 1 9/28/21 | Station 1 3/17/22 | Station 2 9/28/21 | Station 2 3/17/22 | Station 4 9/28/21 | Station 4 3/17/22 | Station 5 9/28/21 | Station 5 3/17/22 |
|----------------|-------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| Total Aluminum | 75 ug/L | 1300 | 84 | * | 75 | 140 | 100 | 940 | 1100 |
| Total Arsenic | 5 ug/L | 7.3 | * | * | * | * | * | * | * |
| Total Cobalt | 0.9 ug/L | 2.3 | 2.4 | * | * | * | * | * | 1.0 |
| Total Copper | 5.0 ug/L | * | * | * | * | * | * | * | 7.7 |
| Total Iron | 300 ug/L | 39000 | 39000 | * | * | * | * | 1400 | 6200 |
| Total Zinc | 20 ug/L | 26 | 43 | * | * | * | * | * | 80 |

Note: * meets PWQO

All the remaining tested parameters met PWQO guidelines. Complete chain of custody laboratory results are provided in **Appendix J**.

A Piper Diagram was prepared for the groundwater and surface water quality samples and is shown in **Drawing 14**. Both the groundwater and surface water quality results generally plot within the calcium magnesium bicarbonate alkaline zone of the Piper Diagram with a few outliers. SW Station 1 was found to have the highest chloride concentrations, likely due to runoff from Marion Street. SW Station 4 has the highest concentrations of sulfate on September 28, 2021, as a result of its organic wetland composition. BH7/MW-A shows a different chemical signature between the two sampling events with the sample from March, 2022 being an outlier. This sample had a much larger concentration of total dissolved solids (610 mg/L) than the sample collected in September 2021 (230 mg/L) and it is possible that this affected the chemical signature of the March 2022 sample of BH7/MW-A in the piper plot.

Schoeller Diagrams were also prepared for the groundwater and surface water quality samples for major and minor ions (**Drawings 15a to 15d**). Surface water SW Station 1 shows the highest concentrations in NaCl in both sampling events, further suggesting road salt impact from Marion Street. Sulfate concentrations are lower in SW Stations 1, 4 (March, 2022) and 5 compared to all other sampling locations.



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5. Monthly Water Balance Assessment

The monthly water balance assessment for the Site was completed in accordance with the recommendations indicated in the guidance document "Hydrogeological Assessment Submissions: Conservation Authority Guidelines to Support Development Applications" (Conservation Ontario, 2013), and using appropriate site condition values obtained from Table 3.1 of the MOE Stormwater Management Planning and Design Manual (MOE, 2003). The results of the water balance are provided in **Appendix K**.

The water balance accounts for all water in and out-flows in the hydrologic cycle. Precipitation (P) falls as rain and snow. It can then run off towards wetlands, ponds, lakes, and streams (R), infiltrate into the ground (I), or evaporate from surface water and vegetation (ET). When long-term average values of P, R, I, and ET are used, then minimal or no net change to groundwater storage (Δ S) is assumed.

The annual water balance can be stated as follows:

 $P = ET + R + I + \Delta S$

Where:

P = precipitation (mm/year)

ET = evapotranspiration (mm/year)

R = runoff (mm/year)

I = Infiltration (mm/year)

 ΔS = change in groundwater storage (taken as zero) (mm/year)

5.1. Precipitation and Evapotranspiration

The annual total precipitation used for this water balance (1011 mm/yr) is based on data provided by Environment Canada, based on the 30 year average data for climate normals, using the nearest local weather station information (London CS ID 6144478, located approximately 7.7 km northwest of the Site). In this detailed monthly water balance, precipitation as rain and snow are both considered. Snow storage and resulting snow melt in the winter and early spring months is considered as part of the evapotranspiration volumes.

Evapotranspiration combines evaporation and transpiration and refers to the water lost to the atmosphere. The rate of evapotranspiration is a function of the water holding capacity of the soil and varies with soil and vegetation type and amount of impermeable surface cover.

Monthly evapotranspiration volumes were calculated using the monthly water balance graphical interface created by the U.S. Geological Survey (USGS), Open-File report 2007-1088 (McCabe and Markstrom, 2007). This interface uses the principles outlined by Thornthwaite and Mather (1957) and permits the user to easily modify water balance parameters and provide useful estimates of water balance components for a specified location.



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The difference between the annual precipitation and the annual evapotranspiration represents the surplus water which is available for infiltration and surface run-off. Distribution of the surplus water to infiltration is based on an infiltration factor based on site conditions for topography, cover vegetation and soil.

5.2 Infiltration and Runoff

The soil water holding capacities and infiltration rate were determined using values presented in Table 3.1 of the MOE Stormwater Management Planning and Design Manual (MOE, 2003) based on the vegetative cover and the hydrologic soil group. The weighted values based on the Site conditions are presented in the calculation sheets provided in **Appendix K**.

Localized infiltration rates will vary based on factors such as the saturated hydraulic conductivity of surface soils, land slope, rainfall intensity, relative soil moisture at the start of a rainfall event, and type of cover on the ground surface.

Based on soil mapping by the Ministry of Agriculture, Food and Rural Affairs, the surficial soils at the Site are predominantly B-type soils (sandy loam) within the eastern portion of the Site and D-A-type soils (clay-fine sand) in the western portion of the Site associated with the drains. This mapping is consistent with borehole and test pit logs from the Site indicating the soil cover is mainly silty sand, sandy silt to clayey silt in the eastern portion of the Site and sandy/organic in the western portion of the sand.

For the water balance analysis, soil moisture capacity for B-type soil was utilized in the eastern portion of the Site and mainly A-type soil in the western portion of the Site.

5.3 Pre-development and Post-development Calculations

Pre-development and Post-development monthly water balance calculations have been carried out and are based on available design data. This water balance will be provided to the stormwater engineer for consideration as part of the design of the proposed SWM strategy for the Site.

In general, the Site comprises a land area of approximately 45.31 hectares. To complete the Pre-development water balance, the Site was divided into four (4) drainage areas. The drainage areas are presented in **Drawing 16**. Area A (19.04 ha) drains directly into the Sandusky Drain. Based on the current development plan dated May 12, 2022 (**Appendix B**), it is understood that the Sandusky Drain and Wetlands A and C will be preserved in the post-development environment. Area B (7.17 ha) drains into Wetland C in the northeast portion of the Site, Area C (2.14 ha) drains to the southeast, and Area D (16.96 ha) drains south to southwest and ultimately reaches the Sandusky Drain through a culvert. It should be noted that Areas A and D both end in the Sandusky Drain and under post-development conditions, these areas are essentially combined as being drainage areas to the Sandusky Drain.

Existing conditions across the Site result in varying water holding capacities and infiltration factors. Each drainage area was individually estimated for the present coverage of vegetation under Pre-development conditions. Calculation worksheets are provided in **Appendix K**.

Water balance calculations were completed in accordance with the conceptual SWM strategy for the Site (Stantec, 2022). A map of the proposed drainage areas is provided in **Appendix B**. Detailed assumptions for the post-development water balance are included in **Appendix K**.



Table 6 provides a summary of the pre and post development water balance calculations.

Table 6: Summary of Water Balance Estimates

| | Pre- Development | Post- Development | % Difference (No Mitigation) | Post - Development with Mitigation | % Difference with Mitigation | |
|----------------------------------|-----------------------|----------------------|---------------------------------|---|---------------------------------|--|
| | Drainage to | the Sandusky Drai | n | | | |
| Estimated Runoff (m³/year) | 111,228 | 226,546 | 204% | 135,928 | 122% | |
| Estimated Infiltration (m³/year) | 69,161 | 36,354 | 53% | 55,384 | 80% | |
| | Drainage to Wetland C | | | | | |
| Estimated Runoff (m³/year) | 20,779 | 25,264 | 122% | 10,106 | 49% | |
| Estimated Infiltration (m³/year) | 14,554 | 8,223 | 57% | 11,710 | 80% | |
| | Drainage to the | southeast (Ida Str | eet)* | | | |
| Estimated Runoff (m³/year) | 6,506 | 3,212 | 49% | 128 | 2% | |
| Estimated Infiltration (m³/year) | 4,022 | 448 | 11% | 3,224 | 80% | |

^{*}Runoff and infiltration to the southeast (Ida Street) are significantly different due to a substantially smaller drainage area in the post development.

Due to the increased impermeable surfaces (such as rooftops, roadways, sidewalks, driveways), the proposed development is expected to result in a reduction in the post-development infiltration volumes, and a corresponding increase in the estimated run-off. Conservation Ontario Guidelines (Conservation Ontario, 2013) suggest a target of 80% of the pre-development infiltration being maintained in the post-development conditions.

Infiltration volumes to the Sandusky Drain is estimated to be 53% in the post-development environment with no mitigation measures implemented. If an estimated 40% of runoff was reduced and utilized for infiltration, the 80% target can be met in the Sandusky Drain catchment in the post-development environment.

Infiltration volumes to Wetland C is estimated to be 57% in the post-development environment with no mitigation measures implemented. If an estimated 60% of runoff was reduced and utilized for infiltration, the 80% target can be met in the Wetland C catchment in the post-development environment. It is recommended that only clean runoff from rooftops or landscaped areas be used as added mitigation to Wetland C.

Drainage to the southeast (proposed Ida Street) varies from 2.14 ha in the pre-development environment, to 0.54 ha in the post-development. Under post-development conditions, the majority of drainage is re-directed towards the Sandusky Drain. Due to this modified drainage path, the post-development infiltration and runoff volumes are low and would need to be mitigated significantly. At this time, the post-development mitigation measures are recommended across the development and these volume deficits in the southeast are likely to considered as mitigated volumes across the Site.



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Due to the infiltration volume deficits observed across the Site in the post-development environment, it is recommended to use secondary infiltration and run-off reduction techniques to improve post development infiltration as described below.

5.4 Secondary Infiltration Opportunities

Low Impact Development (LID) is a stormwater management strategy that seeks to mitigate the impacts of increased runoff and stormwater pollution by managing runoff as close to its source as possible (TRCA, 2010). Effective management of stormwater is critical to the continued health of our streams, rivers, lakes, fisheries and terrestrial habitats. The primary objectives of stormwater management includes maintaining the hydrologic cycle, protecting water quality, and preventing increased erosion and flooding.

The following list provides some mitigation measures which may be taken into consideration, during the detailed design stage of the development. These measures may include secondary infiltration by directing and capturing run-off water from impervious surfaces into landscaped areas where existing infiltration capacity can be utilized. More specifically, considerations may include the following:

- Landscaped areas should be graded to promote infiltration of surface water. Increased topsoil depth
 throughout yard and green space areas to reduce runoff. In general, a run-off reduction up to 30% may be
 possible in areas where increased topsoil thicknesses are utilized depending on final topsoil thickness,
 storm duration and intensity;
- Collection of rooftop run-off into side yard and rear yard swales and/or vegetative filter strips, which can be directed to infiltration trenches to promote infiltration;
- Installation of linear bioswales to collect and promote infiltration;
- Use of permeable pavers where feasible such as driveways and parking lots;
- Use of pervious pipes to promote infiltration of water collected in the storm sewer system;
- Routing pavement runoff to grassed areas;
- Planting of trees and bushes;
- Installing soakaway areas;
- Implementing rainwater harvesting (i.e. to re-use in toilet flushing and irrigation, etc.);
- Installing green roof technologies;
- Using filters/bio-retention (i.e. islands, parking areas, etc.);
- Installing absorbent landscaping; and,
- Installing oil/grit separators.



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It is noted that water quality will need to be accounted for in the design of any mitigation measure, such as permeable pavers and pervious pipes, to account for potential impacts from contaminate sources such as winter maintenance on roads and parking lots.

If LID measures are being considered as part of the post-development design, consideration should be given to conducting field percolation tests, at proposed LID locations.

In terms of maintaining infiltration rates in post-development, the most effective stormwater management practices include installing infiltration trenches, lot grading, roof leader discharge to soakaway pits/pervious areas, using pervious pipes, and installing pervious catch-basins.

It is recommended that some of these practices be utilized in site planning and design in order to mitigate the impact of increased runoff and stormwater pollution. By implementing LID practices during development, infiltration volumes can be effectively stored and returned to the natural environment by various development technologies and methods described above.



6. Sourcewater Protection Considerations

6.1 Significant Groundwater Recharge Areas (SGRA)

Groundwater recharge is largely controlled by soil conditions, and typically occurs in upland areas. The groundwater flow direction has been previously identified as flowing in a southwesterly direction.

As defined in the Clean Water Act (2006), an area is a significant groundwater recharge area if,

- 1. the area annually recharges water to the underlying aquifer at a rate that is greater than the rate of recharge across the whole of the related groundwater recharge area by a factor of 1.15 or more; or
- 2. the area annually recharges a volume of water to the underlying aquifer that is 55% or more of the volume determined by subtracting the annual evapotranspiration for the whole of the related groundwater recharge area from the annual precipitation for the whole of the related groundwater recharge area.

An assessment report for the Upper Thames River Source Protection Area was completed by the Thames-Sydenham and Region Source Protection Committee. As defined by the Clean Water Act (2006) and identified by the Thames-Sydenham and Region Source Protection Committee, the eastern half of the Site is located within a SGRA with vulnerability scores of 4 and 6 (**Drawing 17**).

6.2 Highly Vulnerable Aquifers (HVA)

The susceptibility of an aquifer to contamination is a function of the susceptibility of its recharge area to the infiltration of contaminants. As defined in the *Clean Water Act (2006)*, the vulnerability of groundwater within a source protection area shall be assessed using one or more of the following groundwater vulnerability assessment methods:

- 1. Intrinsic susceptibility index (ISI).
- 2. Aguifer vulnerability index (AVI).
- 3. Surface to aquifer advection time (SAAT).
- Surface to well advection time (SWAT).

In the Thames-Sydenham and Region, HVAs were mapped using the ISI method. The ISI method is an indexing approach using existing provincial Water Well Information System (WWIS) database. The ISI method is described in detail in the MECP's Technical Terms of Reference (2001). However, in short, the ISI method is a scoring system that takes into consideration the unique hydrogeologic conditions at a particular location. The scores are determined using a combination of the saturated thickness of each unit and an index number related to the soil type, and as such, the scores reflect the susceptibility of the aquifer to contamination.

As defined in the MECP's 2001 Technical Rules,

an area having an ISI score of less than 30 is considered to be an area of high vulnerability;



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- an area having an ISI score greater than or equal to 30, but less than or equal to 80, is considered to be an area of medium vulnerability; and,
- an area having an ISI score of greater than 80 is considered to be an area of low vulnerability.

The Thames-Sydenham and Region Source Protection Committee has determined, using the ISI method, that the western half of the Site is located within an HVA with a vulnerability score of 6 (**Drawing 18**).



7. Impact Assessment

7.1 Water Well Users

A search of the Ontario MECP WWR database was completed using a buffer of 1000 m from the centre of the Site to account for the site area. This resulted in the identification of 62 records for an area within approximately 500 m from the eastern and western Site boundaries and approximately 800 m from the northern and eastern site boundaries (**Drawing 19**). The majority of the wells were found to be located along Marion Street north of the Site.

Water uses in the area include the following:

- Domestic or domestic and livestock (45 wells);
- Livestock (1)
- Monitoring, test holes or observation wells (12 wells);
- Public (1);
- Unknown use (1); and
- Abandoned wells (2).

The approximate locations of identified wells are shown on **Drawing 19**, with the MECP WWR Summary provided in **Appendix F**. One of the MECP WWR classified as municipal (MECP Well ID 7115588) is a monitoring well based on the driller's log.

Domestic water supply in the local area wells is generally drawing from the confined intermediate sand and gravel aquifer or from the bedrock aquifer. Four (4) domestic wells and one public well within 500 m of the Site are reported as being less than 10 m deep. These wells were all installed between 1966 and 1979 and may no longer be in use given that much of the surrounding area is now developed and connected to municipal services as evident by the presence of fire hydrants in the area. If construction activities extend into the sand and gravel aquifer, there may be some impact to these shallow wells. A well survey was completed to further assess potential impacts. Results of the well survey are presented below.

Monitoring wells have been installed at the Site as part of the Site investigations to document stabilized groundwater conditions. Prior to the Site grading work, and when the monitoring wells are determined to be no longer required, the wells should be properly decommissioned in accordance with Ontario Regulation 903. Decommissioning a well which is no longer in use helps to ensure the safety of those in the vicinity of the well, prevents surface water infiltration into an aquifer via the well, prevents the vertical movement of water within a well, conserves aquifer yield and hydraulic head and can potentially remove a physical hazard.

7.2 Door to Door Well Survey

A door-to-door survey was completed in the vicinity of the mapped MECP WWR within 500 m of the Site along Marion Street to the north, Clara Street to the east, Catherine Street to the South and Ron Allen Drive to the west to confirm whether the shallow domestic wells are still in use. A total of 87 well survey forms were delivered on April 26, 2022.

To date, 12 responses have been received by EXP, and are summarized in **Table 7**, with full responses provided in **Appendix L**.



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Table 7 – Well Survey Questionnaire Response Summary

| Address | Response Received |
|-----------------------|---|
| 4647 Marion Street | Municipal Water – No well present |
| 4611 Marion Street | Private Well: ~1.8 m bgs shallow well installed more than 60 years ago. Static Water Level: shallow *Based on the MECP WWR Driller Log, this well is dug to 24.4 m bgs (WWR Well ID: 4102895) No connection to municipal water |
| 4984 Marion Street | Private Well- 19.8 m bgs well in use Likely no municipal water |
| 4673 Marion Street | Private Well- 25.9 m bgs drilled well installed in ~1964 Static Water Level: 18.9 m bgs The property is connected to municipal water and the well is no longer in use. |
| 4231 Catherine Street | Municipal Water – No well present |
| 3826 Catherine Street | Private Well- in use well installed in ~1954, depth unknown Likely no municipal water |
| 3832 Catherine Street | Municipal Water – No well present |
| 4216 Catherine Street | Likely municipal water |
| 4218 Catherine Street | Likely municipal water |
| 289 Clara Street | Municipal Water – No well present |
| 268 Clara Street | Private Well: ~2.4 m bgs shallow dug well Static Water Level: approximately 1.8 m bgs The property is connected to municipal water and the well is no longer in use. |
| 272 Clara Street | Municipal Water – No well present |

Based on the results from the door-to-door survey, it has been confirmed that a number of residences within 500 m of the Site utilize private well water.

7.3 Surface Water Features

Several drains are mapped within the Site include the Sandusky Drain, the Porter Subdivision Drain and the Hunter Branch which all drain south into the Hunt Drain. EXP staff noted the Porter Subdivision Drain does not exist on Site. Additionally, there are unmapped wetlands including Wetland A to the west of the Sandusky Drain and Wetland B and Wetland C in the northeast portion of the Site. Maps of the surface water features and drainage on Site are provided in **Drawing 2** and **Drawing 3**.

Wetland B is proposed to be removed and may be either compensated on-site in Wetland C or off-site. Wetlands A and C as well as the Sandusky Drain will be predominantly retained.



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The current design plan for the Site includes natural heritage buffer areas surrounding each wetland area. During development of catchment areas to wetland features and surface water features, it is important that design features are considered which will provide sufficient quality and quantity of runoff and infiltration to the natural features, in order to maintain existing conditions.

The wetland and surface water features are considered as being vulnerable to contamination from surface sources. During construction, short term impacts to the surface water may be anticipated, particularly where vegetation on nearby land is stripped and area grading works are underway.

The following comments are provided with recommendations to help minimize impact to surface water features observed at the site:

- During the site grading work, suitable sedimentation controls will be required to help control and reduce the turbidity of run-off water which may flow towards the surface water features;
- A Best Management Practice (BMP) and spill contingency plan (including a spill action response plan) should be in place for fuel handling, storage and onsite equipment maintenance activities to minimize the risk of contaminant releases as a result of the proposed construction activities;
- Re-establishing vegetative cover in disturbed areas following the completion of the construction work;
- Limit the use of commercial fertilizers in landscaped areas which border a habitat feature; and,
- Limit the use of salts or other additives for ice and snow control on the roadways and parking areas.

7.3.1 General Comments

As due diligence, the following comments are provided with recommendations to help minimize impact to the surface water features on Site:

- During the site grading work, suitable sedimentation controls will be required to help control and reduce the turbidity of run-off water;
- A Best Management Practice (BMP) and spill contingency plan (including a spill action response plan) should be in place for fuel handling, storage and onsite equipment maintenance activities to minimize the risk of contaminant releases as a result of the proposed construction activities;
- Re-establishing vegetative cover in disturbed areas following the completion of the construction work;
- Limit the use of commercial fertilizers in landscaped areas which border a habitat feature; and,
- Limit the use of salts or other additives for ice and snow control on the roadways and parking areas.

7.4 Construction Dewatering Considerations

Daily construction water takings in excess of 50,000 L/day require an Environmental Activity and Sector Registry (EASR) in accordance with Ontario Regulation 63/16. For volumes of 400,000 litres or more per day, a Category 3 permit to take water (PTTW) applications will need to be approved by the MECP according to Sections 34 and 98 of the Ontario Water Resources Act R.S.O. 1990 and the Water Taking and Transfer Regulation O. Reg. 387/04.

Initial groundwater levels across the Site have been relatively high and near ground surface with groundwater levels up to less than 1 m bgs, with the exception of groundwater levels in monitoring well BH6/MW which is a the deepest



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well screened at 10.7 m bgs. For the dewatering calculations, groundwater elevations were assumed at 0.5 m bgs, for the purposes of calculating the 'worst case scenario'. The dewatering calculations are based on existing conditions in the southwest portion of the Site where a shallow saturated sandy aquifer was observed.

Dewatering calculations were completed based on the following conservative assumptions:

- basement excavations of 20 x 20 m;
- sanitary sewer excavations of 5 x 50 m;
- steady state unconfined flow conditions are occurring;
- a groundwater elevation at 0.5 m bgs was assumed based on shallow groundwater levels found seasonally across the Site;
- dewatering target is assumed to be 0.5 m below base of excavation at 3.0 m bgs (basement foundation) and 3.5 m bgs (sanitary sewer);
- the underlying confining layer of sandy silt was encountered at approximately 250 m amsl (6 m bgs);
- the saturated sand is assumed to be encountered at the dewatering target depth; and
- the predominant soil to be encountered is sand with a hydraulic conductivity of 8.2 x 10⁻⁴ m/s.

The Dupuit Forcheimer Equation for unconfined flow into a radial excavation for the basement and linear excavation for the sanitary sewer (Powers et al., 2007) were used to estimate lateral flow into the proposed excavations. Based on the assumptions above, the estimated maximum dewatering rate at the proposed excavations is approximately 1,500,000 L/day for the basement and 2,500,000 L/day for the sanitary sewer. Dewatering calculations are provided in **Appendix M**.

Based on available groundwater levels and hydraulic conductivities of soils at the Site and assuming typical foundation depth of 3.5 m bgs for servicing and/or basement construction, a Category 3 PTTW for dewatering purposes is expected to be required. Dewatering estimates will need to be updated once a detailed design for the Site becomes available.

Any collected water from service trenches and temporary excavations should be discharged a sufficient distance away from the excavated area to prevent the discharge water from returning to the excavation. Sediment control measures should be provided at the discharge point of the dewatering system.

During construction, short term impacts to the near surface and shallow groundwater quantity may be anticipated as a result of construction dewatering where wet soils are present in open excavations. The length of time where this impact would occur would be limited to the time when active pumping of the groundwater is being carried out. Once construction activities are complete, the shallow groundwater levels would be expected to stabilize.

Several of the private wells in the area are installed in the shallow sand and gravel aquifer to depths less than 10 m bgs. Residents in the vicinity of the Site should be notified prior to construction activities and contingency measures will need to be in place to mitigate impacts to their water supply, if necessary.



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8. Qualifications of Assessors

EXP Services Inc. provides a full range of environmental services through a full-time Earth and Environmental Services Group. EXP's Environmental Services Group has developed a strong working relationship with clients in both the private and public sectors and has developed a positive relationship with the Ontario MECP. Personnel in the numerous branch offices form part of a large network of full-time dedicated environmental professionals in the EXP organization.

This report was authored by Ms. Hagit Blumenthal M.Sc., P.Geo. Ms. Blumenthal has experience in conducting hydrogeological assessments. Ms. Blumenthal is a hydrogeologist and environmental geoscientist with more than 8 years' experience in the environmental field, and is a licensed Professional Geoscientist (P.Geo.) in Ontario. She obtained a Master of Science (M.Sc.) in 2010 from the University of Waterloo and has worked in the Hydrogeological and Environmental fields since then.

This report was reviewed by Ms. Heather Jaggard, M.Sc., P.Geo. Ms. Jaggard is a hydrogeologist and environmental geoscientist with more than 9 years in the environmental field and is a licensed Professional Geoscientist (P.Geo.) in Ontario. She obtained a Master's of Science (M.Sc.) in 2012 from Queen's University in Kingston, and is a Qualified Person (QP) registered with the Ontario MECP. She has worked in the Hydrogeological and Environmental fields since that time. In her professional career for the past few years, Ms. Jaggard has completed numerous hydrogeological assessments and modelling works for land development sites. Environmental site assessments and preparation of submissions for PTTW have been part of her routine assignments.



9. References

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Date: June 14, 2022

10. General Limitations

The information presented in this report is based on a limited investigation designed to provide information to support an assessment of the current environmental conditions within the subject property. The conclusions and recommendations presented in this report reflect Site conditions existing at the time of the investigation. Consequently, during the future development of the property, conditions not observed during this investigation may become apparent. Should this occur, EXP Services Inc. should be contacted to assess the situation, and the need for additional testing and reporting. EXP has qualified personnel to provide assistance in regard to any future geotechnical and environmental issues related to this property.

Our undertaking at EXP, therefore, is to perform our work within limits prescribed by our clients, with the usual thoroughness and competence of the engineering profession. It is intended that the outcome of this investigation assist in reducing the client's risk associated with environmental impairment. Our work should not be considered 'risk mitigation'. No other warranty or representation, either expressed or implied, is included or intended in this report.

The comments given in this report are intended only for the guidance of design engineers. The number of test holes required to determine the localized underground conditions between test holes affecting construction costs, techniques, sequencing, equipment, scheduling, etc. would be much greater than has been carried out for design purposes. Contractors bidding on or undertaking the works should in this light, decide on their own investigations, as well as their own interpretations of the factual borehole results, so that they may draw their own conclusions as to how the subsurface conditions may affect them.

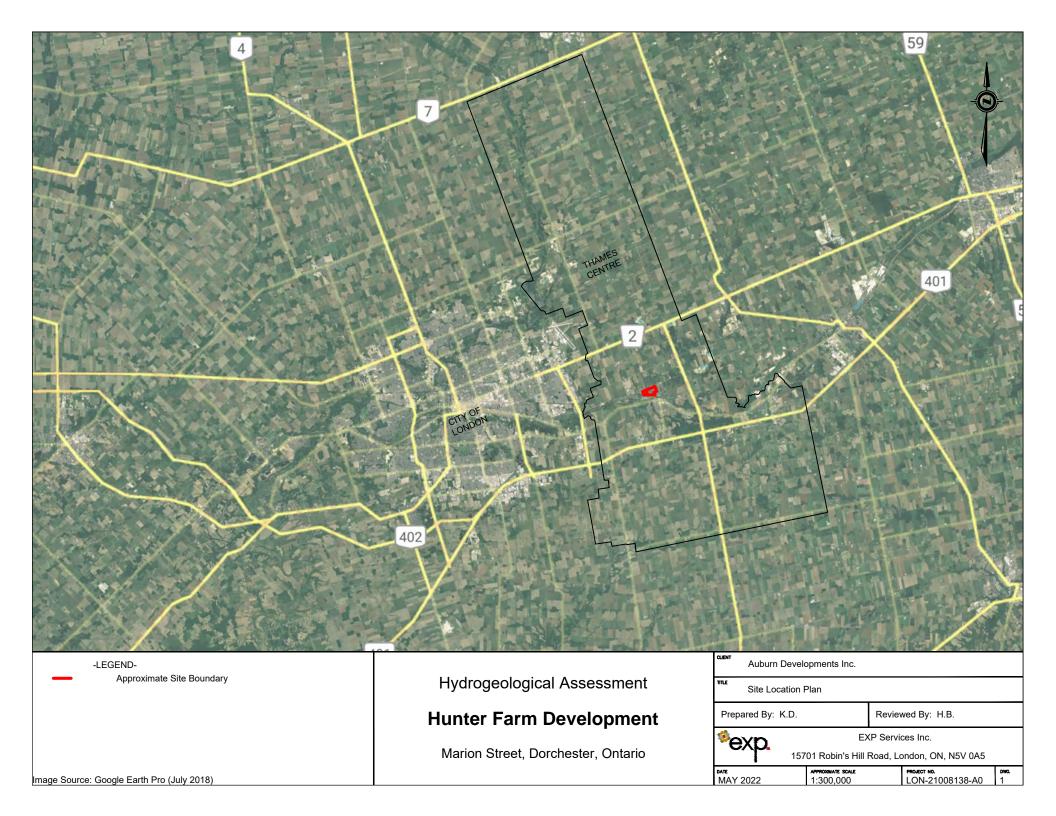
EXP Services Inc. should be retained for a general review of the final design and specifications to verify that this report has been properly interpreted and implemented. If not afforded the privilege of making this review, EXP Services Inc. will assume no responsibility for interpretation of the recommendations in this report

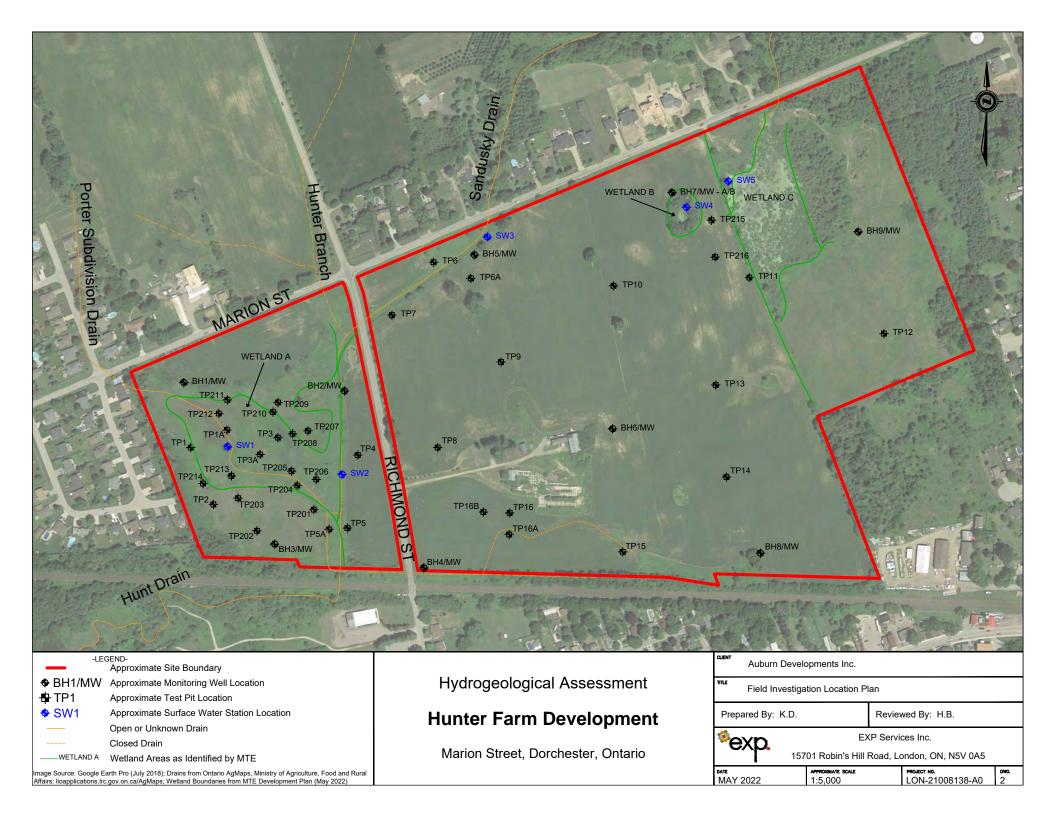
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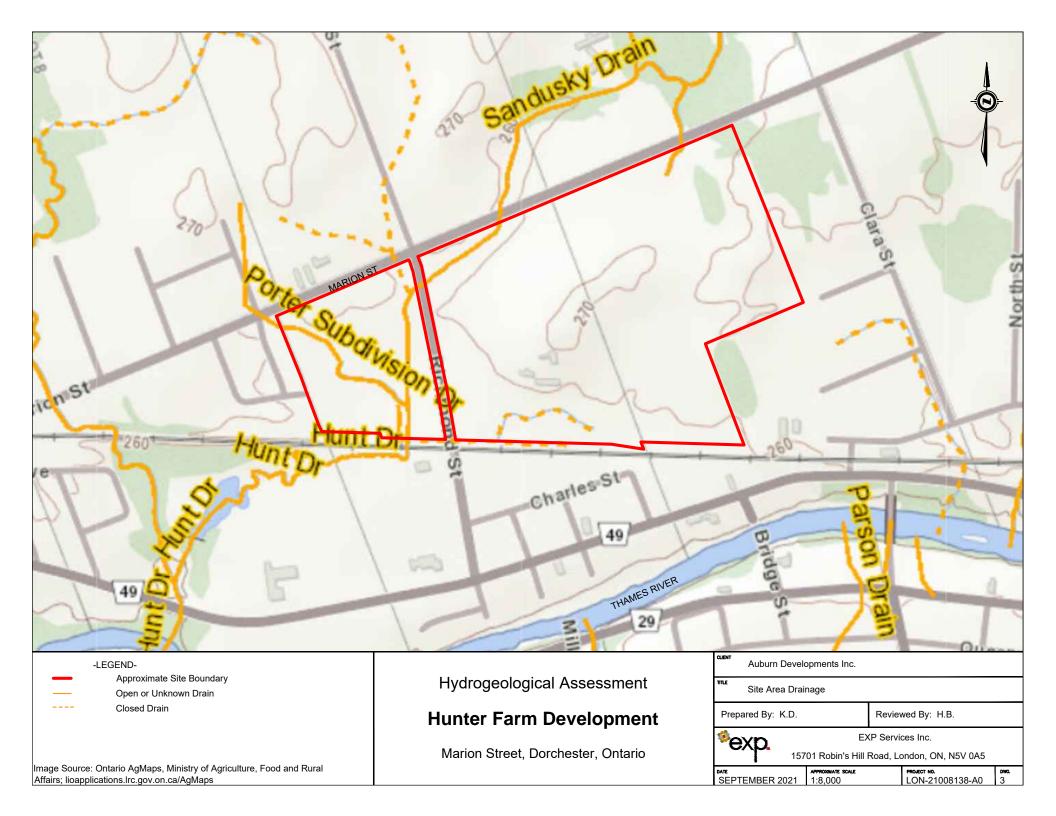
We trust this report is satisfactory for your purposes. Should you have any questions, please do not hesitate to contact this office.

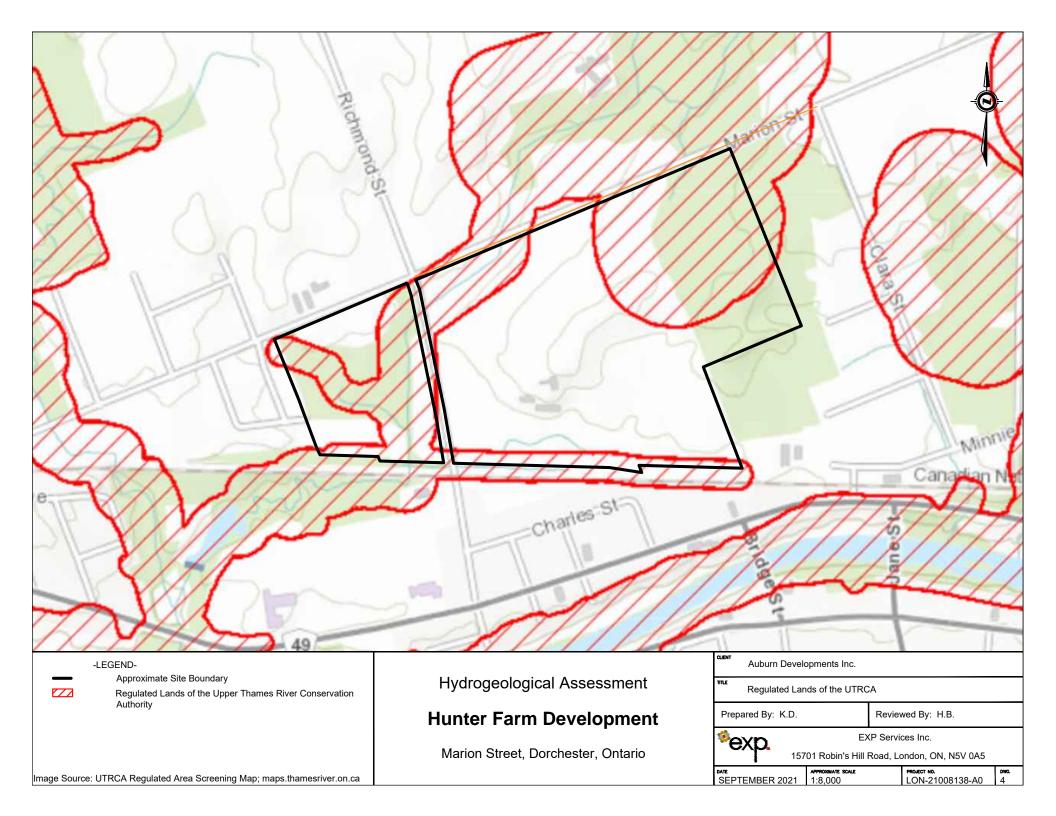


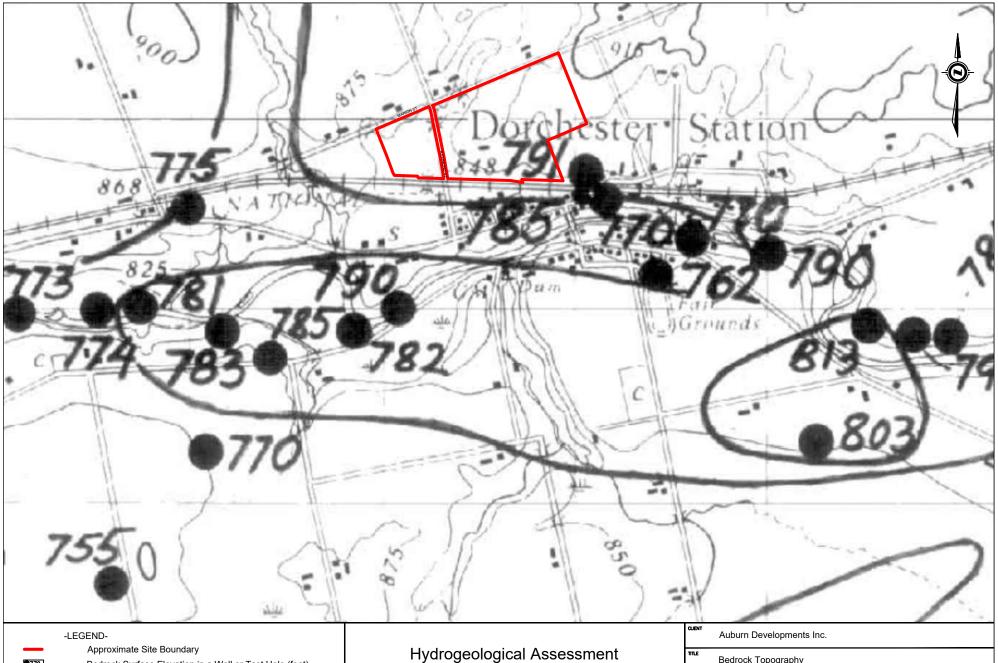
Appendix A - Drawings











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Approximate Site Boundary Bedrock Surface Elevation in a Well or Test Hole (feet)

Contours on Bedrock Surface (feet)

Hunter Farm Development

Marion Street, Dorchester, Ontario

Bedrock Topography

Prepared By: K.D.

Reviewed By: H.B.



EXP Services Inc.

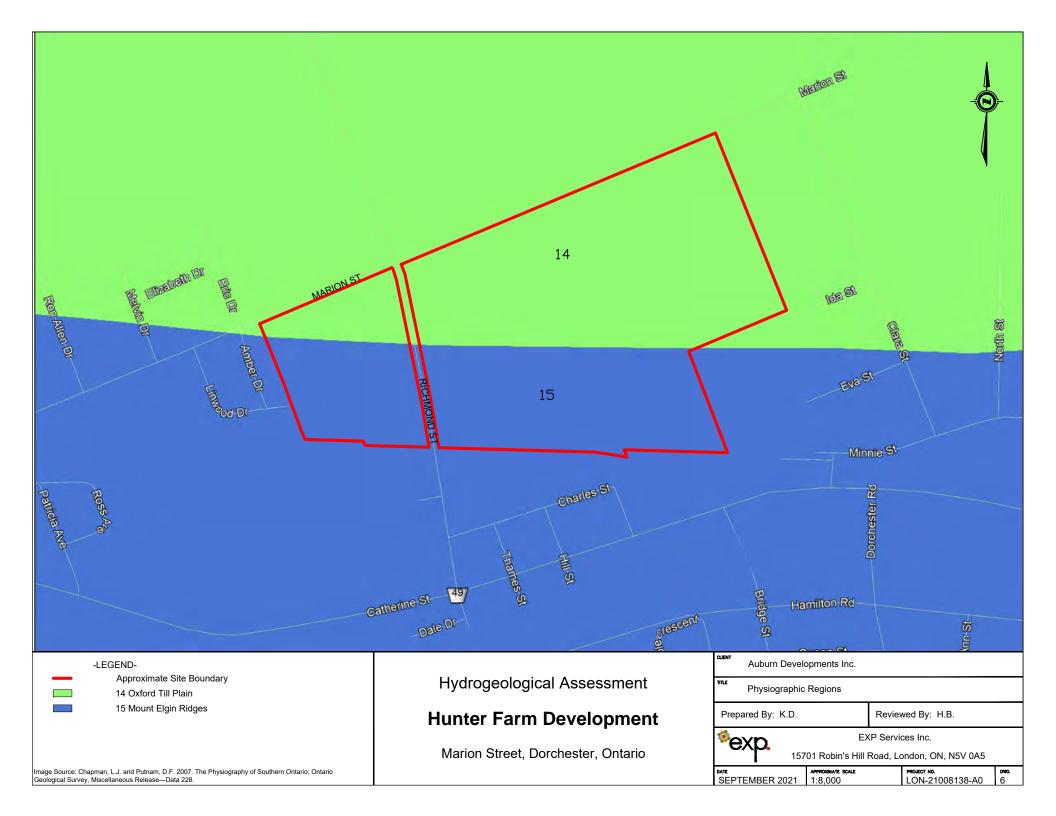
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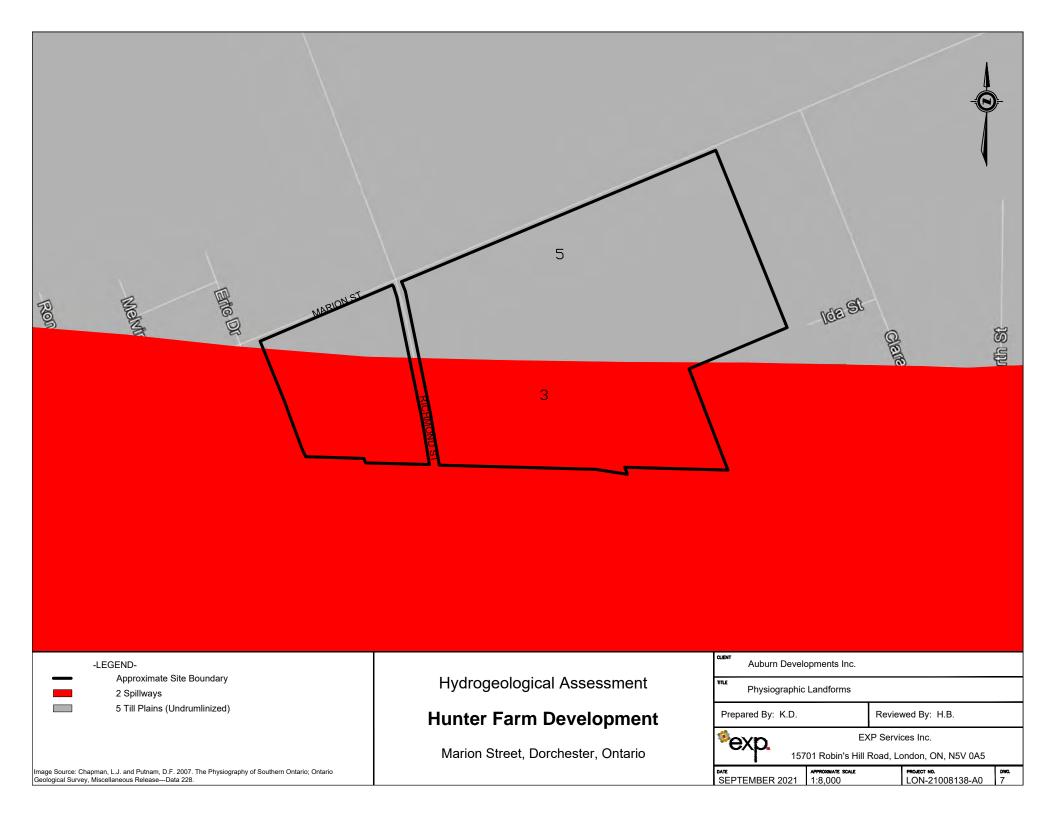
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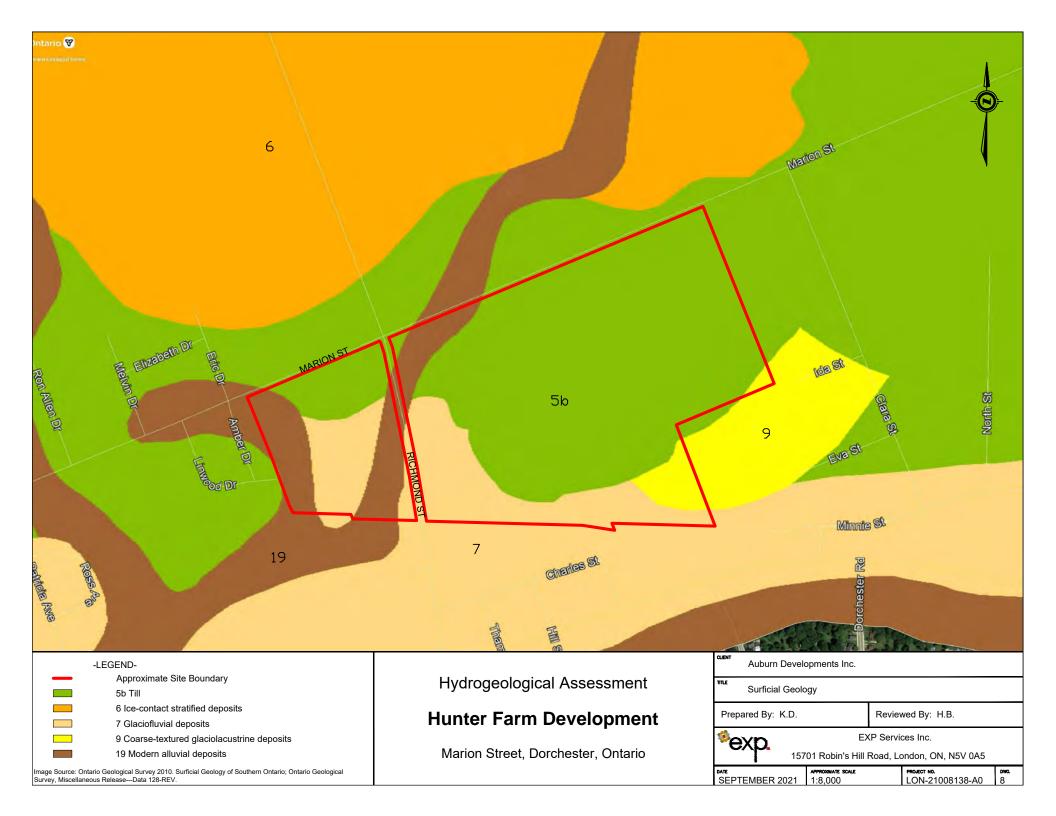
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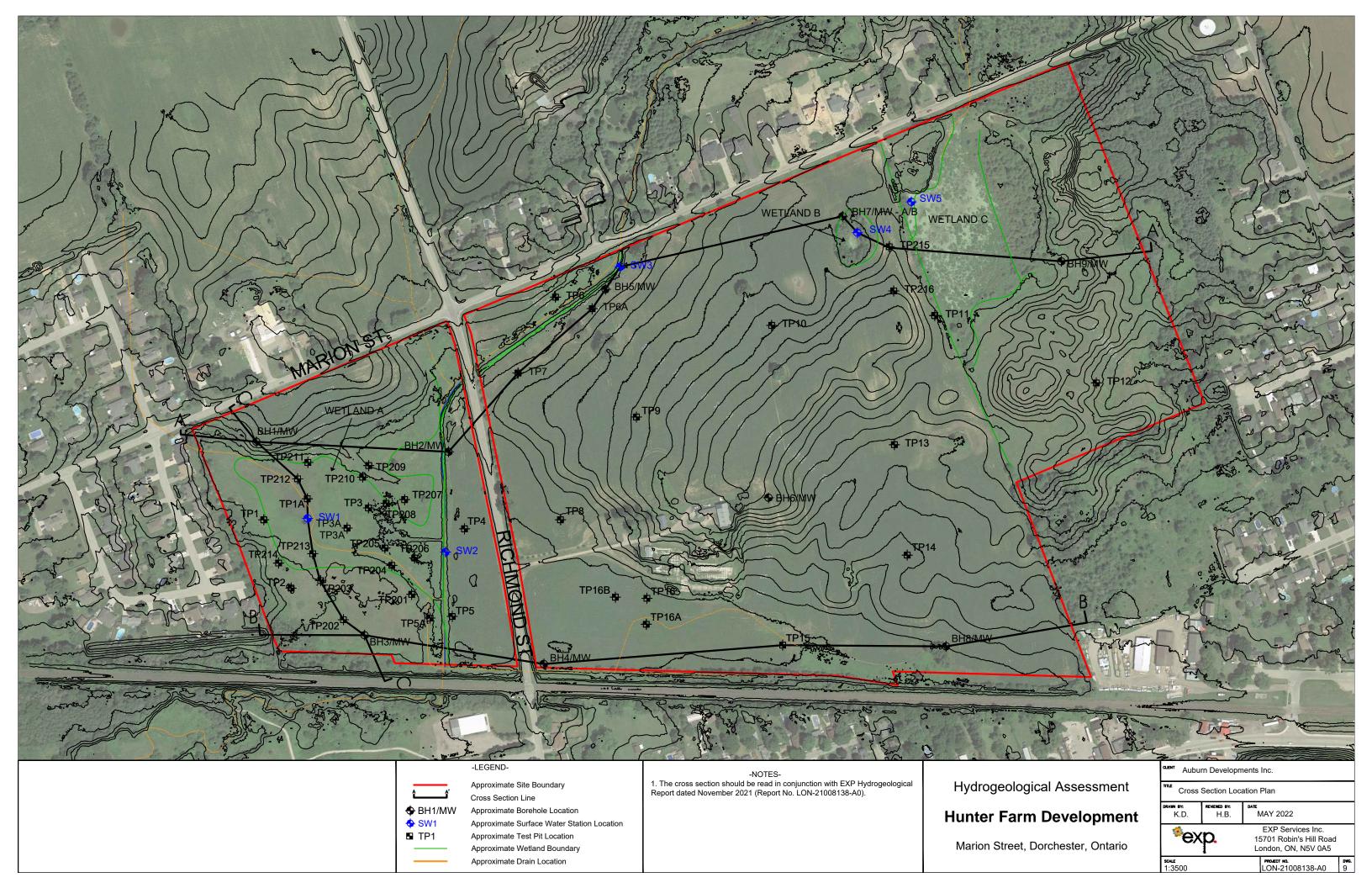
PROJECT NO. LON-21008138-A0

Image Source: Dreimanis, A., Vagners, U.J., and Pinder, G.F., 1968. St. Thomas Sheet, Southern Ontario, Bedrock Topography Series; Ontario Geological Survey, Preliminary Map No. P.482, 1:50,000.

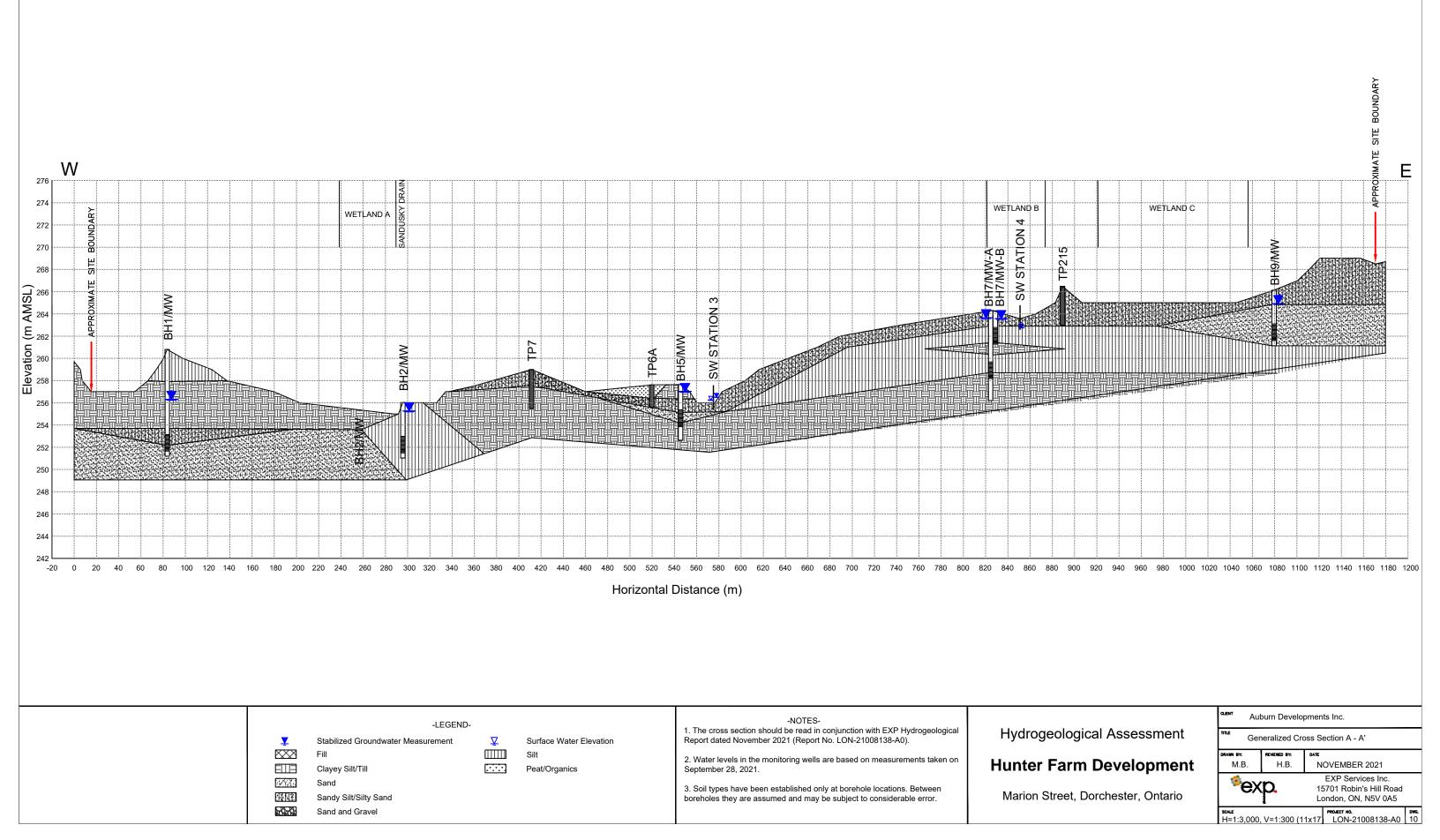




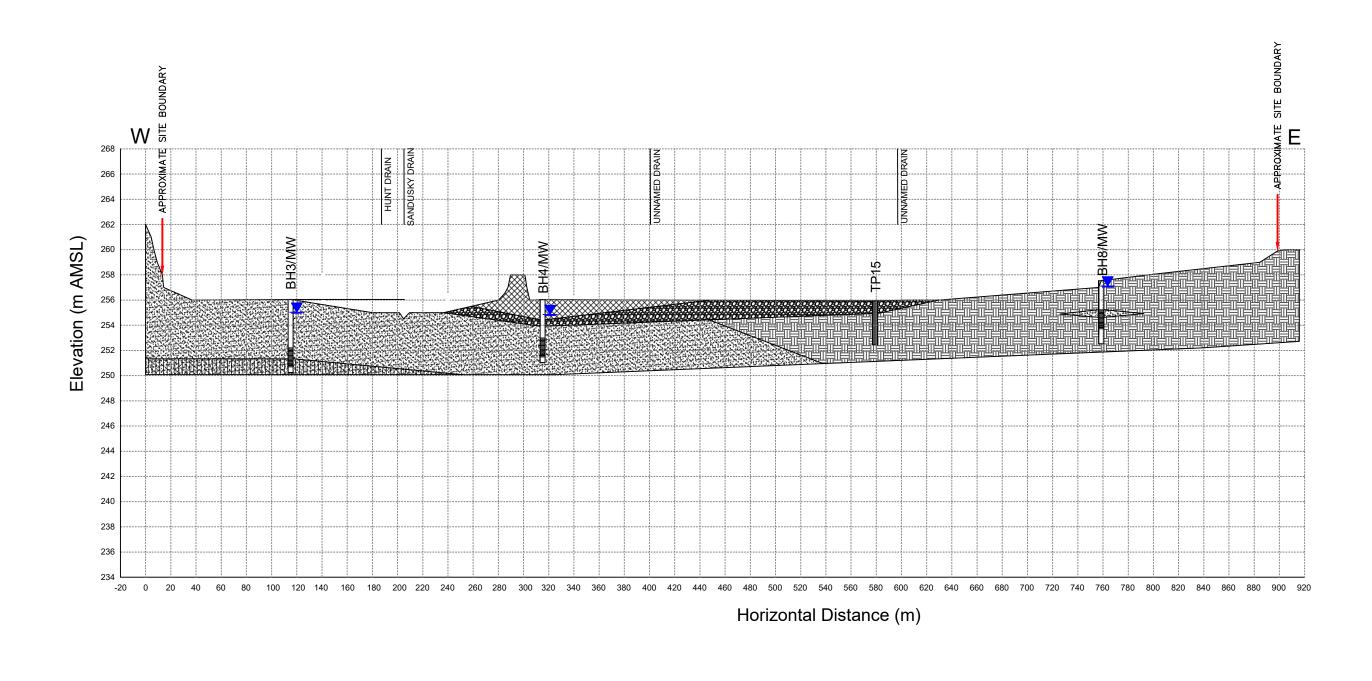


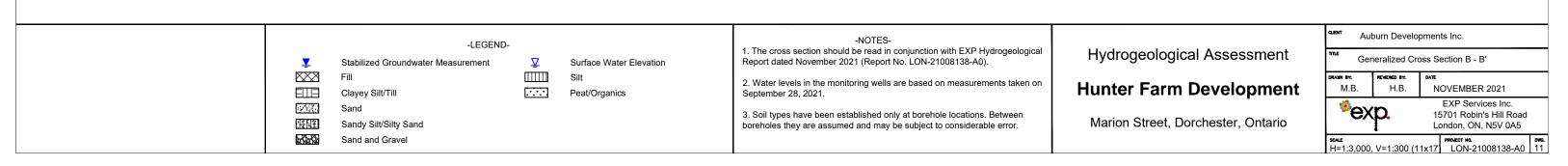


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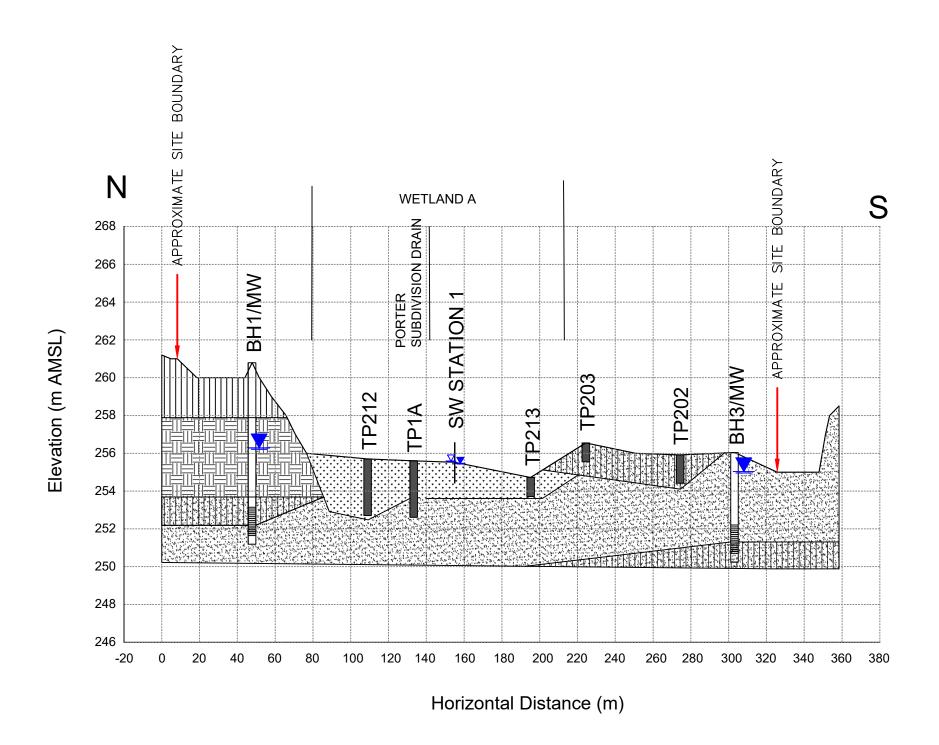


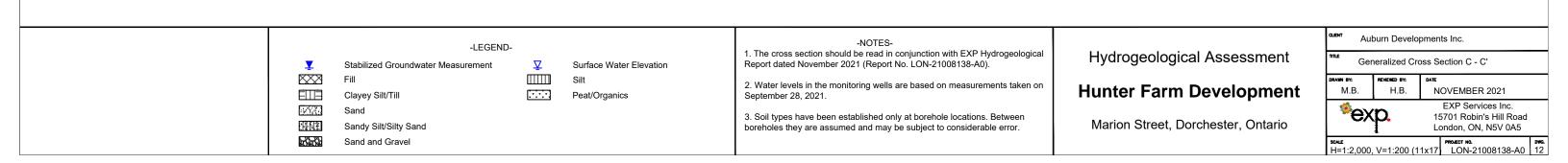
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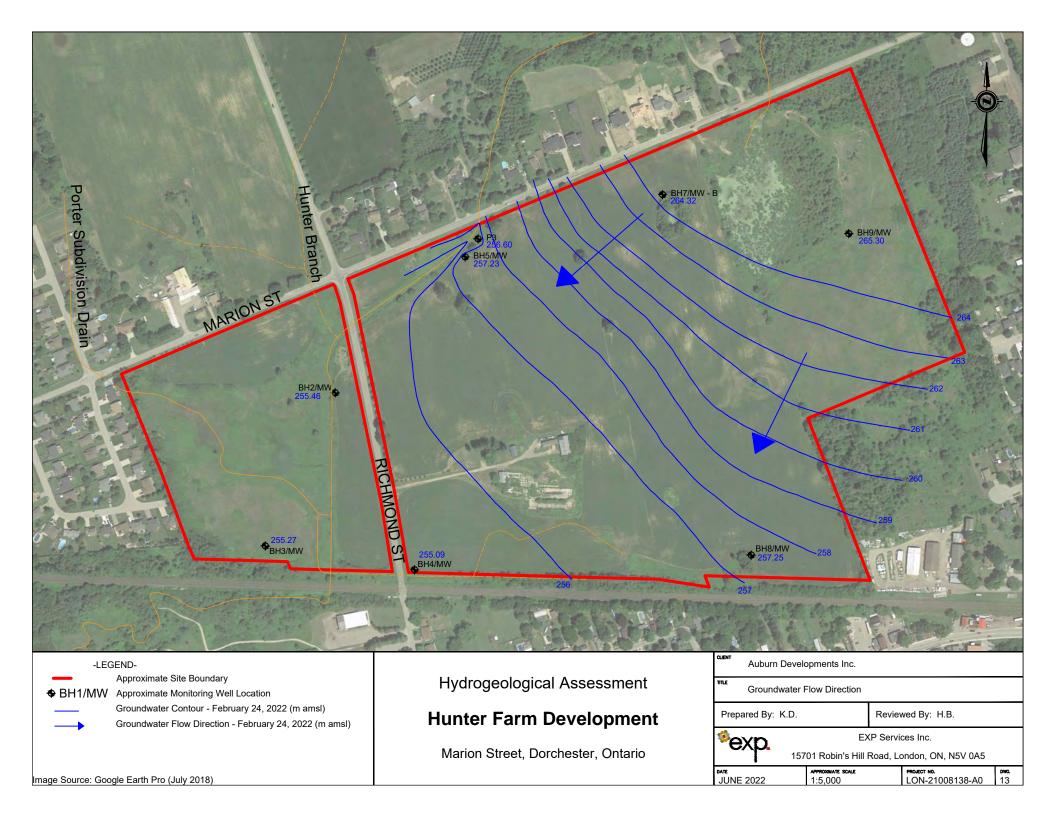


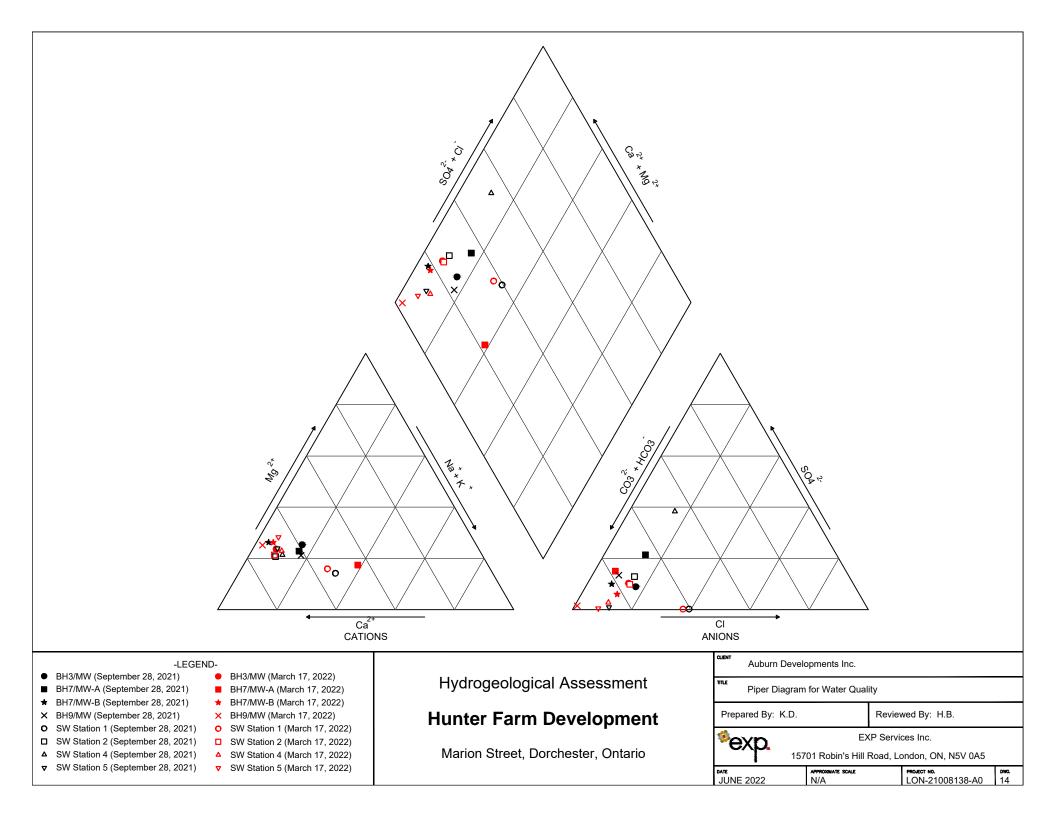


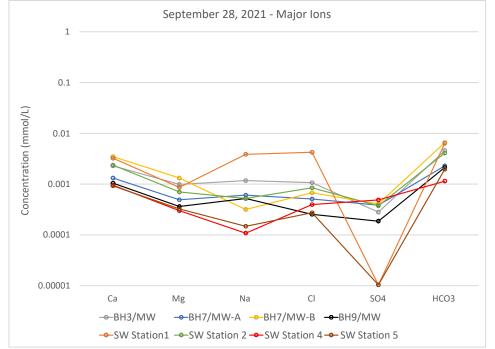
CROSS SECTION C-C'

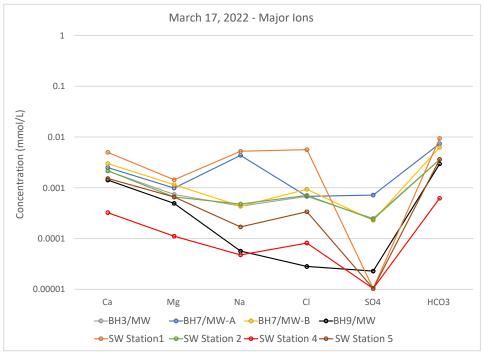










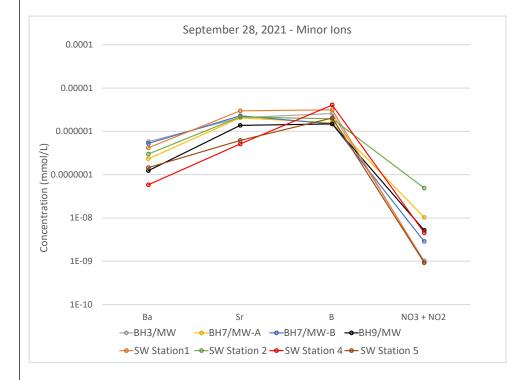


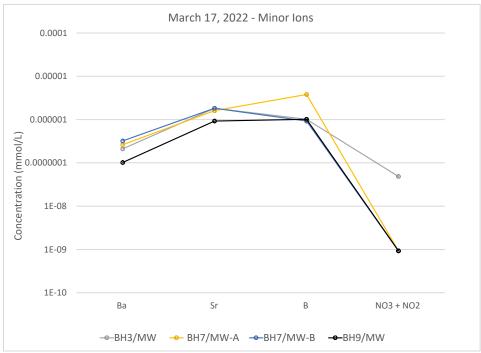
Hydrogeological Assessment

Hunter Farm Development

Marion Street, Dorchester, Ontario





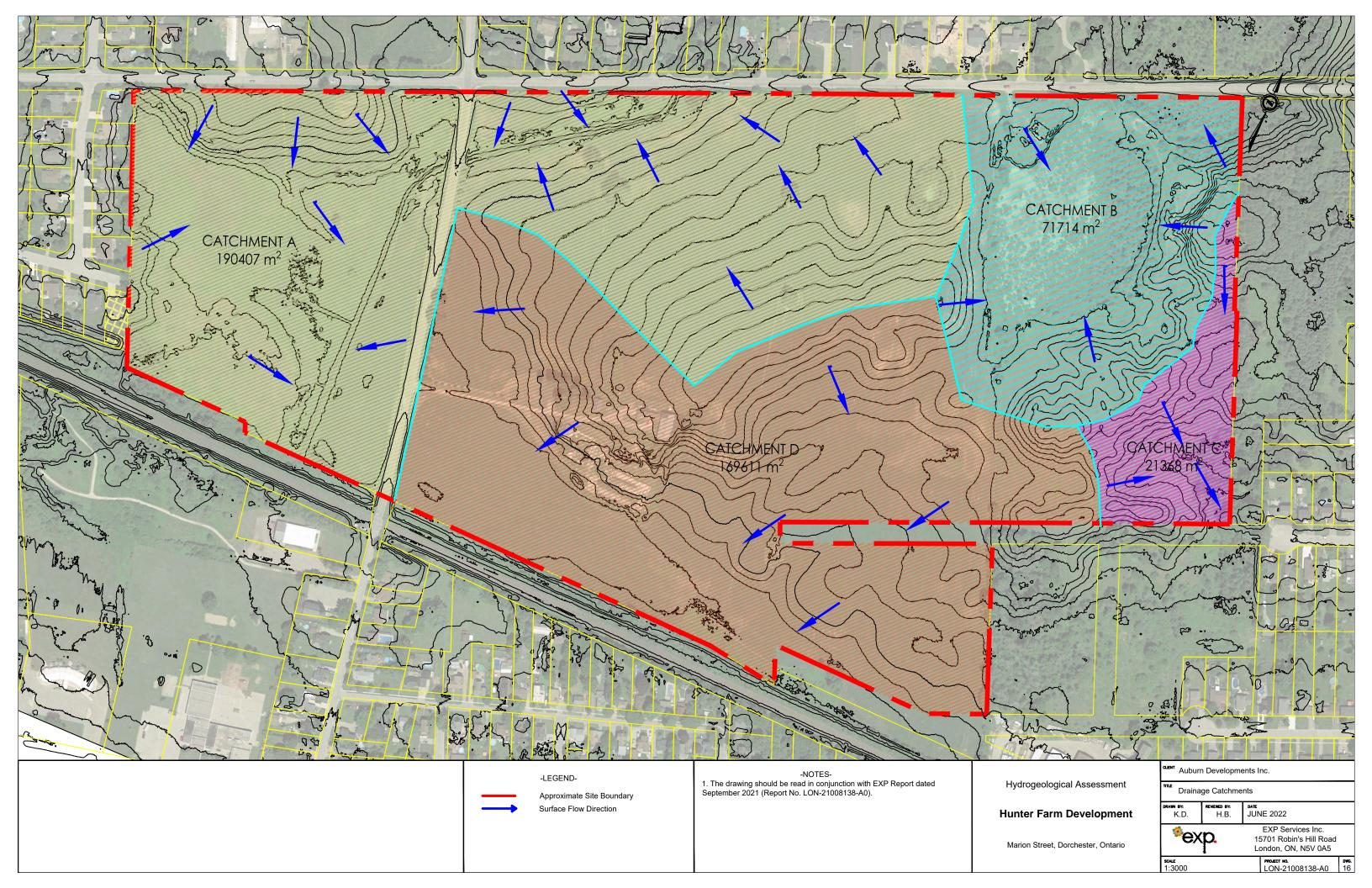


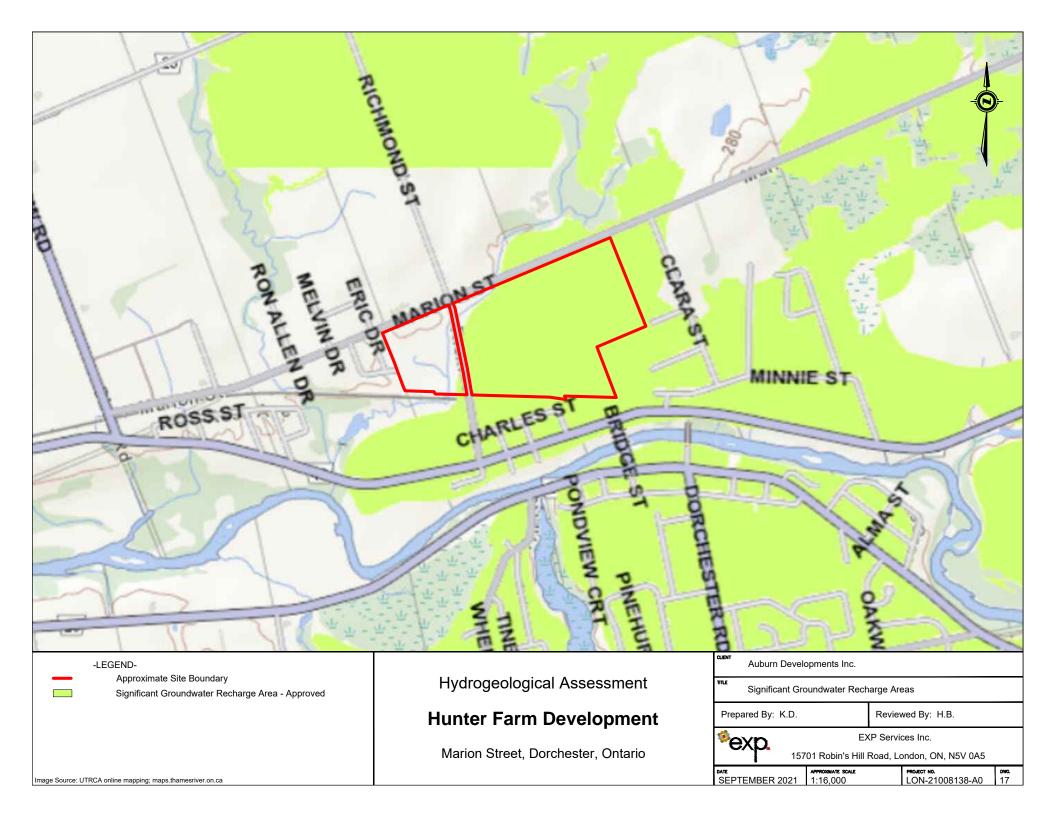
Hydrogeological Assessment

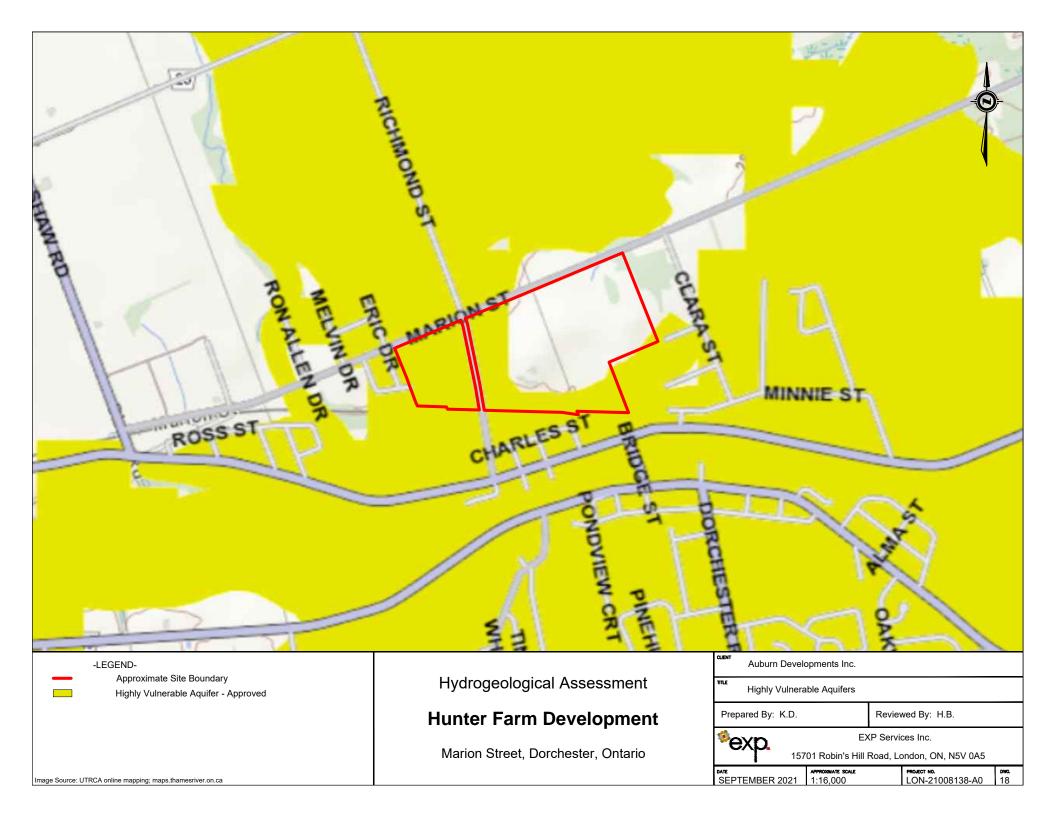
Hunter Farm Development

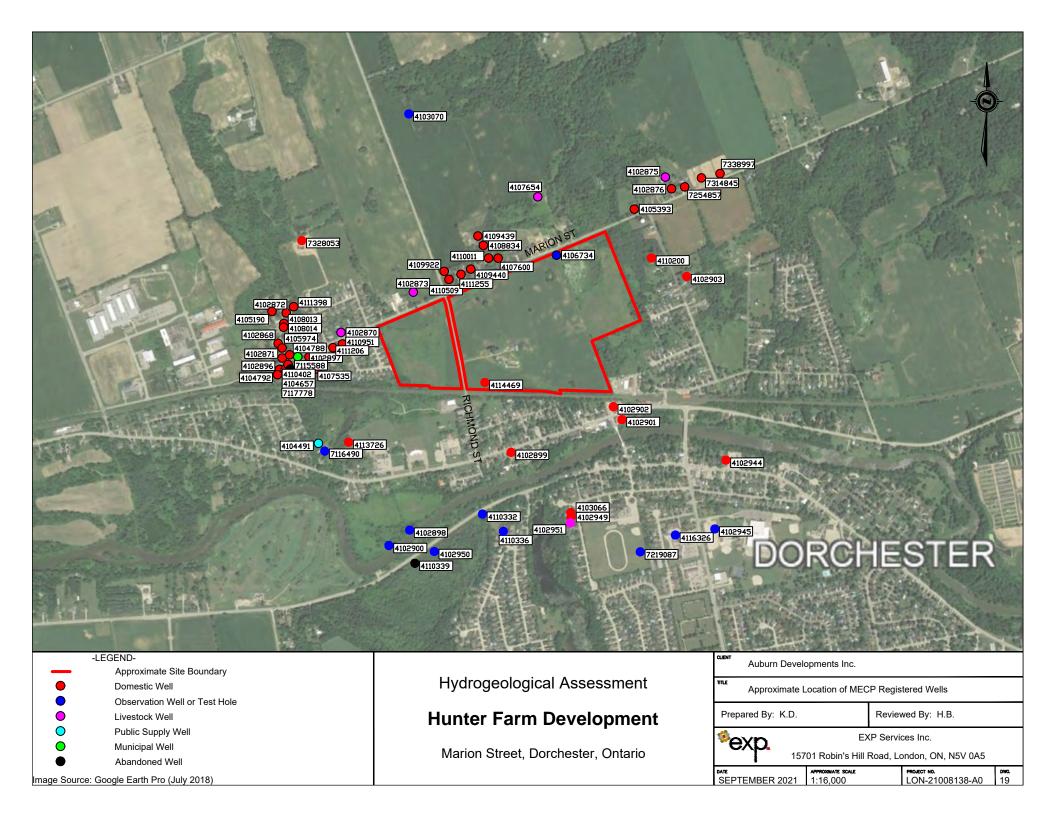
Marion Street, Dorchester, Ontario



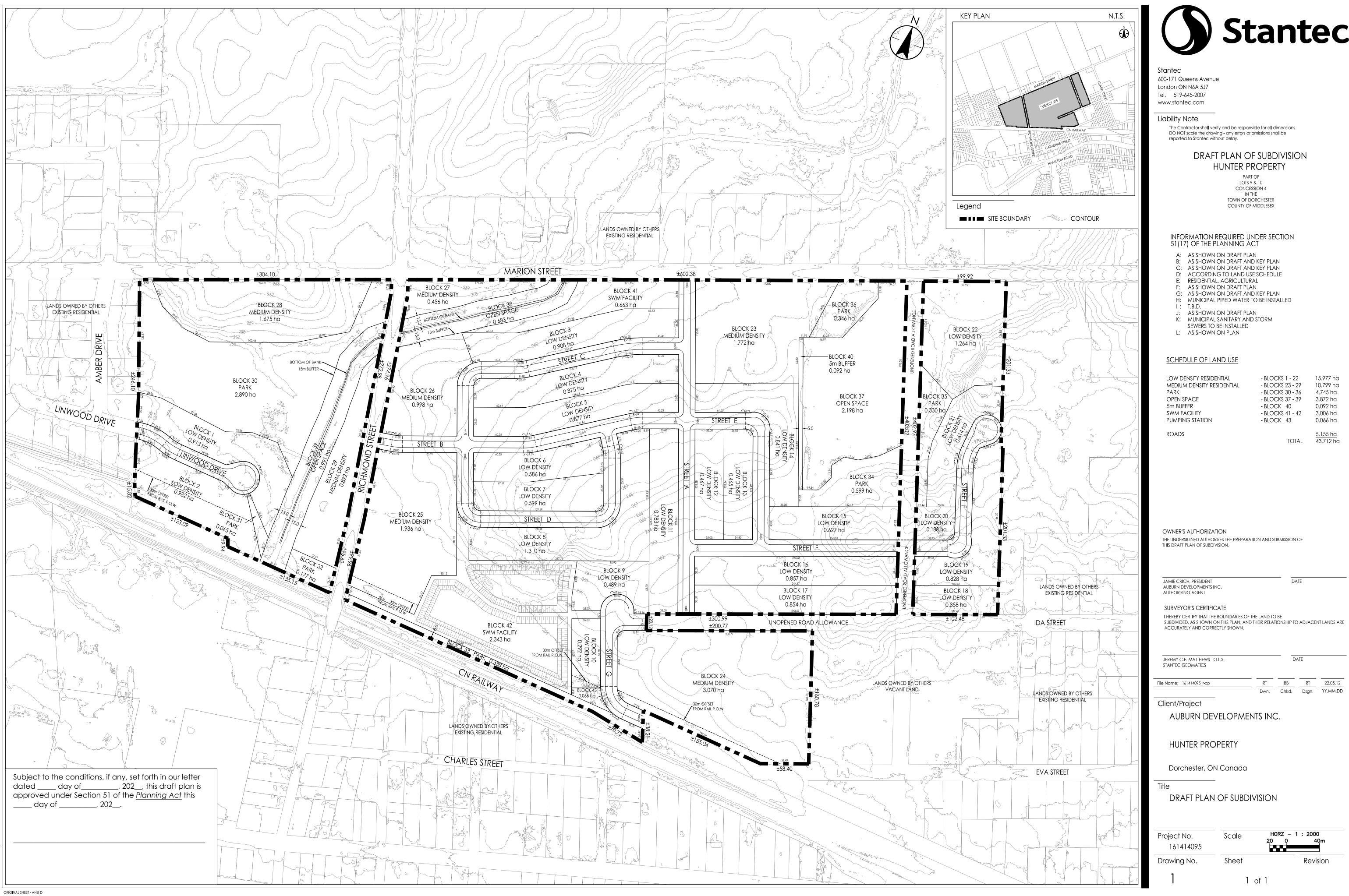


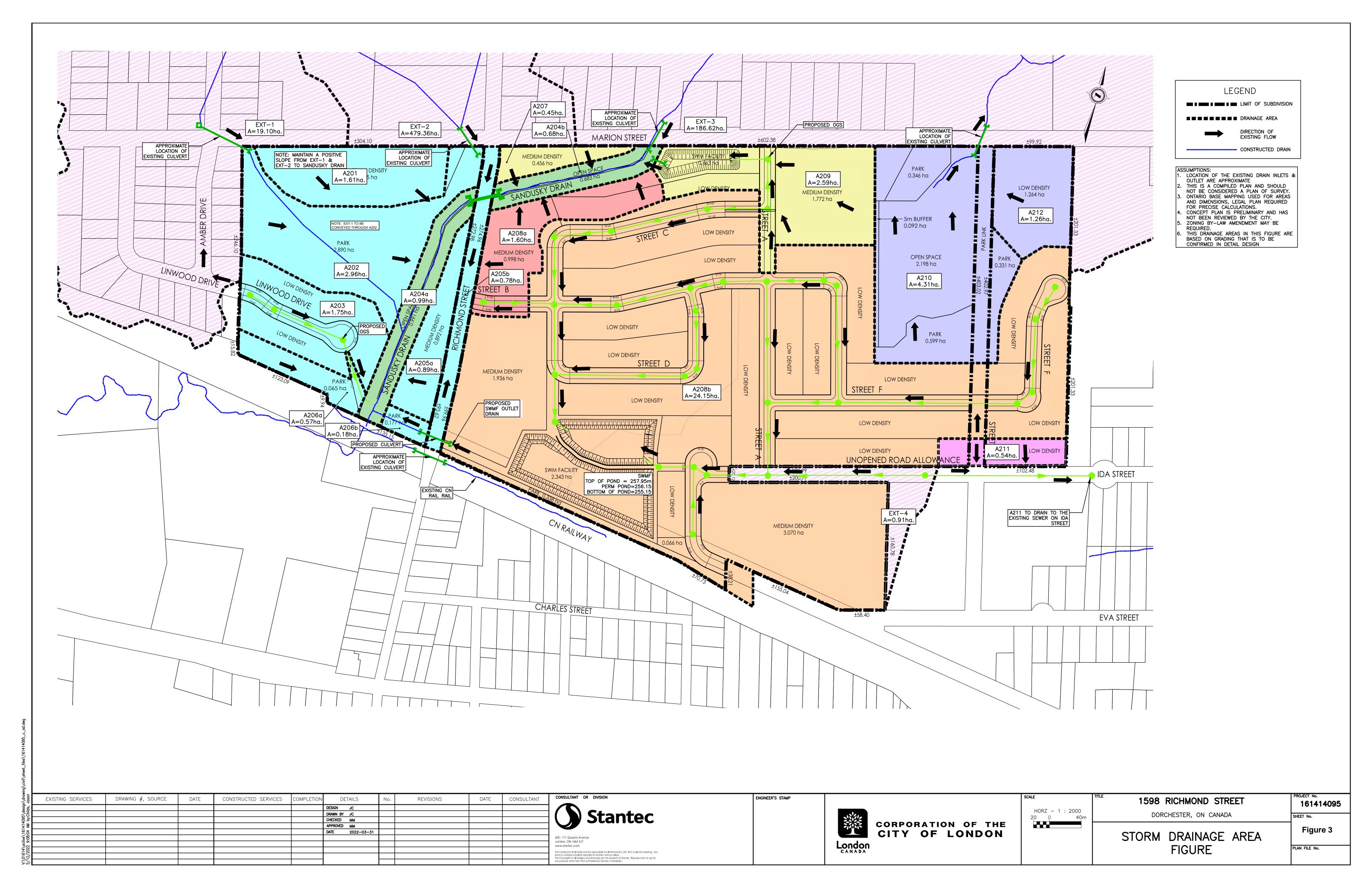






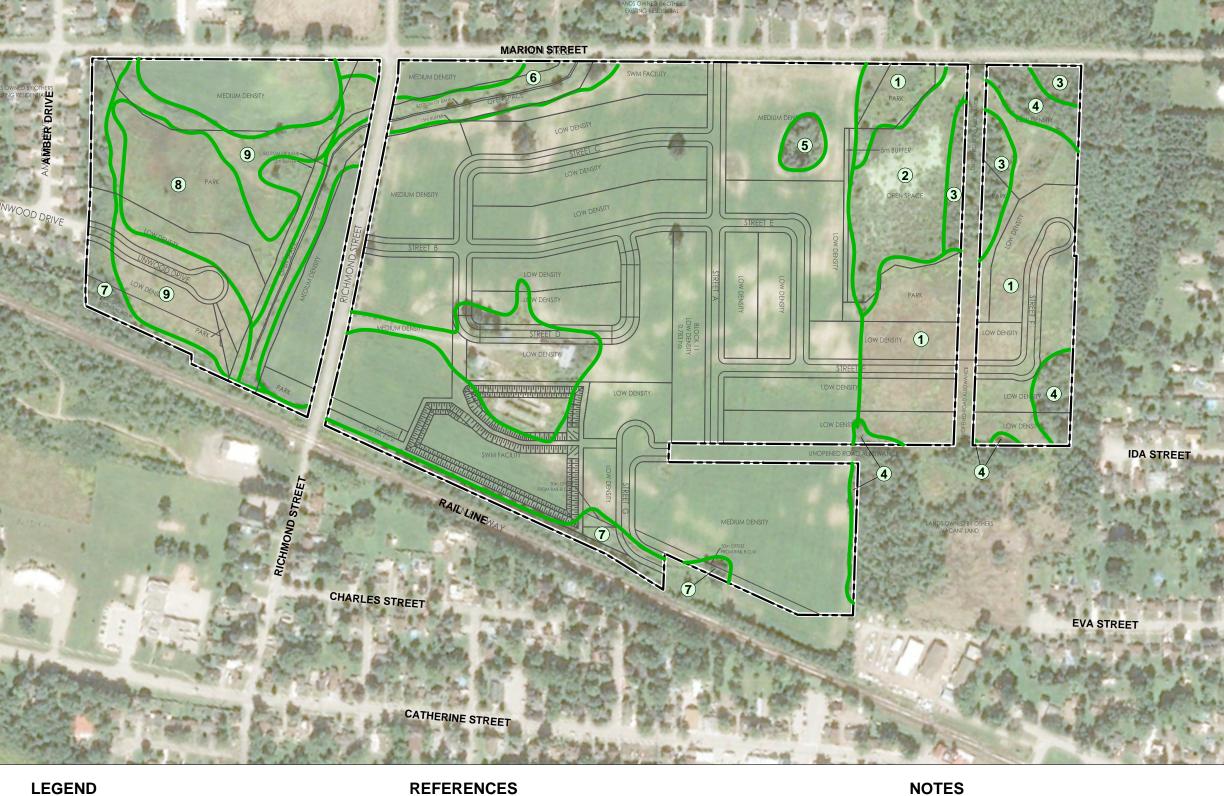
Appendix B – Development Plan

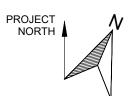




——— SITE BOUNDARY

VEGETATION COMMUNITY





| NUMBER | ELC CODE | Description |
|--------|-----------|---|
| 1 | CUM1 | Mineral Cultrual Meadow |
| 2 | MAS3 | Organic Shallow Marsh |
| 3 | SWC3 | White Cedar Organic Coniferous Swamp |
| 4 | CUW1 | Mineral Cultrual Woodland |
| 5 | MAS | Shallow Marsh |
| 6 | MAMS/CUM1 | Mineral Meadow Marsh / Mineral Cultrual Meadow |
| 7 | CUM1 | Mineral Cutural Meadow |
| 8 | MAM2 | Mineral Meadow Marsh |
| 9 | CUM1 | Mineral Cutural Meadow |
| 10 | | Residential Farmyard |





NATURAL HERITAGE REPORT HUNTER SUBDIVISION DORCHESTER, ONTARIO

THIS FIGURE IS SCHEMATIC ONLY AND TO BE READ IN CONJUNCTION WITH ACCOMPANYING TEXT.

BING IMAGERY USED FOR ILLUSTRATION

PURPOSES ONLY AND NOT TO BE USED FOR MEASUREMENTS. ALL LOCATIONS ARE APPROXIMATE.

DEVELOPMENT PLAN

| ıwn | Scale |
|-------------|--------------------------|
| DCH | AS SHOWN |
| ecked | Project No. 48975-100 |
| e May 16/22 | Rev No. |

FIGURE 8

BING IMAGERY AS OF JANUARY 18 - 2022 (IMAGE DATE UNKOWN); MRN LIO DATA, WATER BODIES AND WATER COURSES, 2022; AND CONCEPT PLAN PROVIDED BY STANTEC, AUTOCAD FILE "cad_161414095_20220513_draft_plan.dwg", MAY 13 - 2022.

Appendix C – Scoping Meeting Notes (April 20, 2022)

From: <u>Stefanie Pratt</u>

To: Heather Jaggard; John Bice; Stephen Stapleton
Cc: Jenna Allain; Karen Winfield; Kelli Dobbin
Subject: Re: 1598 Richmond Street, Dorchester, Thames Centre

Subject: Re: 1598 Richmond Street, Dorchester, Ti Date: Wednesday, April 20, 2022 9:01:32 PM

Attachments: <u>ATT00001.bmp</u>

ATT00002.bmp ATT00004.png ATT00005.png



Hi Stephen,

As noted in John's email below, we will not be requiring a TOR for this project as it is nearing completion and would not be a good use of resources for yourselves nor us. We will also not be accepting draft reports at this time. We will await the final reports and accept the package as a whole for review.

While we understand that the EIS was scoped, please be advised that future projects should be fully scoped for EIS and Hydrog in advance of undertaking the required monitoring periods. We have worked with Heather on many projects and are typically comfortable with the scope of work proposed, however it is beneficial for all to have a clear understanding of the site and have the opportunity to provide feedback and input early on.

We will await your formal submission to the municipality and provide feedback at that time.

Kind Regards,

Stefanie Pratt

Planning Coordinator 1424 Clarke Road London, ON N5V 5B9 t: 519-451-2800 ext. 430 e: pratts@thamesriver.on.ca



>>> Stephen Stapleton <sstapleton@auburndev.com> 2022-04-20 5:48 PM >>>

John we have a reputable hydro engineer and a reputable developer that have done these studies for years on many projects..we don't need to waste time of ToR. We will send you our draft reports.

Get Outlook for Android

From: John Bice

Sent: Wednesday, April 20, 2022 11:40:54 AM

To: Heather Jaggard

Heather.Jaggard@exp.com>

Cc: Jenna Allain <AllainJ@thamesriver.on.ca>; Karen Winfield <WinfieldK@thamesriver.on.ca>; Kelli Dobbin

<Kelli.Dobbin@exp.com>; Stefanie Pratt <PrattS@thamesriver.on.ca>; Stephen Stapleton

<sstapleton@auburndev.com>

Subject: RE: 1598 Richmond Street, Dorchester, Thames Centre

Hi Heather,

My last email was rather vague, apologies and I can clarify ToR requirements for you as well as requirements moving

forward. Typically we are looking for a formal ToR letter submission that lays out scope, summary of work to date, locations of monitoring wells, etc. in a formal letter submission. We would like to see this completed in conjunction with the EIS ToR for consistency.

Normally, we would take this ToR and have it reviewed by internal staff. However, since we are currently without a Hydrogeologist on staff we have been sending ToR's to a third party (along with the final study submissions).

Since you are already so far in the process we are not going to be asking for a ToR as you will be submitting the final study within the next month or so. We will await this study and send it for third party review. Apologies for the confusion here. In the future we would prefer to see a ToR near the beginning of the study to ensure consistency with supplementary requirements.

Kind Regards,

John Bice



John Bice Land Use Planner Upper Thames River Conservation Authority (UTRCA) t: <u>519-451-2800</u> ext. 228 e: bicej@thamesriver.on.ca

>>> Heather Jaggard <Heather.Jaggard@exp.com> 20/04/2022 11:15 AM >>> Hi John,

Please specify what exactly you require as a 'formal TOR'. I have only ever completed a HydroG scoping meeting followed by an email summary of study components discussed.

Is the external reviewer looking for a letter memo summarizing the study components completed to date?

Please clarify and I can provide.

Thank you.

Heather Jaggard, M.Sc., P.Geo., QP

EXP | Hydrogeologist, Project Manager

t: +1.226.616.0748 | m: +1.905.977.9030 | e: <u>heather.jaggard@exp.com</u>

exp.com | legal disclaimer

keep it green, read from the screen

From: John Bice

Sent: Wednesday, April 20, 2022 10:57 AM

To: Heather Jaggard

Heather.Jaggard@exp.com>

Cc: Jenna Allain <AllainJ@thamesriver.on.ca>; Karen Winfield <WinfieldK@thamesriver.on.ca>; Kelli Dobbin <Kelli.Dobbin@exp.com>; Stefanie Pratt <PrattS@thamesriver.on.ca>; Stephen Stapleton <sstapleton@auburndev.com>

Subject: RE: 1598 Richmond Street, Dorchester, Thames Centre

Good morning Heather,

Apologies for the delay in getting back to you and thank you for your patience. The UTRCA would require a formal submission of a TOR. Please see UTRCA's Hydro G Guidelines attached if you wish to submit a TOR.

Kind Regards,

John Bice



John Bice Land Use Planner Upper Thames River Conservation Authority (UTRCA) t: <u>519-451-2800</u> ext. 228 e: bicei@thamesriver.on.ca

>>> Heather Jaggard <<u>Heather.Jaggard@exp.com</u>> 11/03/2022 4:09 PM >>> Hi John,

Sure no problem. Please let me know if the following will suffice as a HydroG TOR.

The attached email includes the locations of the monitoring wells and on site surface water features. See below for a list of work completed so far. Monitoring started in May 2021 and is expected to go until May 2022.

- 38 test pits (part of Geotech report)
- 10 monitoring wells in 9 locations installed May 9-10, 2021
- 5 surface water (SW) stations installed May 27, 2021. Shallow piezometer and staff gauge installed at each.
- Monthly WLs since May 2021. To continue until at least May 2022
- 4 SWRT completed in May 2021
- 3 grain size samples
- 4 GW and 4 SW samples in September 2021. Second round scheduled for spring 2022
- Dataloggers in 4 wells and 4 piezometers and a barologger in one well. Installed in wells on May 18, 2021 and in piezometers on May 27, 2021. Will remain in place until at least May 2022.
- Monthly water balance completed
- Rough dewatering estimate completed
- MECP well record search done. Door to door survey scheduled for Spring 2022

Please let me know if you require any additional information at this time.

Thanks very much.

Heather

Heather Jaggard, M.Sc., P.Geo., QP

EXP | Hydrogeologist, Project Manager

t: +1.226.616.0748 | m: +1.905.977.9030 | e: <u>heather.jaggard@exp.com</u>

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From: John Bice < bicej@thamesriver.on.ca > Sent: Thursday, March 10, 2022 8:43 AM

To: Heather Jaggard < <u>Heather.Jaggard@exp.com</u>>

Cc: Jenna Allain < AllainJ@thamesriver.on.ca>; Karen Winfield < WinfieldK@thamesriver.on.ca>

Subject: 1598 Richmond Street, Dorchester, Thames Centre



CAUTION: This email originated from outside of the organization. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Good morning Heather,

Apologies for the delay in getting back to you. Christine had forwarded me your request. We currently do not have a Hydrogeologist on staff to be able to answer any questions you may have in the scoping meeting.

We are completing this review through a third party. Typically we a receiving comments back ranging from 1 to 3 weeks. Could you complete a ToR for the Hydrogeological study, that way we can forward your ToR to our third party reviewer for comments?

Please let me know if this approach works for you?

Thank you,

John Bice



John Bice Land Use Planner Upper Thames River Conservation Authority (UTRCA) t: 519-451-2800 ext. 228

e: bicei@thamesriver.on.ca

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<The contents of this e-mail and any attachments are intended for the named recipient(s). This e-mail may contain information that is privileged, confidential and/or exempt from disclosure under applicable law. If you have received this message in error, are not the named recipient(s), or believe that you are not the intended recipient immediately notify the sender and permanently delete this message without reviewing, copying, forwarding, disclosing or otherwise using it or any part of it in any form whatsoever.>

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Appendix D – Borehole Logs

| | _ |
|----|----|
| ex | D, |
| | 10 |

BH1/MW

Sheet 1 of 1 Auburn Developments Inc. CLIENT PROJECT NO. **LON-21008138-A0** PROJECT Hunter Farm DATUM <u>Geodetic</u> LOCATION Marion Street, Dorchester, ON DATES: Boring May 12, 2021 Water Level August 17, 2021 **SHEAR STRENGTH SAMPLES** STRATA M CONTENT S Field Vane Test (#=Sensitivity) WELL DEPTH ISTURE RECOVERY ▲ Penetrometer ■ Torvane Ν A NUMBER **VALUE STRATA** T P E Atterberg Limits and Moisture **DESCRIPTION** PLOT W_P W W_L (~m) **SPT N Value** × Dynamic Cone (mm) (%) 260.8 (blows) 10 -0 TOPSOIL - 300 mm 260.5 SILT - brown, trace to some clay, trace sand, trace gravel, compact, moist SS SA 1 350 14 11 SS SA₂ 450 20 16 -2 SS SA3 100 27 12 257.9 -3 **CLAYEY SILT TILL** - brown, trace sand, trace SA4 450 20 gravel, very stiff, damp SS 14 4 - some brown, dilatent silt layerin at 4.5 m bgs SS SA 5 400 23 21 -5 -6 - becoming hard near 6.0 m bgs SS SA 6 450 37 13 253.7 SILTY SAND TILL - brown, gravelly, well graded, dense, wet SS SA 7 30 450 8 -8 252.2 SAND - grey, fine to medium grained, trace silt, trace gravel, compact, wet -9 SS SA 8 350 21 16 251.2 End of borehole at 9.6 m bgs. -10 SAMPLE LEGEND ☑ AS Auger Sample ☑ SS Split Spoon ST Shelby Tube **NOTES** Rock Core (eg. BQ, NQ, etc.) VN Vane Sample 1) Borehole Log interpretation requires assistance by EXP before use by others. Borehole Log must be read in conjunction with EXP Report LON-21008138-A0. OTHER TESTS No significant methane gas detected upon completion of drilling. G Specific Gravity C Consolidation No significant metrialle gas detected upon completion of animing.
 bgs denotes below ground surface.
 Geodetic elevation surveyed by using a SOKKIA GCX2 Receiver.
 Water level, May 17, 2021: 4.71 m bgs (Elevation 256.18 m)

 July 20, 2021: 4.86 m bgs (Elevation 256.03 m)
 August 17, 2021: 4.92 m bgs (Elevation 255.97 m)

 CD Consolidated Drained Triaxial H Hydrometer S Sieve Analysis CU Consolidated Undrained Triaxial Y Unit Weight **UU Unconsolidated Undrained Triaxial** P Field Permeability **UC Unconfined Compression DS Direct Shear** K Lab Permeability WATER LEVELS Measured Artesian (see Notes)

| 0.0 | |
|-----|--------------|
| -CX | \mathbf{n} |
| 0/1 | \sim |
| | |

BH2/MW

| | CA | ь. | ΚE | :חנ | JL | | . L | O. | , | | Sheet 1 of 1 |
|-----------------|------------------|---|-----------------|-------------|------------------------|----------|---------------|------------------|-------------------|--------------|--|
| CL | IENT | Auburn Developments Inc. | | | | | | | | PR | ROJECT NO. <u>LON-21008138-A0</u> |
| PR | OJECT | Hunter Farm | | | | | | | | DA | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | В | oring | Ma | ıy 12, 20 | 021 | Water Level <u>August 17, 2</u> 02 |
| | Ę | | ş | | | | SAM | IPLES | | мс | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) |
| Ē | ШЫМ ДТ−ОZ | | STRATA | W E L | | | | R | N | MO-STURE | ▲ Penetrometer ■ Torvane |
| DEPTH | Î | STRATA | Ā | t | Ţ | ; | N U | Ö | VALUE | ŤĖ | , 100 , 200 kPa |
| н | Ö | DESCRIPTION | P | L OG | T Y P E | : | NUMBER | RECOVERY | | E T | Atterberg Limits and Moisture WP W WL |
| (m bgs) | (~m) | | P Q T | G | | | R | Ϋ́ | | | ● SPT N Value × Dynamic Cone |
| -o - | 256.0 | TOPOOL 400 mm | 131 12 · 3 | 1 | <u> </u> | | | (mm) | (blows) | (%) | 10 20 30 40 |
| - | 255.6 | TOPSOIL - 400 mm SILT - grey, trace to some sand, trace gravel, | | 0 0 | | | | | | | |
| _₁ | | dilatent, very loose to compact, very moist to wet | | Ш | | | SA 1 | 400 | 10 | 15 | |
| -1 | | | | ¥ | | 3 | SA I | 400 | 10 | 15 | |
| - | | | | | s | ss | SA 2 | 350 | 8 | 17 | - |
| -2 | | | | | | | | | | | |
| _ | | | | | s | ss | SA 3 | 350 | 9 | 14 | |
| -3 | | | | | 77 | | | | | | |
| - | | | | :目: | Ms. | SS | SA 4 | 350 | 10 | 15 | - |
| -4 | | - sandy seams encountered near 3.8 m bgs | | | S | 33 | SA 5 | 400 | 11 | 17 | |
| | | | | | | | 0, (0 | 100 | '' | '' | |
| _ | 251.0 | | | | s | ss | SA 6 | 450 | 3 | 19 | |
| - 5- | 201.0 | End of borehole at 5.0 m bgs. | | | | | | | | | |
| - | | | | | | | | | | |] 1 |
| -6 | | | | | | | | | | | - |
| _ | | | | | | | | | | | - |
| -7 | | | | | | | | | | |]- |
| _ | | | | | | | | | | | - |
| -8 | | | | | | | | | | | |
| _ | | | | | | | | | | | |
| | | | | | | | | | | | |
| -9 | | | | | | | | | | |] |
| _ | | | | | | | | | | | 11 |
| -10 | | | | | | | | | | |] |
| - | | | | | | | | | | | |
| -11 | | | | | | | | | | | - |
| - | | | | | | | | | | | - |
| 12 | | | | | | | 044 | <u> </u> | FOEND | | |
| NOT | ES | | | | | \dashv | \boxtimes A | AS Aug | EGEND jer Samp | ole 🛮 | SS Split Spoon ST Shelby Tube |
| 1) B | orehole Lo | og interpretation requires assistance by EXP before u | | | | | | Rock C ER TE | ore (eg. STS | BQ, NQ | Q, etc.) VN Vane Sample |
| 2) N | o significa | og must be read in conjunction with EXP Report LOI int methane gas detected upon completion of drilling | n-∠10(| JO138- | AU. | | G S | | Gravity | | Consolidation D Consolidated Drained Triaxial |
| 3) by 4) G | eodetic el | s below ground surface. evation surveyed by using a SOKKIA GCX2 Receive , May 17, 2021: 1.10 m bgs (Elevation 255.01 m) | r. | | | | S Si | eve Ar | nalysis | Cl | U Consolidated Undrained Triaxial |
| ۷۱ (ن | alei ievei | , May 17, 2021: 1.10 m bgs (Elevation 255.01 m) July 20, 2021: 0.97 m bgs (Elevation 255.14 m) August 17, 2021: 1.12 m bgs (Elevation 254.99 m) | | | | | P Fi | | rmeability | y UC | U Unconsolidated Undrained Triaxial C Unconfined Compression |
| | | August 17, 2021. 1.12 III bgs (Elevation 254.99 m) | 1 | | | | | ab Perr ER LE | neability | DS | S Direct Shear |
| | | | | | | - 1 | | LK LE | | ▼ N4. | leasured Ā Artesian (see Notes) |

| 0.0 | |
|-----|----|
| ex | D. |
| 1 | 1 |

BH3/MW

| | | Г. ВО | KE | :пс | JL | _E | | O. | • | | Sheet 1 of 1 |
|------------------------------|--|---|---------------|------------------|-----|-------------|---|--|---|-----------------------------|---|
| CL | IENT | Auburn Developments Inc. | | | | | | | | _ PR | ROJECT NO. <u>LON-21008138-A0</u> |
| PR | ROJECT | Hunter Farm | | | | | | | | DA | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | : В | oring | Ma | y 12, 20 | 021 | Water Level August 17, 20 |
| ₽ | ELEVAT-OZ | | STRATA | W E L L | | | SAM | IPLES R | N | MO-STURE | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane |
| DEPTH | A T | STRATA | Î | Ł | ; | Ţ | N U M | RECOVERY | VALUE | J E | , 100 , 200 kPa |
| п | Ņ | DESCRIPTION | P Q T | L OG | É | T P E | NUMBER | Ě | | ET | Atterberg Limits and Moisture W _P W W _L |
| (m bgs) | (~m) 256.0 | | 우 | | | | K | - | (blows) | (%) | SPT N Value |
| -0 - | 255.8 | TOPSOIL - 280 mm | 7/1/2··7 | <i>i i</i> | | | | (, | (blows) | (70) | |
| - | | SAND - brown, fine to medium grained, trace to some silt, trace gravel, loose to compact, very | | | | | | | | | |
| -1 | | moist to wet | | | | SS | SA 1 | 150 | 5 | 14 | - |
| - | | | | | | | | | | | - |
| -2 | | | | | | SS | SA 2 | 400 | 8 | 24 | |
| - | | | | | | SS | SA 3 | 150 | 14 | 22 | - |
| -3 | | - some grey, stiff, clayey silt layering encountered | | | | 22 | SA 4 | 450 | 11 | 18 | - |
| - | | at 3.15 m bgs - becoming grey, compact and wet at 3.3 m bgs | | | | 00 | 0.7.4 | 130 | '' | | - |
| - 4 | | | | | | SS | SA 5 | 450 | 26 | 13 | |
| - | 251.3 | SANDY SILT - grey, trace gravel, compact, very | | | | SS | SA 6 | 450 | 19 | 15 | - |
| - 5 | | moist to wet | | | | | | | | | |
| - | 250.2 | | | | | SS | SA 7 | 450 | 23 | 22 | <u> </u> |
| -6 | | End of borehole at 5.8 m bgs. | | | | | | | | | - |
| - | | | | | | | | | | | - |
| -7 | | | | | | | | | | | - |
| - | | | | | | | | | | | - |
| -8 | | | | | | | | | | | - |
| - | | | | | | | | | | | |
| -9 | | | | | | | | | | | |
| _10 | | | | | | | | | | | |
| 10 - | | | | | | | | | | | |
| -11 | | | | | | | | | | | |
| - | | | | | | | | | | | |
| 12 | | | | | | | | | | | |
| NO | TES | | | | | | $\boxtimes A$ | AS Aug | EGEND Jer Samp | | SS Split Spoon ST Shelby Tube |
| 1) B 2) N 3) b 4) G | orehole La Borehole La Borehol | og interpretation requires assistance by EXP before og must be read in conjunction with EXP Report LOI ant methane gas detected upon completion of drilling is below ground surface. evation surveyed by using a SOKKIA GCX2 Receive 1, May 17, 2021: 1.28 m bgs (Elevation 254.79 m) July 20, 2021: 1.58 m bgs (Elevation 254.49 m) August 17, 2021: 1.70 m bgs (Elevation 254.37 m) | N-21Ó(er. | | | | OTHI G SI H H S Si Y UI P Fi K La | ER TE pecific ydrome eve Ar nit We eld Per ab Perr | Gravity eter alysis ight meability neability | C CI CI UI y U(| Q, etc.) |
| | | | | | | | | ER LE | | ▼ N4. | leasured 🚡 Artesian (see Notes) |

| 0.0 | |
|-----|--------------|
| -CX | \mathbf{n} |
| 0/1 | \sim |
| | |

BH4/MW

| | | | | | <i>_</i> _ | | | | • | | Sheet 1 of 1 |
|----------------|---------------------------|--|----------------|-------------|------------|----|--------|------------------|-------------------|-------------|---|
| CL | IENT | Auburn Developments Inc. | | | | | | | | PR | ROJECT NO. LON-21008138-A0 |
| PR | OJECT | Hunter Farm | | | | | | | | | ATUM Geodetic |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | В | oring | Ма | y 11, 20 |)21 | Water Level August 17, 202 |
| | | | Π_ | | | | | PLES | | | SHEAR STRENGTH |
| | ШЫР∀Т-О Z | | ST RATA | w | | | SAIVI | | | MO-SHURE | S Field Vane Test (#=Sensitivity) |
| DEPTH | V A | | <u>K</u> | W E L | | | N | RECOVERY | N | Į N Į Į | ▲ Penetrometer ■ Torvane |
| 뒵 | Ī | STRATA | Å | | Y | , | Ù | Ö | VALUE | Ρ̈́Ρ̈́ | 100 200 kPa |
| | N | DESCRIPTION | P | L OG | P | • | ZUEBER | Ě | | È' | Atterberg Limits and Moisture W _P W W _L |
| (m bgs) | (~m) | | P Q | G | | | R | Ŷ | | | ● SPT N Value × Dynamic Cone |
| -0 - | 256.0 | | | | | | | (mm) | (blows) | (%) | 10 20 30 40 |
| ٥ | 255.8 | TOPSOIL - 230 mm | XXX 7/7: 7/ | <i>B B</i> | | | | | | | |
| - | | FILL - SAND - brown/grey/black, trace silt, trace gravel, topsoil inclusions, building debris, loose, | \bowtie | | | | | | | | |
| -1 | | very moist | \bowtie | | | SS | SA 1 | 350 | 6 | 21 | |
| - | 254.4 | | \bowtie | Y | | | | | | | |
| | | SAND and GRAVEL - grey, trace silt, well | 60.000 | | | SS | SA 2 | 400 | 17 | 22 10 | |
| -2 | 253.9 | graded, compact, wet SAND - brown, some gravel, trace silt, compact, | | | | | | | | | |
| - | | wet | | | | ss | SA 3 | 450 | 25 | 14 | |
| -3 | | | | | 77 | | | | | | |
| | | | | | | SS | SA 4 | 450 | 13 | 21 | • 0 |
| | | | | | | | | | | | |
| - 4 | | | | ŀ∄: | | | | | | | |
| - | | | | [:目: | 77 | | | | | | |
| -5 | 251.0 | | | | | SS | SA 5 | 300 | 10 | 16 | <u> </u> |
| ļ | | End of borehole at 5.0 m bgs. | | | | | | | | | |
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| 4.0 | | | | | | | | | | | |
| 1/2 | | | | | | _ | | | EGEND Jer Samp | ole 🕏 | SS Split Spoon ST Shelby Tube |
| 1) B | | og interpretation requires assistance by EXP before ι | ise hv | othere | | | | | ore (eg. | | |
| В | orehole Lo | og must be read in conjunction with EXP Report LON | N-2100 | 08138- | A0. | | | ER TE | STS Gravity | <u> </u> | Consolidation |
| ∠) N 3) b | o significa gs denotes | Int methane gas detected upon completion of drilling below ground surface. evation surveyed by using a SOKKIA GCX2 Receive | - | | | | HH | /drome | eter | CI | D Consolidated Drained Triaxial |
| 4) G 5) W | eodetic el /ater level | , May 17, 2021: 1.52 m bgs (Elevation 254.59 m) | r. | | | | | eve An nit We | | | U Consolidated Undrained Triaxial U Unconsolidated Undrained Triaxial |
| , | | July 20, 2021: 1.38 m bgs (Elevation 254.73 m) ugust 17, 2021: 1.51 m bgs (Elevation 254.60 m) | | | | | P Fi | eld Pei | rmeability | y UC | C Unconfined Compression |
| | | agast, 2021. 1.01 III bgs (Elevation 204.00 III) | | | | | | ıb Perr ER LE | neability VFLS | DS | S Direct Shear |
| | | | | | | | | ∟r ∟∟ ∖ppare | | ▼ Me | leasured 🛕 Artesian (see Notes) |

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Sheet 1 of 1

Auburn Developments Inc. CLIENT PROJECT NO. **LON-21008138-A0** PROJECT Hunter Farm DATUM <u>Geodetic</u> LOCATION Marion Street, Dorchester, ON DATES: Boring May 12, 2021 Water Level August 17, 2021 **SHEAR STRENGTH SAMPLES** STRATA M CONTENT S Field Vane Test (#=Sensitivity) Ä DEPTH ISTURE RECOVERY ▲ Penetrometer ■ Torvane Ν A Ł NUMBER **VALUE STRATA** T P E **Atterberg Limits and Moisture DESCRIPTION** PLOT WP W WL (~m) × Dynamic Cone SPT N Value (mm) 257.6 (blows) 20 40 10 -0 257.4 TOPSOIL - 280 mm CLAYEY SILT - grey, trace sand, trace gravel, firm moist SS SA 1 450 6 256.3 SANDY SILT - grey, some gravel, compact, SA₂ 450 5 -2 255.1 SS SA₃ 400 13 SAND - grey, fine to medium grained, some silt to silty, compact, wet -3 SA4 400 SS 31 254.2 -some silt layering encountered at 3.3 m bgs SILT TILL - grey, some sand to sandy, trace gravel, dense to very dense, moist 4 SS SA 5 450 38 SS SA 6 450 50* 252.6 End of borehole at 5.0 m bgs. -6 -8 9 10 SAMPLE LEGEND ☑ AS Auger Sample ☑ SS Split Spoon ST Shelby Tube Rock Core (eg. BQ, NQ, etc.) VN Vane Sample Borehole Log interpretation requires assistance by EXP before use by others. Borehole Log must be read in conjunction with EXP Report LON-21008138-A0.
 No significant methane gas detected upon completion of drilling. OTHER TESTS G Specific Gravity C Consolidation bgs denotes below ground surface. CD Consolidated Drained Triaxial H Hydrometer 5) bgs deribtes below ground surface.
4) * denotes 50 blows per less than 150 mm split spoon sampler penetration.
5) Geodetic elevation surveyed by using a SOKKIA GCX2 Receiver.
6) Water level, May 17, 2021: 0.90 m bgs (Elevation 256.87 m)
July 20, 2021: 0.81 m bgs (Elevation 256.96 m)
August 17, 2021: 0.95 m bgs (Elevation 256.82 m) S Sieve Analysis CU Consolidated Undrained Triaxial Y Unit Weight **UU Unconsolidated Undrained Triaxial** P Field Permeability **UC Unconfined Compression DS Direct Shear** K Lab Permeability WATER LEVELS Measured Artesian (see Notes)

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Sheet 1 of 1

Auburn Developments Inc. CLIENT PROJECT NO. **LON-21008138-A0** PROJECT Hunter Farm DATUM Geodetic **DATES: Boring** May 11, 2021 LOCATION Marion Street, Dorchester, ON Water Level August 17, 2021 **SHEAR STRENGTH** SAMPLES STRATA M CONTENT S Field Vane Test (#=Sensitivity) DEPTH ISTURE RECOVERY **▲** Penetrometer ■ Torvane Ν Ą Ł NUMBER **VALUE STRATA** T P E **DESCRIPTION Atterberg Limits and Moisture** PLOT W_P W W_L (~m) **SPT N Value** × Dynamic Cone (mm) (%) 268.1 (blows) 10 20 40 -0 267.9 TOPSOIL - 150 mm SILTY SAND - brown, trace gravel, loose, very SS SA 1 300 6 11 266.7 SILT - brown, some sand, trace gravel, dilatent, sand laminations, compact, moist to very moist SS SA₂ 300 13 16 -2 265.9 CLAYEY SILT - brown, trace to some sand, trace gravel, sand laminations, moist to very SS SA3 50 28 15 moist, very stiff to dense -3 -some very moist silt layering encountered at 2.9 SA4 400 SS 18 15 4 SS SA₅ 400 23 17 263.6 SANDY SILT - brown, trace gravel, moist, moist SS SA₆ 450 16 14 -5 262.5 SAND - brown, fine to medium grained, trace silt, trace gravel, loose, moist -6 SS SA 7 400 9 7 -some silt layering encountered at 7.8 m bgs 260.2 8 7 SA8 SS 450 8 CLAYEY SILT - brown, trace sand, trace gravel, stiff, moist 259.5 SAND - brown, fine to medium grained, trace to some silt, trace gravel, compact, moist -9 SA9 SS 400 6 12 257.9 CLAYEY SILT - grey, trace sand, trac gravel, soft, very stiff, very moist to wet SS SA 10 400 19 13 -11 256.9 End of borehole at 11.1 m bgs. SAMPLE LEGEND ☑ AS Auger Sample ☑ SS Split Spoon ST Shelby Tube **NOTES** Rock Core (eg. BQ, NQ, etc.) VN Vane Sample 1) Borehole Log interpretation requires assistance by EXP before use by others. Borehole Log must be read in conjunction with EXP Report LON-21008138-A0. OTHER TESTS No significant methane gas detected upon completion of drilling. G Specific Gravity C Consolidation No significant methale gas detected upon completion of anims.
 bgs denotes below ground surface.
 Geodetic elevation surveyed by using a SOKKIA GCX2 Receiver.
 Water level, May 17, 2021: 9.27 m bgs (Elevation 258.87 m)

 July 20, 2021: 9.53 m bgs (Elevation 258.61 m)
 August 17, 2021: 9.55 m bgs (Elevation 258.59 m)

 CD Consolidated Drained Triaxial H Hydrometer S Sieve Analysis CU Consolidated Undrained Triaxial Y Unit Weight **UU Unconsolidated Undrained Triaxial** P Field Permeability **UC Unconfined Compression DS Direct Shear** K Lab Permeability WATER LEVELS Measured Artesian (see Notes)

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| CL | ENT | Auburn Developments Inc. | | | | | | | PR | ROJECT NO. <u>LON-21008138-A0</u> |
| PR | OJECT | Hunter Farm | | | | | | | DA | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Boring | <u> Ma</u> | ay 11, 20 | 021 | Water Level August 17, 20 |
| _ | E L E | | S | w | | SAI | /PLES | ; | M C | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) |
| DEP PTH | M-M>40z | STRATA | S R A T A | W E L | Ţ | NU | RECOVERY | N VALUE | MO-STURE | ▲ Penetrometer ■ Torvane 100 200 kPa |
| | | DESCRIPTION | P Q | L O G | T P E | | E R Y | | RT | Atterberg Limits and Moisture W _P W W _L |
| bgs) | (~m) 264.3 | | " | | | | (mm) | (blows) | (%) | ● SPT N Value X Dynamic Cone 10 20 30 40 |
| ۲° | 264.0 | TOPSOIL - 300 mm | 7 <u>/ /</u> · · 7 | | | | | | | |
| 1 | | SANDY SILT - brown, trace gravel, loose to compact, very moist | | | // ss | S SA 1 | 50 | 5 | 24 | - |
| | 262.9 | SILT - grey, trace to some sand, trace gravel, dilatent. loose, wet | <u> </u> | _ ¥ | | S SA 2 | 400 | 7 | 20 | - |
| 2 | | | | | 22 22 | | | | | |
| 3 | 261.4 | CLAYEY SILT - grey, trace sand, trace gravel, | | | 22 22 | S SA 3 | | 10 | 18 | |
| | | saturated silt lamination, stiff, moist | | | SS | S SA 4 | 450 | 14 | 19 | - |
| 1 | 260.3 | SILT - grey, trace sand, trace gravel, dilatent, loose, wet | | | | | | | | |
| 5 | 258.7 | | | | S | S SA 5 | 400 | 11 | 20 | |
| 5 | 200.1 | SILT TILL - grey, some sand, trace gravel, saturated sand lamination, thin clay laminations, compact, moist | | | S | S SA 6 | 400 | 27 | 9 | |
| 7 | | | | | | | | | | |
| 3 | 256.2 | End of how hall and Od on how | | | ss | SA 7 | 450 | 29 | 10 | φ |
| | | End of borehole at 8.1 m bgs. | | | | | | | | |
| | | | | | | | | | | - |
| 0 | | | | | | | | | | _ |
| | | | | | | | | | | - |
| 11 | | | | | | | | | | |
| ا 1 | | | | | | | | <u></u> | | |
|) Bo Bo) No) bo) G | orehole Lo o significa gs denotes eodetic el | og interpretation requires assistance by EXP before by must be read in conjunction with EXP Report LC ant methane gas detected upon completion of drilling is below ground surface. evation surveyed by using a SOKKIA GCX2 Receive, May 17, 2021: 0.64 m bgs (Elevation 263.69 m) |)N-2100 g. ⁄er. | others 08138- | i. A0. | OTH GS HH SS | AS Aug Rock C IER TE | Gravity eter nalysis | BQ, NG C CI Cl | ST Shelby Tube Q, etc.) ST Shelby Tube VN Vane Sample Consolidation Consolidated Drained Triaxial U Consolidated Undrained Triaxial U Unconsolidated Undrained Triaxial |
| | А | Úly 20, 2021: 1.07 m bgs (Elevation 263.26 m) ugust 17, 2021: 1.35 m bgs (Elevation 262.98 m) |) | | | P F K L WA | ield Pe | rmeability meability VELS | y UG | C Unconfined Compression S Direct Shear Artesian (see Notes) |

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| IENT | Auburn Developments Inc. | | | | | | | PF | ROJECT NO. I | _ON-21008138-A0 |
| OJECT | Hunter Farm | | | | | | | | ATUM Geodeti | |
| | N Marion Street, Dorchester, ON | | DAT | FS: F | Borina | Ma | y 11, 20 | | · | r Level August 1 |
| | Wallon Street, Dorchester, Or | | T | | | | | | | |
| ELEVAT | STRATA | ST R A T A | W E L L | ı | | RECOVERY | N VALUE | MO-STURE | | STRENGTH Test (#=Sensitivity ■ Torvane 200 kPa |
| ON N | DESCRIPTION | P | | T Y P E | M B | Ĭ | | ĔŤ | Atterberg Lim | nits and Moisture |
| N | | [| LOG | E | NUMBER | Ŗ | | - | W _P | w w _L |
| (~m) | | ¥ | | | '` | - | | | SPT N Value | × Dynamic Cone |
| 264.3 | | | | | | (mm) | (blows) | (%) | 10 20 | 30 40 |
| 264.0 | TOPSOIL - 300 mm | 7/1/2. 7 | | | | | | | | +++++++ |
| | SANDY SILT - brown, trace gravel, loose to compact, very moist | | | | | | | | | |
| 262.9 | | | | | | | | | | |
| | SILT - grey, trace to some sand, trace gravel, dilatent, loose, wet | | | | | | | | | |
| 261.4 | | | | | | | | | | |
| 201.4 | CLAYEY SILT - grey, trace sand, trace gravel, | 1 | : <u> </u> : | | | | | | | |
| | saturated silt lamination, stiff, moist | | | | | | | | | |
| 260.2 | | 1/1/2 | | | | | | | | |
| | SILT - grey, trace sand, trace gravel, dilatent, loose, wet | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| 258.7 | SILT TILL grove come conditions are series | 02:12 | 1 | | | | | | | |
| | SILT TILL - grey, some sand, trace gravel, saturated sand lamination, thin clay laminations, | | | | | | | | | |
| | compact, moist | | | | | | | | | |
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| | | 1913 | | | | | | | | |
| 256.2 | | | | | | | | | | |
| | End of borehole at 8.1 m bgs. | 10/2012 | 1 | | | | | | T | |
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| | • | | | | SAM | PLE LI | EGEND | | | |
| <u>ES</u> | | | _ | | | | ger Samp ore (eg. | | SS Split Spoon | ST Shelby TubVN Vane Samp |
| | Log interpretation requires assistance by EXP before Log must be read in conjunction with EXP Report L0 | | | | | ER TE | , 0 | DQ, 140 | x, 0.0. <i>j</i> | w viv valie Gallip |
| o signific | cant methane gas detected upon completion of drillir | איב וטנ ig. | JU 130- | AU. | GS | pecific | Gravity | | Consolidation | nad Triavis! |
| eodetic e | es below ground surface. elevation surveyed by using a SOKKIA GCX2 Receiv | /er. | | | | ydrome eve Ar | | | D Consolidated Drai U Consolidated Und | |
| ater leve | el, May 17, 2021: 0.57 m bgs (Elevation 263.75 m) July 20, 2021: 1.10 m bgs (Elevation 263.22 m | | | | γ υ | nit We | ight | Ū | U Unconsolidated U | ndrained Triaxial |
| | August 17, 2021: 1.39 m bgs (Elevation 262.93 m) | , | | | | | rmeability neability | | C Unconfined Comp S Direct Shear | pression |
| | | | | | WAT | ER LE | VELS | | _ | |
| | | | | | I \(\subseteq \) | Appare | nt | ▼ M | leasured 本 | Artesian (see Note |

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|-----------------|---------------------------|--|--------------|--------------|----------|----|-------------|----------|----------------------|----------------|--|
| CL | IENT | Auburn Developments Inc. | | | | | | | | PR | ROJECT NO. <u>LON-21008138-A0</u> |
| PR | OJECT | Hunter Farm | | | | | | | | DA | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | В | oring | Ma | ıy 11, 20 | 021 | Water Level August 17, 202 |
| D | МТМ | | STRATA | w | | | SAM | IPLES | | MO-STURE | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) |
| DEPTH | A A | STRATA | À | W E L | ١, | - | N | RECOVERY | N VALUE | s T T E | ▲ Penetrometer ■ Torvane 100 200 kPa |
| H | 4T-0Z | DESCRIPTION | | | I Y | | ZUEBEC | V V | | U N E T | Atterberg Limits and Moisture |
| | | | P Q | LOG | E | | E | Ŕ | | | W _P W W _L |
| (m bgs) | (~m) 257.5 | | T | | | | | (mm) | (blows) | (%) | ● SPT N Value × Dynamic Cone 10 20 30 40 |
| 0 - | 257.3 | TOPSOIL - 250 mm | <u> </u> | <i>D E</i> | П | | | | | | |
| - | 256.7 | CLAYEY SILT - brown, some sand to sandy, trace gravel, stiff, moist | } } | \mathbf{Y} | 77 | | | | | | - |
| -1 | | SILT TILL - brown, trace sand, trace gravel, compact, moist to wet | | | | SS | SA 1 | 450 | 21 | 11 | |
| - | | -some sand layering encountered at 1.2 m bgs | | | | | | | | | |
| -2 | 055.0 | | | | | SS | SA 2 | 450 | 18 | 10 | |
| - | 255.2 | SAND - brown, some silt chunks, trace gravel, | d' hd' | | | SS | SA 3 | 350 | 17 | 9 | |
| -3 | 254.6 | compact, wet | ටන්. 12 | | M | | 0, (0 | | | | |
| ٥ | | SILT TILL - brown, some sand to sand, trace gravel, thin wet sand laminations, compact, very | | [] | | ss | SA 4 | 350 | 28 | 13 | 0 • |
| | | moist to wet | | [:目: | | | | | | | |
| - 4 | | | | | | SS | SA 5 | 350 | 41 | 14 | |
| - | | - becoming grey and dense at 4.4 m bgs | | | | - | SA 6 | 450 | 45 | 10 | |
| - 5- | 252.5 | End of borehole at 5.0 m bgs. | J. | | 4 | 33 | 5A 0 | 450 | 45 | 10 | |
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| | | | | | | | | | | | 11 |
| 12 | | | | | | | | | EGEND | | SS Split Spoon Type |
| 1) B | | og interpretation requires assistance by EXP before | ise hv | others | | | □ F | Rock Č | ger Samp ore (eg. | ле ഥ BQ, NQ | SS Split Spoon ST Shelby Tube VN Vane Sample |
| ÉВ | orehole L | og must be read in conjunction with EXP Report LOI int methane gas detected upon completion of drilling | N-21Ó0 | | | | | ER TE | STS Gravity | С | Consolidation |
| 3) bo | gs denote: leodetic el | s below ground surface. evation surveved by using a SOKKIA GCX2 Receive | | | | | HH | ydrome | | CI | D Consolidated Drained Triaxial U Consolidated Undrained Triaxial |
| 5) W | /ater level | , May 17, 2021: 0.62 m bgs (Elevation 257.03 m) July 20, 2021: 0.56 m bgs (Elevation 257.09 m) | - | | | | γ Uι | nit We | | UL | U Unconsolidated Undrained Triaxial C Unconfined Compression |
| | А | ugust 17, 2021: 0.70 m bgs (Elevation 256.95 m) | | | | | K La | b Perr | neability | | S Direct Shear |
| | | | | | | | | ER LE | | ▼ N4. | leasured T Artesian (see Notes) |

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|-----------------------|--|--|------------------|-------------|------------------|---------|-----------------|-------------------|-------------------|---|--|
| CL | IENT | Auburn Developments Inc. | | | | | | | PR | ROJECT NO. <u>LON-21008138-A0</u> | |
| PR | OJECT | Hunter Farm | | | | | | | DA | ATUM <u>Geodetic</u> | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Borin | g <u>Ma</u> | ay 11, 20 | 021 | Water Level August 17, 202 | |
| D | ELEVAT-OZ | | STRATA | Ψ | | SAI | MPLES | | MO-STURE | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane | |
| DEPTH | Å | STRATA | A A | W E L | Ţ | N | RECOVERY | N VALUE | S T T E U N | 100 , 200 kPa | |
| н | o N | DESCRIPTION | P L O T | LOG | T Y P E | NUM BER | V E R | | RT | Atterberg Limits and Moisture W _P W W _L | |
| (m bgs) | (~m) 266.1 | | 우 | | | K | | (blows) | (%) | ● SPT N Value × Dynamic Cone 10 20 30 40 | |
| -0- | 265.8 | TOPSOIL - 300 mm | 7/1/×. ·7/ | 4 6 | | + | () | (Siewe) | (/// | | |
| - | | SILTY SAND - brown, trace gravel, dense, moist | 1,1 | | 77 | | | | | - | |
| -1 | 264.8 | | | | s | S SA | 1 300 | 30 | 11 | | |
| - | | SAND - fine to medium grained, brown, trace to some silt, trace gravel, loose to compact, wet | | ¥ | s | S SA 2 | 2 250 | 8 | 20 | - | |
| - 2 | | | | | | S SA S | 3 450 | 8 | 26 | | |
| -3 | | | | | | S SA | 430 | 0 | 20 | | |
| - | | | | | S | SA 4 | 4 400 | 12 | 24 | - | |
| - 4 | | - becoming grey near 4.0 m bgs | | | | | | | | | |
| - | 004.4 | | | | S | S SA ! | 5 400 | 13 | 22 | - | |
| - 5- | 261.1 | End of borehole at 5.0 m bgs. | | | | - | - 100 | | | } | |
| - | | - | | | | | | | | | |
| -6 | | | | | | | | | | | |
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| | | | | | | | | | | 1 | |
| 12 | | | | | | | | EGEND ger Samp | | SS Split Spoon ST Shelby Tube | |
| 2) N 3) bo 4) G | 1) Borehole Log interpretation requires assistance by EXP before use by others. Borehole Log must be read in conjunction with EXP Report LON-21008138-A0. 2) No significant methane gas detected upon completion of drilling. 3) bgs denotes below ground surface. 4) Geodetic elevation surveyed by using a SOKKIA GCX2 Receiver. 5) Water level, May 17, 2021: 1.40 m bgs (Elevation 264.84 m) July 20, 2021: 1.40 m bgs (Elevation 264.81 m) August 17, 2021: 1.61 m bgs (Elevation 264.60 m) August 17, 2021: 1.61 m bgs (Elevation 264.60 m) Rock Core (eg. BQ, NQ, etc.) OTHER TESTS G Specific Gravity H Hydrometer S Sieve Analysis V Unit Weight P Field Permeability K Lab Permeability K Lab Permeability WATER LEVELS ✓ Apparent ✓ Measured Ā Artesian (see Notes) | | | | | | | | | | |

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| PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | | | |
|---|------------------|---|--|--------|--------------|--|------------------|-------------------|--|---------------|--|--------|---------------|-----------------|---------------|----------------|-----------|---------------|--------------|--------------------|--------------------|
| CLIENT Auburn Developments Inc. | | | | | | | | | | | | | | | | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Excava | ation _ | May 12 | 2, 2021 | | | | _ ۷ | Vate | er L | Leve | el . | | | | |
| | Ę | | s | | | SAN | IPLES | | B SHEAR STRENGTH U S Field Vane Test (#=Sensitivity) | | | | | | | | | | | | |
| ₽ | шш | | STRAT | WELL | | | R | N | Ľ | | | | eld V tron | | | | | Sensi vane | | ty) | |
| ОШР⊢Н | 4 T-02 | STRATA | Î | Ł | Ţ | Ņ | Ö | VALUE | ₽ | , 40 , 80 ķPa | | | | | | | | | | | |
| Н | ÖN | DESCRIPTION | l P | LOG | T P E | NUMBER | RECOVERY | (blows) or | DE NSI | | Α | tter | berg | | | ts ar V | | /loist | ure | | |
| (\ | (m) | | 卢 | G | | R | (mm) | RQD (%) | | ١. |) SI | рт і | N Va | - ⊩ | | >— | ┪ ̄ | mic | Cor | 16 | |
| (m) -0 - | 254.9 | T0000H 500 | 17. 18. 12 | | <u> </u> | | or (%) | 1 | (kN/m3) | | - | 10 | | 20 | | | 30 | 4 | | .• ' | ot |
| L | | TOPSOIL - 500 mm | 1/. 3/./ | | | | | | | Ħ | | | | | # | # | Ш | # | Ш | | 1] |
| L | 054.4 | | 7. 1. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. | | | | | | | Ħ | Ħ | | Ш | \dagger | \sharp | # | Ш | # | Ш | | <u> </u> |
| _ | 254.4 | MARL - mixed peat, light grey, wet | 17. 17. 19. 19. 19. 19. 19. 19. 19. 19. 19. 19 | | \forall | | | | | H | | | | | \pm | \pm | Ш | # | Ш | | ┨. |
| | | | <u> </u> | | GE | 3 SA 1 | | | | H | Ш | Ħ | Ш | \pm | \pm | \pm | Ш | Ш | Ш | Ħ | þ 134 |
| -1 | | | 7 7 7 | | \Box | | | | | H | Н | | Ш | | \pm | \pm | Ш | \pm | Ш | | |
| ' | | | <u> </u> | | | | | | | H | \coprod | ∄ | \coprod | $\pm \parallel$ | \pm | + | \coprod | # | \coprod | \coprod |] |
| | | | 1, 11, | | | | | | | | + | | H | + | ${\mathbb H}$ | + | Н | + | \mathbb{H} | + | $\left\{ \ ight]$ |
| | | | 77 7 | | | | | | | H | | | Н | | ${\mathbb H}$ | \mp | Н | | П | | 17 |
| - | | | 77 77 | | | | | | | H | H | H | H | H | Ħ | # | H | \mp | H | H | 11 |
| | 252.9 | | 1/ 1/ | | | | | | | H | H | H | H | Ħ | # | # | Ħ | # | H | Ħ | 11 |
| -2 | 202.9 | SAND and GRAVEL -grey, alluvial, loose, wet | 0.000 | | abla | | | | | Ħ | Ħ | | Ш | Ħ | # | # | Щ | # | Ш | | 11 |
| - | | | 0.00 | | X GE | SA 2 | | | | Ħ | | c | | | # | # | Ш | # | Ш | | 11 |
| - | | | 0.0.0 | | \Box | | | | | H | Ш | | Ш | | \pm | \pm | Ш | \pm | Ш | | 1 1 |
| _ | | | 0.0.0 0.0.0 | | | | | | | H | H | | | | \pm | \pm | Ш | | Ш | | 1 1 |
| - | | | 0 0 0 | | | | | | | H | H | | | | \pm | \pm | Ш | \pm | Ш | + | - |
| -3 | 251.9 | SAND - brown/grey, fine to medium grained, | ه م | | | | | | | H | $^{+}$ | | | \pm | \pm | \pm | Ш | | Ш | | ┨┤ |
| - | 251.6 | loose, wet | | | X GE | 3 SA 3 | | | | H | + | | | φ | ${\mathbb H}$ | + | Н | + | \mathbb{H} | + | |
| - | | End of test pit at 3.3 m bgs. | | | | | | | | | | | | | | | | | | | - |
| - | | | | | | | | | | | | | | | | | | | | | |
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| -5- | | | | | | | | | | | | | | | | | | | | | |
| NO | TES . | | | | | | | EGEND jer Samp | ole 🛭 | s | S S | plit : | Spoo | on | ı | . ; | ST S | Shelb | y Tu | ıbe | |
| 1) T | est pit inte | erpretation requires assistance by EXP before use | by others | . Test | pit log | , 🗆 F | Rock C | ore (eg. | | | | • | | | | | | /ane | | | ٠ |
| 2) T | est pit is b | ad in conjunction with EXP Report LON-21008138 assed on observations of the excavator resistance. | | | _4: | OTHER TESTS G Specific Gravity C Consolidation H Hydrometer CD Consolidated Drained Triaxial | | | | | | | | | | | | | | | |
| 4) b | gs denote | red and water observed near 2.0 m bgs upon comp s below ground surface. | | excav | ation. | S Si | eve Ar | nalysis | CI | U C | cons | solic | dated | d Un | ıdrai | ined | d Tria | axial | | | |
| 5) G | eodelic el | evations surveyed using a SOKKIA GCX2 Receive | Π. | | | P Fi | nit We eld Pe | rmeability | y U | Сί | Jnco | onfir | ned (| Com | | drain essic | | Triaxi | al | | |
| | | | | | | | ab Perr ER LE | neability | D | SE |)irec | t SI | hear | | | | | | | | |
| | | | | | | | \ppare | | ▼ M | eas | sure | d | | Ā | | Arte | siar | ı (see | e No | tes) | |

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TP1A

| PR | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | |
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| CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | | |
| | | Marion Street, Dorchester, ON | | DAT | ES: | Excava | ation _ | May 12 | 2, 2021 | | | | W | /ate | r L | eve | Ι_ | | | |
| | Ę | | s | | | SAN | IPLES | | В | | | | | | | REN | | | | |
| Ē | шш | | STRATA | W | | | R | N | Į Ķ | ♣ S Field Vane Test (#=Sensitive A Penetrometer ■ Torvane | | | | | | | | vity) | | |
| DEPTH | | STRATA | 🚡 | WELL | Ţ | Ŋ | RECOVERY | VALUE | ₽ | | 40 , 80 kPa | | | | | | | | | |
| Ĥ | 4T-02 | DESCRIPTION | P | LOG | T P E | NUMBER | ¥ E R | (blows) or | DE NS- | | At | terk | | | | | | oistu | re | |
| | (m) | | Ļ | Ğ | - | Ŕ | Ý (mm) | RQD (%) | ¦ | | e D | T N | Val | - ⊢ | —≎ | W | _ | nic C | ono | |
| (m) -0 - | 255.2 | | | | | | or (%) | 1 | (kN/m3) | | | 10 | Vai | 20 | <u>, </u> | 30 | | 40 | one — | \perp |
| - | | TOPSOIL - 300 mm | 7 | | | | | | | Ш | \pm | ╁ | † | Ħ | | Ш | | | | ∄. |
| L | 254.9 | MARL - mixed peat, light grey, wet | 717 7 | | \forall | | | | | Н | + | + | $^{+}$ | $^{+}$ | | Н | | | | ┨. |
| | | | 1, 11, | | GI | B SA 1 | | | | Н | + | + | + | ${\mathbb H}$ | | ${\mathbb H}$ | + | Ш | + | Н |
| _ | | | 71 V | | \triangle | | | | | H | \blacksquare | \blacksquare | H | H | | H | | | | \mathbb{H}^{-} |
| - | | | <u> </u> | | | | | | | Ħ | \parallel | \parallel | Ħ | $oxed{\dagger}$ | | # | | | | |
| -1 | | | 1/2 1/2 | | | | | | | Ħ | \parallel | \sharp | \dagger | Ħ | | # | | Ш | | − |
| - | | | 71/7 | | | | | | | Ш | \parallel | \parallel | Ħ | Ħ | | Ш | | | | ╽- |
| - | | | <u> </u> | | | | | | | Ш | Ш | ╽ | Ш | Ш | | Ш | | Ш | | ╽- |
| - | | | 7 7 7 7 7 7 | | | | | | | Н | \pm | + | $^{+}$ | $^{+}$ | | Ш | | | | Ӈ- |
| - | | | 71/7 | | | | | | | H | + | + | + | + | | H | | | | H - |
| -2 | 253.2 | SAND - brown/grey, fine to medium grained, | 1, | | Н | | | | | H | \blacksquare | \mathbb{H} | H | H | | H | H | | | - |
| - | | loose, wet | | | $\left\ \cdot \right\ _{G}$ | B SA 2 | | | | H | \blacksquare | Ħ | Ħ | Ħ | | Ħ | | | | - |
| _ | | | | | \mathbb{N} | | | | | П | \parallel | \parallel | Ħ | Ħ | | # | | | | |
| _ | | | | | | | | | | Ш | \parallel | Ħ | Ħ | Ħ | | \sharp | | | | ╽. |
| _ | | | | | | | | | | H | \pm | \pm | † | \parallel | | \parallel | | Ш | | ╽. |
| -3 | 252.2 | | | | | | | | | Ш | | | \parallel | H | | Ш | | | | |
| Ĺ | | End of test pit at 3.0 m bgs. | | | | | | | | | | | | | | | | | | |
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| 5 | | | | | | SAM | | EGEND | <u> </u> | <u> </u> | | | | | | | | | | |
| NO | TES | | | | | $\neg \boxtimes A$ | AS Aug | ger Samp | | | | lit S | роо | n | | | | nelby ane S | | |
| 'n | nust be re | erpretation requires assistance by EXP before use land in conjunction with EXP Report LON-21008138 | by others -A0. | . Test | pit lo | g oth | ER TE | | | | | | | | L | ⊒ VI | IN Võ | ai ie 3 | amp | C |
| 2) T 3) V | est pit is b /ater obse | pased on observations of the excavator resistance. Erved near 2.5 m bgs upon completion of excavation | | | | HH | ydrome | | | Cor D Co | | | | Dra | ine | d Tri | axia | l | | |
| 4) b | gs denote | s below ground surface. evations surveyed using a SOKKIA GCX2 Receive | | | | S Si | , eve Ar nit We | nalysis | CI | U C | onso | olida | ated | Und | draiı | ned [·] | Tria | | | |
| , - | | , 0 | | | | P Fi | eld Pe | rmeability neability | y U | | ncor | nfine | ed C | | | ssior | | , and | | |
| | | | | | | WAT | ER LE | VELS | | | | | cal | | | | | | | |
| | | | | | | | | nt | ▼ M | eası | ured | l | | Ā | Α | ۱rtes | ian | (see l | Notes | s) |

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TP2

| PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | | |
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| | - | Auburn Developments Inc. | | | | | | | | | JM | | | | | 14-2 | 100 | 013 | <i>)-</i> — | |
| | | Marion Street, Dorchester, ON | | DAT | ES: E | Excava | ation _ | May 12 | | | | | | | | eve | :I _ | | | |
| | E | | Т. | | | | IPLES | | В | Π | SHEAR STRENGTH | | | | | | | | | |
| | ╙┸╙╱⋖┴─ | STRATA | ST RA T | W E L | Ţ | | RECOVERY | N VALUE | K | • | S I Pe | Fiel netr | d Va | eter | r | | Γorv | ensit ⁄ane 80 ķl | | y) |
| H | -ON | DESCRIPTION | A P | | T Y P E | NUMBER | ¥ | (blows) | DE NS- | ┢ | At | terb | erg | 40 Lir | | s an | | oistu | | \dashv |
| | | | ļ | L O G | E | Ē | | or RQD | S I | | | | | WP | , W | / W | L_ | | | |
| (m) -0 - | (m) 256.7 | | | | | | (mm) or (%) | (%) | Ť Y (kN/m3) | | | | | | | | | | | 9 |
| - | 256.5 | TOPSOIL - 250 mm | 17 · 11·19 | | | | | | | L | Ш | \parallel | | | | | | Ш | Н | Ш. |
| _ | 256.2 | SAND , brown, weathered, some silt to silty, loose, very moist | | | GE | SA 1 | | | | Ħ | | \parallel | | | | | \dagger | | H | \ |
| <u> </u> | | SILT TILL - brown/grey, trace gravel, compact, moist | | | | SA 2 | | | | | | | | | | | | | H | |
| - | | | | | | 5A 2 | | | | Ħ | | \parallel | | | | | \parallel | | H | |
| -1 | | | | | | | | | | Ħ | | | | | | | | | Ħ | Ш- |
| - | | | | | | | | | | Ħ | | | | | | | | Ш | | Ш |
| - | | | | | | | | | | Ħ | | Ш | | Ш | | | | Ш | Ш | Ш. |
| - | | | | | | | | | | H | | | | | | | | | \mathbf{H} | ╽ |
| - | | | | | | | | | | H | | | | | | | | | + | H - |
| -2 | | becoming grow poor 2.0 m has | | | | | | | | H | H | H | H | H | | | | Ш | H | Щ- |
| - | | - becoming grey near 2.0 m bgs | | | | | | | | Ħ | | | | | | | | | | Щ. |
| _ | | | | | | | | | | Ħ | Ш | | | Ħ | | | | Ш | Ħ | Ш. |
| | | | | | | | | | | Н | | | | | | | | Ш | Н | Ш. |
| | | | | | | | | | | H | \mathbb{H} | + | + | $^{+}$ | | | + | Н | $^{+}$ | Н |
| _ | | | | | | | | | | H | H | H | H | H | | | | Н | H | H. |
| -3 | | | | | | | | | | Ħ | H | \blacksquare | H | H | | | | | Ħ | П |
| - | | | | | | | | | | Ħ | | | | | | | | Ш | Ħ | Ш. |
| | 253.2 | | | | | | | | | H | | | | | | | | | | Ш |
| ŀ | | End of test pit at 3.5 m bgs. | | | | | | | | | | | | | | | | | | |
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| 5 | | | - | | | | | EGEND ger Samp | | 00 | S Sp | lit C | noc | n | | | T 91 | helby | Tul | <u> </u> |
| <u>NO1</u> | | erpretation requires assistance by EXP before use b | v others | s Test | nit Ioo | _ □ F | Rock Č | ore (eg. | | | | iii 3 | μου | | | | | ane S | | |
| ĺ'n | nust be re | ad in conjunction with EXP Report LON-21008138- based on observations of the excavator resistance. | A0. | . 100l | pit 10g | IOIH | ER TE | STS Gravity | С | Coı | nsoli | datio | on | | | | | | | |
| 3) T | est pit ope | en and dry upon completion of excavation. s below ground surface. | | | | HH | ydrome eve Ar | eter | CI | D C | onso | olida | ated | | | | iaxia Tria | | | |
| 5) G | eodetic el | evations surveyed using a SOKKIA GCX2 Receiver | - | | | γ υ | nit We | ight | Ul | U U | ncor | nsoli | idate | ed L | Jnd | rain | ed T | riaxia | ıl | |
| | | | | | | KLa | eid Per ab Perr | rmeability neability | y U(| | ncor rect | | | om | pre | SSIO | 11 | | | |
| | | | | | | | ER LE Appare | | ▼ Me | eas | ured | | | Ā | Þ | \rtes | sian | (see | Not | es) |

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TP3

| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | |
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| | - | Hunter Farm | | | | | | | | | | | | | -210 | 0813 | 3-A0 | _ | | |
| | | Auburn Developments Inc. | го. | | (0.0) (0 | tion | M 40 | | TUM | | | | , al | | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAI | ES. | | | | May 12 | | | | | | | | | _ | | |
| DEPTH | MLM>41-02 | | STRATA | W E L L | | | | PLES RECOVERY | N | שטרא י | SHEAR STRENGTH ◆ S Field Vane Test (#=Sensitivity) ▲ Penetrometer ■ Torvane | | | | | | | | | |
| 1 | I | STRATA DESCRIPTION | Å | | Y P E | ; | Ü M | δĀ | (blows) | Ē | | to ele e | 40 | -14 | , , , , , , , , , , , , , , , , , , , | 80 k | | 41 | | |
| | O N | DESCRIPTION | P | L OG | P | | NUMBER | E R | or RQD | ロ田区のートン | A | terbe | _ | M W | | ioisti | ire | | | |
| (m) -0 - | (m) 256.2 | | 후 | | | | | (mm) or (%) | (%) | Ť Y (kN/m3) | | T N V | — <u>⊢</u> | × | ⊣ | mic (| | | | |
| | | TOPSOIL - 300 mm | 17.71.1 71.14.71 | | | | | | | | | | | | | | | $\mathbb{H}_{\mathbb{L}}$ | | |
| | 255.9 | PEAT - black, fibrous, wet | 17 - 71-17 | | \forall | | | | | | ++ | +++ | Ш | + | + | | H | H | | |
| | | TEXT States, No. | 1, 11, | | $ V _{c}$ | 3B S | SA 1 | | | | | | | \blacksquare | | | | 323 | | |
| - | | | 71/ | | \mathbb{N} | | 5, () | | | | | | | | | | Ш | ∄ 1 | | |
| - | | | 1/ 1// | | | | | | | | | | | | | | | Н- | | |
| -1 | 255.2 | MARL - mixed peat, light grey, wet | 77 7 | | Н | | | | | | - | +++ | Ш | + | | | | H- | | |
| - | | marke mixed peak, light groy, wet | 1, 11, | | | GB S | SA 2 | | | | | | Ш | \blacksquare | | Ш | | dio | | |
| - | | | <u> </u> | | \mathbb{N} | | J, (_ | | | | | | | | | | Ш | $\sharp \downarrow$ | | |
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| -2 | | | 1, 11, | | | | | | | | | | Ш | | | Ш | Ш | $\exists \exists$ | | |
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| - | | | 1, 11, | | | | | | | | | | | +H | +H | | | \mathbb{H} | | |
| - | | | 71/2 | | | | | | | | | | | | | | | П- | | |
| _ | | | <u> </u> | | | | | | | | Ш | | Ш | Ш | | Ш | Ш | ∄. | | |
| -3 | 253.2 | | 711/2 V | | | | | | | | | | | | | | | \mathbb{H}_{\perp} | | |
| | | SAND - brown, loose, wet | | | M | | | | | | Ш | +++ | \mathbb{H} | + | + | + | Н | \mathbb{H} | | |
| | | | | | | GB S | SA 3 | | | | О | | | +H | \blacksquare | \blacksquare | Н | H1 | | |
| | 252.7 | Find of the day's at 0.5 m. have | | | \mathbb{H} | | | | | | Ш | | | | | | | П | | |
| - | | End of test pit at 3.5 m bgs. | | | | | | | | | | | | | | | | | | |
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| 5 | | | 1 | | | | | | EGEND | | | | | | | | | _ | | |
| <u>NO1</u> | | | | _ | | | | | er Samp ore (eg. l | | SS Sp (, etc.) | olit Spo | on | | | Shelby /ane s | | | | |
| m | iust be re | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | ∕ others \0. | s. Test | pit lo | og | OTHE | R TES | STS | | | | | | | | Ċ | | | |
| 2) Te 3) Te | est pit is b est pit cav | ased on observations of the excavator resistance. ed and water observed near 3.0 m bgs upon comple s below ground surface. | tion of | excav | ation | 1. | H Hy | drome | | C | Consol) Cons | olidate | d Drai | | | | | | | |
| 4) bo 5) G | gs denote eodetic el | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | | | eve An nit Wei | | | J Cons J Unco | | | | | | ıl | | | |
| | | , , | | | | | P Fie | eld Per | meability | / UC | C Unco S Direct | nfined | Comp | | | | | | | |
| | | | | | | - 1 | | | neability VELS | DS | DILEC | ı ənea | ı | | | | | | | |
| | | | WATER LEVELS | | | | | | | | | | | | | | | | | |

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TP3A

| PR | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | | | |
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| | | uburn Developments Inc. | | | _ | | | | | | Ge | | | | | | | | _ | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | | | | | | Mater Level | | | | | | | | | | | |
| DWPLI | M-M>4H-OZ | STRATA | ST R A T A | W E L L | T Y P | - | SAM NUMBER | PLES RECOVERY | N VALUE (blows) | שטרא סהי | | P | ene | eld ' tro | Van net | e T er 0 | est | (#=: To | Sens rvan 80 | e ķPa | | |
| '' | N N | DESCRIPTION | P | G G | PE | • | BE | E R V | or RQD | ロயヱの――> | | А | tte | rbei | _ | | ts a W | | Mois | ture | • | |
| (m) | (m) 255.4 | | 후 | | | | ĸ | (mm) or (%) | (%) | T Y (kN/m3) | | S | PT 10 | N V | ا alue 2 | | | ⊣ Dyna 30 | amic | Cor | ne | |
| -0 - | 200.4 | TOPSOIL - 300 mm | 7/1 /V | | П | | | (70) | | (KIWIII) | Ħ | Н | Ï | Ή | HÌ | Ť | Щ | Ŧ | | Π | | Ħ |
| | 255.1 | SAND - brown/grey, trace gravel, loose, wet | 17 : 7.17 | | \sqcup | | | | | | H | Ħ | Ħ | | | | \blacksquare | | | \boxplus | | |
| _ | | CAND - Blown/gley, trace graver, loose, wet | | | | ЗB | SA 1 | | | | H | Ħ | H | | | \blacksquare | \blacksquare | | | \blacksquare | | 11 |
| | | | | | $\langle \rangle$ | | | | | | H | H | | | \blacksquare | \blacksquare | \blacksquare | | | \blacksquare | | |
| − 1 | | | | | | | | | | | H | H | | | | | | | | Ш | | |
| · - | | | | | | | | | | | H | Ħ | | | | | Ш | | | Ш | | 11 |
| - | | | | | | | | | | | H | Ħ | \parallel | | | | | | | $\frac{1}{1}$ | | 11 |
| - | | | | | | | | | | | Ħ | Ħ | Ħ | | | | Н | | | \boxplus | | 1 |
| - | | | | | | | | | | | H | Ħ | H | | | | | | | H | | 1 |
| -2 | | | | | | | | | | | H | H | H | | | | H | | | \blacksquare | | $\left\{ \cdot \right\}$ |
| - | | | | | | | | | | | H | H | H | | \blacksquare | | | | | \blacksquare | | $\left\{ \cdot \right\}$ |
| _ | 252.9 | | | | | | | | | | | H | | | | | | | | Ш | | H |
| - | | End of test pit at 2.5 m bgs due to unstable sidewalls. | | | | | | | | | | | | | | | | | | | | $ \cdot $ |
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| 5 | | | <u> </u> | | | \dashv | | | EGEND | | | | | | | | | | | | | Ц |
| <u>NO1</u> | | rpretation requires assistance by EXP before use by | nit I | | ⊠ A □ F | S Aug Rock C | er Samp ore (eg. | le | S), e | S S tc.) | plit | Spo | on | | | | Shell Vane | | | , | | |
| 2) T | nust be rea | ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. | \0. | s. Test | рии | og | G Sp | | Gravity | | | | | ation | | | | | | | | |
| 3) To 4) bo | est pit cav gs denote | ed upon completion of excavation. s below ground surface. | | | | | S Si | /drome eve An | alysis | CL | JC | cons | solio | date | d U | ndra | aine | | iaxial | | | |
| [5) G | eodetic el | evations surveyed using a SOKKIA GCX2 Receiver. | | | | | P Fie | | meability | y UC | Cι | Inco | onfi | ned | Cor | | | | Triax | tial | | |
| | | | | | | | WAT | ER LE | | DS | S C | ired | ct S | hea | r | | | | | | | |
| | | | - [| | ppare | | ▼ Me | eas | ure | ed | | 7 | Ĭ. | Art | esia | n (se | e No | otes) | | | | |

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| _ | DDO IFOT House Farms | | | | | | | | | | | | | | | | | | | |
|---|---|--|---------------|----------|----------|-------------|-------------------|-----------------------------|-----------------------|---|---------|-----|---|------|--------|------|---|--|--|--|
| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | |
| | | Auburn Developments Inc. Marion Street, Dorchester, ON | Fxcav | ration | May 12 | | | | | | vel | | | _ | | | | | | |
| | | manori otreet, Boronester, ON | $\overline{}$ | D/(1 | LО. Т | | | | | Mater Level SHEAR STRENGTH | | | | | | | | | | |
| DWPHI | ZO1> <mr< th=""><th>STRATA DESCRIPTION</th><th>STRATA P</th><th>WELL LOG</th><th>TYPE</th><th>N U M B E R</th><th>RECOVERY</th><th>N VALUE (blows) or</th><th>BULK DEZW-FY</th><th colspan="8">◆ S Field Vane Test (#=Sensitivity) ◆ Penetrometer ■ Torvane 40 80 kPa Atterberg Limits and Moisture</th></mr<> | STRATA DESCRIPTION | STRATA P | WELL LOG | TYPE | N U M B E R | RECOVERY | N VALUE (blows) or | BULK DEZW-FY | ◆ S Field Vane Test (#=Sensitivity) ◆ Penetrometer ■ Torvane 40 80 kPa Atterberg Limits and Moisture | | | | | | | | | | |
| (m) | (m) 256.0 | | Ļ | Ğ | _ | Ē | (mm) or (%) | 1, | Ĭ T Y kN/m3) | , | | | | | | | | | | |
| -0- | | TOPSOIL - 300 mm | 7/1/N. 7/1 | | | | 1 | Ì | | | | Ш | Н | | | Н | П | | | |
| - - - -1 | 255.7 | SAND - brown/grey, some silt, loose, moist to very moist | <u> </u> | | G | B SA 1 | | | | | | | | | | | | | | |
| - - - -2 - | | - becoming grey near 2.0 m bgs | | | | | | | | | | | | | | | | | | |
| - - - - | 253.0 | End of test pit at 3.0 m bgs. | | | | | | | | | | | | | | | - | | | |
| - - -4 - | | | | | | | | | | | | | | | | | - | | | |
| 5 | r=0 | | | | | | | EGEND ger Sampl | e Ø | SS S | nlit Sn | oon | | ST S | Shelby | Tube | - | | | |
| NOTES 1) Test pit interpretation requires assistance by EXP before use by others. Test pit log must be read in conjunction with EXP Report LON-21008138-A0. 2) Test pit is based on observations of the excavator resistance. 3) Test pit caved and dry upon completion of excavation. 4) bgs denotes below ground surface. 5) Geodetic elevations surveyed using a SOKKIA GCX2 Receiver. As Auger Sample Rock Core (eg. BQ, NQ, etc.) VN Vane Sample C Consolidation H Hydrometer CD Consolidated Drained Triaxial S Sieve Analysis CU Consolidated Undrained Triaxial Y Unit Weight UU Unconsolidated Undrained Triaxial P Field Permeability K Lab Permeability K Lab Permeability UC Unconfined Compression WATER LEVELS Apparent Measured Artesian (see Notes) | | | | | | | | | | | | | | | | | | | | |

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| PR | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | |
|---|---|--|---|----------|-------------|-------|------|-----------------|---|-------------------------------------|--|--|--|--|
| | | uburn Developments Inc. | DATUM Geodetic Excavation May 12, 2021 Water Level | | | | | | | | | | | |
| LO | _ | Marion Street, Dorchester, ON | | DATI | ES: | | | | May 12 | | | | | |
| Эшент () | — З ZO1><ш-ш | STRATA DESCRIPTION | SHRAHA PLOH | WELL LOG | T P E | | ` (n | RECOVERY mm) or | N VALUE (blows) or RQD (%) | ≺א-שבשם ארכש | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane 40 80 kPa Atterberg Limits and Moisture WP W WL SPT N Value X Dynamic Cone | | | |
| -0- | 255.1 | TOPSOIL - 300 mm | 7,1 \(\frac{1}{2}\). \(\frac{1}{2}\) | | П | | + | (%) | | (kN/m3) | 10 20 30 40 | | | |
| - - - -1 - - - | 254.8 | SAND and GRAVEL - brown, trace silt, loose, moist to wet - becoming grey near 2.0 m bgs | | | | GB SA | | | | | ф — — — — — — — — — — — — — — — — — — — | | | |
| - | 252.6 | | 0.00 | | | | | | | | | | | |
| - - - - - - - - - - - - - | | End of test pit at 2.5 m bgs due to unstable sidewalls. | W A 10 | | | 9 | MARI | | GEND | | - - - - - - - | | | |
| NOTES 1) Test pit interpretation requires assistance by EXP before use by others. Test pit log must be read in conjunction with EXP Report LON-21008138-A0. 2) Test pit is based on observations of the excavator resistance. 3) Test pit caved and water observed near 2.0 m bgs upon completion of excavation. 4) bgs denotes below ground surface. 5) Geodetic elevations surveyed using a SOKKIA GCX2 Receiver. SAM ☐ F OTH G S H H S Si Y U P Fi K La WAT | | | | | | | | | | BQ, NQ CI CL UL U DS | SS Split Spoon In ST Shelby Tube In VN Vane Sample Consolidation Consolidated Drained Triaxial Consolidated Undrained Triaxial Consolidation Consolidation Consolidation Consolidated Undrained Triaxial | | | |

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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | |
|------------|---|--|--|------------------------------------|--------------|------------------|----------|-------------------|------------------------|-------------------|--|--|--|--|
| | ` | uburn Developments Inc. Marion Street, Dorchester, ON | | TUM <u>Geodetic</u> Water Level | | | | | | | | | | |
| LO | _ | Midifort Street, Dorchester, ON | | DAII | _3 | | | PLES | May 12 | | SHEAR STRENGTH | | | |
| DHPHI | ELEVAT- | STRATA | STRATA | WELL | - | т | | NECO>WEY | N VALUE | יס ארכש | ◆ S Field Vane Test (#=Sensitivity) ▲ Penetrometer ■ Torvane 40 80 kPa | | | |
| Ĥ | i O N | DESCRIPTION | P | LOG | Ì | T Y P E | NUMBER |) ER | (blows) or | ロ田区の――> | Atterberg Limits and Moisture W _P W W _L | | | |
| (m) | (m) 255.1 | | Ρ̈́ | G | | | R | (mm) or (%) | RQD (%) | † Y (kN/m3) | ● SPT N Value × Dynamic Cone | | | |
| -0- | | TOPSOIL - mixed fill, 1.2 m | \(\frac{1}{2\frac{1}{2}\frac{1}{2 | | | | | | | | | | | |
| | | | : <u>7</u> \(\frac{7}{2}\); | | | | | | | | | | | |
| | | | <u>''</u> . <u>\ </u> | | | | | | | | | | | |
| | | | $\frac{1}{2}$ | | | | | | | | | | | |
| | | | 77. ·7 | | | | | | | | | | | |
| -1 | 253.9 | | <u> </u> | | | | | | | | | | | |
| | | SAND and GRAVEL - grey, loose, wet | 0.00 0.00 | | M | GB | SA 1 | | | | | | | |
| | 253.6 | SILTY SAND - grey, loose, wet | 0.00 | | А | 0.2 | . | | | | | | | |
| | | SIETT SAND - grey, 100se, wet | | | M | GB | SA 2 | | | | | | | |
| - | | | | | \mathbb{N} | | | | | | | | | |
| -2 | | | | | | | | | | | | | | |
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| - | | | | | | | | | | | | | | |
| - | 050.4 | | | | | | | | | | | | | |
| -3 | 252.1 | End of test pit at 3.0 m bgs. | | | | | | | | | | | | |
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| 5 | | | | | Ш | | SAMI | L PLE LE | EGEND | | | | | |
| <u>NO1</u> | | | | _ | | | ⊠ A | S Aug | er Samp ore (eg. | | SS Split Spoon ■ ST Shelby Tube □ VN Vane Sample | | | |
| ľm | nust he re: | rpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | .O | | • | _ | OTHE | ER TE | | | Consolidation | | | |
| 3) To | est pit is b | ased on observations of the excavator resistance. ed and water observed near 1.2 m bgs upon comple s below ground surface. | tion of | excava | atio | n. | НΗ | drome eve An | eter | C | D Consolidated Drained Triaxial U Consolidated Undrained Triaxial | | | |
| 5) G | eodetic el | evations surveyed using a SOKKIA GCX2 Receiver. | | | | | 7 Ur | nit Wei | ight | UL | U Unconsolidated Undrained Triaxial | | | |
| | | | | | | | K La | b Pern | meability neability | | C Unconfined Compression S Direct Shear | | | |
| | | | | | | | | | VELS nt | ▼ Me | leasured Ā Artesian (see Notes) | | | |

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| DD | PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | | |
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| | | Auburn Developments Inc. | | | | | | | | | | | | det | | 14-2 | 100 | U 130 | ,- /- (| <u> </u> | |
| | | Marion Street, Dorchester, ON | ES: E | Excava | ation _ | May 12 | | | | | | | | eve | l _ | | | | | | |
| | Ę | | s | | | SAM | IPLES | | В | SHEAR STRENGTH | | | | | | | | | | | |
| Б | | | | | | | | | | | | | ivity | " | | | | | | | |
| ОШР⊢Н | Ă | STRATA | 🛱 | WELL | Ţ | Ŋ | C | VALUE | l | | | 1 | | 40 | | 1 | | 80 ķī | Pa | | |
| Ĥ | o N | DESCRIPTION | P | LOG | T Y P E | NUMBER | RECOVERY | (blows) or | DE NS- | | At | terk | perç | | | an W | | oistu | re | | |
| (\ | (m) | | 卢 | Ğ | | Ŕ | (mm) | RQD (%) | | ۱. | SP | TN | Val | lue | —≎ | - | _ | nic C | :one | | |
| (m) -0 - | 257.0 | TORONI | 17. 15. 15 | | | | `or´ (%) | 1 | (kN/m3) | | | 10 | | 20 | <u>-</u> | 30 | | 40 | | | |
| - | 256.7 | TOPSOIL - 300 mm | 1/ 1// | | | | | | | Ħ | | | | | Ш | | | | | Щ. | |
| L | 230.7 | SAND and GRAVEL - brown, loose, moist | 0.00 | | \bigvee | | | | | Ħ | | | \parallel | Ħ | Ш | | # | Ш | | Ш. | |
| _ | 256.4 | | 0:00 | | ∭GE | SA 1 | | | | H | o | | \parallel | | Ш | | | | | Ш. | |
| | | SILT TILL - brown, some clay, trace gravel, compact, moist | | | \mathbb{M}_{a} | | | | | H | | | \coprod | \parallel | Н | | \parallel | Ш | | Н. | |
| -1 | | | | | GE | SA 2 | | | | H | | | Φ | | | | + | | | \mathbb{H}_{-} | |
| | | | | | H | | | | | H | | H | \prod | \prod | H | | H | H | $last \Pi$ | \mathbb{H}^{-} | |
| | | | | | | | | | | H | \blacksquare | H | ${\mathbb H}$ | $oxed{+}$ | H | Н | H | Н | Н | \blacksquare | |
| _ | | | | | | | | | | H | | | \Box | | H | | + | Ш | | \blacksquare | |
| - | | | | | | | | | | Ħ | | | \parallel | | Щ | | # | Ш | | # | |
| | | | | | | | | | | Ħ | | | | | Ш | | | Ш | | # | |
| -2 | | | 9 | | | | | | | Ħ | | | Ħ | \dagger | Ш | | \dagger | Ш | | Ш- | |
| - | | | | | | | | | | H | Ш | Ш | Ш | | Ш | | | Ш | | Ш. | |
| - | | | | | | | | | | Ш | | | | | | | | Ш | | Н. | |
| _ | | - becoming grey near 2.5 m bgs | | | M., | | | | | H | | | + | | Н | | + | Ш | | + | |
| - | | | | | GE | SA 3 | | | | H | | 0 | \blacksquare | | П | | + | | | \blacksquare | |
| -3 | | | | | Н | | | | | H | | \blacksquare | \mathbf{H} | $oxed{+}$ | H | | + | H | | | |
| - | | | | | | | | | | H | | H | Ħ | H | F | | Ħ | Ш | | # | |
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| _ | | | | | | | | | | Ħ | | | \parallel | | Ш | | # | Ш | | 뵘. | |
| _ | | | | | | | | | | Ħ | | | \parallel | | Ш | | | Ш | | Ш. | |
| -4 | 253.0 | | 90 | | | | | | | H | | | | | | | | | | Ш. | |
| -7 - | | End of test pit at 4.0 m bgs. | | | | | | | | | | | | | | | | | | | |
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| 5 | l | | 1 | | | | | EGEND | de 🔽 | <u> </u> | | lit C | · | | | | T 0' | - الم | т! | | |
| NO: | | erpretation requires assistance by EXP before use b | nit loo | □ F | Rock Č | ger Samp ore (eg. | | | SSp c.) | iit S | poc | on | | | | nelby ane S | | | | | |
| 'n | nust be re | ad in conjunction with EXP Report LON-21008138- based on observations of the excavator resistance. | A0. | . rest | pit 10g | TOTH | ER TE | STS Gravity | C | Cor | າຣດli | idati | ion | | | | | | | | |
| l 3) T | est bit obe | en and dry upon completion of excavation. s below ground surface. | | | | G Specific Gravity C Consolidation H Hydrometer CD Consolidated Drained Triaxial S Sieve Analysis CU Consolidated Undrained Triaxial | | | | | | | | | | | | | | | |
| 5) G | eodetic e | evations surveyed using a SOKKIA GCX2 Receiver | - | | | γ υ | nit We | ight | Ül | υU | ncor | nsol | idat | ed L | Jndi | raine | ed T | riaxia | ı | | |
| 1 | | | | | | K La | ab Perr | rmeability neability | y 00 | | rect | | | Com | pres | 55101 | 1 | | | | |
| | | | | | | | WATER LEVELS ✓ ▼ Apparent ▼ Measured | | | | | | | | | | | | | | |

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| D.D. | O IECT | Hunter Form | | | | | | | | | | | · - · | | | | NI O | 100 | 042 | D A | | + |
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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | | | |
| | | Marion Street, Dorchester, ON | | DAT | ES: | Ex | cava | ition _ | May 12, | | | | | | | | evel | | | | | - |
| | E | | | | | | | PLES | | | Τ | | | | EAR | ST | REN | GTI | Н | | | ٦ |
| DHPTH | Ш ₩₩₩₩₩ | STRATA DESCRIPTION | STRATA | WELL . | T Y F | 5 | ZUZBER | RECOVERY | N VALUE (blows) | BULK DEXS-FY | | ▲ Pe | enet | rom | ete 40 | r | ■ T | orv | ensit ane 80 k oistu | Pa | y) | |
| | | | P O | L O G | Ė | • | E | Ŕ | or RQD | S I T | | | | • | • | | w | | | | | |
| (m) | (m) 257.6 | | Ť | | | | | (mm) or (%) | (%) | Ý kN/m3) | | ● SF | PT N 10 | l Va | lue 20 | > | < Dy 30 | - | nic (| - | e | |
| - 0 - - - - | | TOPSOIL - mixed peat, 1.2 m | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | | | | | | | | | | | | | | | | | | | |
| 1 - | 256.4 | SANDY SILT - brown/grey, trace gravel, trace | \(\frac{1}{2} \) \(\frac{1} \) \(\frac{1} \) \(\frac{1}{2} \) \(\frac{1}{2} \ | | | | | | | | | | | | | | | | | | | _ |
| - | 255.6 | clay, loose, very moist to wet | | | X | GB S | SA 1 | | | | | | | | | | | | | | | |
| - 2 - - - - - - | | End of test pit at 2.0 m bgs. | | | | | | | | | | | | | | | | | | | | |
| -4 - - - - 5 | | | | | | | SAMF | PLE LE | EGEND | | | | | | | | | | | | | |
| 1) Te m 2) Te 3) W 4) bo | NOTES 1) Test pit interpretation requires assistance by EXP before use by others. Test pit log must be read in conjunction with EXP Report LON-21008138-A0. 2) Test pit is based on observations of the excavator resistance. 3) Water observed near 1.8 m bgs upon completion of excavation. 4) bgs denotes below ground surface. 5) Geodetic elevations surveyed using a SOKKIA GCX2 Receiver. As Auger Sample □ Rock Core (eg. BQ, NQ, etc.) □ VN Vane Sample □ VN Vane | | | | | | | | | | | | | | | | | | | | | |

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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | |
| | | | | | FO: 1 | - | - 4: | | | | | | | | | | | | - |
| LO | CATION | Marion Street, Dorchester, ON | | DAI | ES: E | xcava | ation _ | May 12 | | | | | | | evel | | | | |
| | E | | ş | | | SAM | IPLES | | אררא | | Fiel | | | | | GTH | | .i4.A | |
| ₽ | M-M02 | | STRAT | W E L L | | | R | N | K | | riei eneti | | | | | | | vity) | |
| ОШР⊢Т | Ą | STRATA | Ţ | E | т | N | မြ | VALUE | ₽ | | | | 40 | | | 8 | 0 kP | а | |
| Ĥ | Ö | DESCRIPTION | ^ p | | T Y P E | NUMBER | RECOVERY | (blows) | Ň | | tterk | erg | | | | | istur | ·e | 71 |
| | | | <u> </u> O | L OG | = | E | | RQD | ロயヱめート≻ | | | | WP | W | w | L | | | |
| (m) | (m) 259.0 | | Ť | | | | (mm) or (%) | (%) | Ϋ́ (kN/m3) | | PT N 10 | Val | ue 20 | > | Oy 30 | | ic Co 40 | one | |
| -0 - | 239.0 | TOPSOIL - 400 mm | 74 1× . 7/ | | | | (%) | | (KIV/III3) | ш | | Т | | П | | П | | Т | |
| - | | | 1/. 311/ | l | | | | | | HH | \mathbb{H} | \mathbb{H} | | | + | Н | \mathbb{H} | + | Н- |
| - | 258.6 | | <u> </u> | | Ц | | | | | Ш | Ш | Ħ | Ш | | | | Ш | | ┇╻ |
| | | SANDY SILT - brown, trace clay, trace gravel, , loose, moist | | | М | | | | | HH | +++ | + | + | + | + | H | +++ | ₩ | $H \mid$ |
| | | , | | | GE | SA 1 | | | | | \blacksquare | H | | | | | | \blacksquare | \square |
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| | 257.5 | CLAYEY SILT TILL - grey, trace sand and | 97. | | Н | | | | | \mathbb{H} | H | + | + | | + | Н | + | + | Н |
| - | | gravel, stiff, moist | | 1 | $\mathbb{N}_{\mathbb{C}^{\mathbb{R}}}$ | SA 2 | | | | Ш | Ш | Ħ | | | | | Ш | | |
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| | 255.5 | | | | | | | | | Ш | Ш | | | | Ш | Ш | Ш | Ш | |
| - | | End of test pit at 3.5 m bgs. | | | | | | | | | | | | | | | | | - |
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| 3 | | | | | | | | EGEND Ier Samn | - le 171 | SS S | nlit S | noo | n | | ST | Γ.Sh | alby ⁻ | Tube | .] |
| | NOTES 1) Test pit interpretation requires assistance by EXP before use by others. Test pit log AS Auger Sample | | | | | | | | | | | | | | | | | | |
| lím | nust be re | ad in conjunction with FXP Report I ON-21008138- | 10. No. | , i Col | pit 10g | JOIH | ER TE | STS Gravity | C | Consc | didati | on | | | | | | | |
| 3) T | est pit ope | pased on observations of the excavator resistance. en and dry upon completion of excavation. s below ground surface. | | | | HH | ydrome | eter | C | O Con | solida | ated | | | | | | | |
| 4) bo 5) G | gs denote eodetic el | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | | eve An nit Wei | | | J Con: J Unc | | | | | | | | | |
| | | | | | | P Fi | eld Per | rmeability | / UC | C Unc | onfin | ed C | | | | | | | |
| | | | | | | 1 | | neability VFLS | DS | S Dire | JI SN | ear | | | | | | | |
| | WATER LEVELS | | | | | | | | | | | | | | | | | | |

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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | |
| | | • | | D 4 T | | - | - 4° | | | | _ | | | | | | | | | - |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: 1 | xcava | ation _ | May 12 | | | | | | | Lev | | | | | |
| | Ę | | ş | | | SAM | IPLES | | B U | L | ° E | _ | | | _ | ENG | | 141 | :4. A | |
| ₽ | ZO1> <mr< td=""><td></td><td>ST RAT</td><td>WELL</td><td></td><td></td><td>R</td><td>N</td><td>Ĺ K</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Sens rvan</td><td></td><td>ity)</td><td></td></mr<> | | ST RAT | WELL | | | R | N | Ĺ K | | | | | | | | Sens rvan | | ity) | |
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| Ĥ | 0 | DESCRIPTION | ^ P | | T Y P E | NUMBER | RHCO>HR> | (blows) | N | | Att | erbe | rg l | Lim | | | Mois | | | 11 |
| | | | <u>-</u> 한 | LOG | E | E R | | or RQD | ロயヱめート> | | | | ١ | N _P | W | WL | | | | |
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| -0- | 258.0 | TOPSOIL - 400 mm | 74 1×. 7/ | | | | (%) | | (kN/m3) | h | \Box | 10 | Ή | 2 0 | ΤП | 30 | тт | 10 | ΙП | + |
| - | | | 17. 71.17 | | | | | | | Ш | \blacksquare | Ш | \blacksquare | \bot | Ш | \blacksquare | Ш | | | 44 |
| | 257.6 | | : <u>\'\\'</u> .\'\\ | | | | | | | Ш | Ш | Ш | | Ш | Ш | \pm | Ш | Ш | | ┧] |
| | | SILTY SAND - brown, loose to compact, moist | | | М | | | | | Н | + | Н | $^{+}$ | $^{+}$ | ++ | $+\!\!+$ | ₩ | + | | $+$ \parallel |
| - | | | | | GE | SA 1 | | | | Ш | \blacksquare | Ш | 0 | $^{\parallel}$ | Ш | # | Ш | Ħ | | 11 |
| - | | | | | \Box | | | | | H | + | Н | + | H | ++ | + | \mathbf{H} | H | | 11 |
| -1 | | | | | | | | | | H | | \mathbb{H} | | | Н | # | Ш | | | 44 |
| _ | 256.8 | | | | | | | | | Ш | Ħ | Ш | | Ħ | Ш | # | $\parallel \parallel$ | | | 11 |
| | | CLAYEY SILT TILL - brown, trace sand, stiff, moist | | | М | | | | | Н | $^{+}$ | Н | $^{+}$ | $^{+}$ | ${\mathbb H}$ | $+\!\!+$ | ₩ | $^{+}$ | | + $ $ |
| | | | | | GE | SA 2 | | | | Ш | | 0 | | Ħ | Ħ | # | Ш | | | 41 |
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| -2 | 256.0 | | | | Ц | | | | | Ш | П | Ш | Ħ | Ħ | Ш | # | Ш | | | 11 |
| | | SILT TILL - grey, compact, moist | 1916 | | М | | | | | H | + | Н | $^{+}$ | $^{+}$ | ++ | ++ | ++ | H | | + |
| | | | | | GE | SA 3 | | | | П | H | ¢ | 1 | H | \blacksquare | \mp | \prod | | | 71 |
| - | | | | | Ц | | | | | Ш | | Ш | | | Ш | \pm | Ш | | | 11 |
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| - | | | 48 | | | | | | | Ш | \blacksquare | Ш | \blacksquare | Ħ | Ш | # | Ш | Ħ | | 44 |
| -3 | | | | | | | | | | Ш | | Ш | | Ħ | Ш | \pm | Ш | | | 11 |
| ٥ | | - dilatant silt layering encountered near 3.0 m bgs | | | | | | | | Н | + | Н | $^{\rm H}$ | $^{+}$ | ${\mathbb H}$ | $+\!\!+$ | ₩ | ₩ | | $+$ \parallel |
| - | | | | | | | | | | Ш | Ħ | Ш | \blacksquare | Ħ | Ш | # | Ш | | | 11 |
| - | 254.5 | | 91 | | | | | | | Ш | | Ш | \parallel | $^{+}$ | Ш | <u></u> | Ш | | | 1- |
| - | | End of test pit at 3.5 m bgs. | | | | | | | | | | | | | | | | | | - |
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| NOTES | | | | | | | | | | | | | | | | | | | | |
| ľm | nust be rea | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | 40 | | | ОТНІ | ER TE | STS | | - | , | | | | | | | | • | |
| 2) T | est pit is b est pit ope | ased on observations of the excavator resistance. In and water observed near 1.2 m bgs upon complet is below ground surface. | ion of e | excava | tion. | | pecific ydrome | Gravity eter | | | | datio lidat | | Orair | ned . | Triax | kial | | | |
| 4) b | gs denote | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | 5. 6 | | | S Si | eve An | alysis | Cl | J Co | nso | lidat | ed (| Jndr | aine | ed Tr | iaxial | | | |
|] , | JOUGHU E | evaluents surveyed dailing a SONNIA GOAZ Necelver. | | | | P Fi | nit Wei eld Per | meability | / UC | C Ur | ncon | fine | d Co | | | | Triax | ııdı | | |
| | | | | | | K La | b Pern | neability [•] | | | | She | | • | | | | | | |
| | WATER LEVELS ✓ ¬ ¬ ¬ ¬ ¬ ¬ ¬ ¬ ¬ ¬ ¬ ¬ ¬ | | | | | | | | | | | | | | | | | | | |

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| | | uburn Developments Inc. | | DAT | го. | | vetion | | | TUM | , | | | al | | | - |
| LO | CATION | Marion Street, Dorchester, ON | | DAI | ES. | | | <u>May 12</u> | | | | Wate | | | | | |
| DEPTH | | STRATA | STRAT | W E L L | | | RECOVERY | | BULK D | | | | Tes r | t (#= | Sensit | • | |
| H | i O N | DESCRIPTION | P | | T Y P E | | İ | (blows) | E N | A | tterbe | rg Lir | nits | | Moistu | | 11 |
| | | | Ŀ | L OG | E | | R | . 1 | ロ田区の一下と | | | _ ∸ | , W | WL | | | |
| (m) -0 - | (m) 263.3 | | Ť | | Ļ | | (mn or (%) | (%) | Ý (kN/m3) | | PT N \ 10 | /alue 20 | × | Dyna 30 | amic C 40 | | Ц |
| | | TOPSOIL - 400 mm | 17.71.14 34.14.71.14 | | | | | | | Ш | | | | | | | |
| | 262.9 | | · · · · · · · · · · · · · · · · · · · | | | | | | | - | +++ | +++ | Н | | | Ш | + 1 |
| | | CLAYEY SILT TILL - brown, stiff, moist | 73/ | | \bigvee | | | | | \Box | \square | \mathbf{H} | | | | Ш | 71 |
| - | | | | | ∭G | BSA | . 1 | | | Ш | Ш | | | | | | 11 |
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| | | | 30 | | | | | | | ++ | +++ | +++ | H | | | HH | $\ \ $ |
| | 260.8 | SILTTILL brown come day compact moist | | | Н | | | | | | | | Ш | | | | 77 |
| - | | SILT TILL - brown, some clay, compact, moist | | 1 | $\mathbb{N}_{\mathbb{C}}$ | B SA | 2 | | | Ш | | | Ш | | | Ш | 11 |
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| - | | | 10 | 1 | | | | | | Ш | Ш | | ш | Ш | | Ш | 11 |
| 4 | 259.3 | End of test pit at 4.0 m bgs. | 991.3 | | | | | | | | | | | | | | $\dagger \dagger$ |
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| <u>NO1</u> | <u>ES</u> | | | | | | AS A | uger Samp Core (eg. | le 🛮 | SS S | plit Sp | oon | | | Shelby Vane S | | |
| 1) Te | est pit inte | rpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | others | s. Test | pit lo | g oı | HER T | ESTS | JW, 190 | ., 0.0.) | | | لنن | . V 1 N | , ui iC (| zai ii pit | ´ |
| 12) Te | est nit is h | ased on observations of the excavator resistance | | | | G | | c Gravity | | Conso | | | ined | l Triav | ial | | |
| 4) bo | gs denote: | n and dry upon completion of excavation. s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | S | Sieve A | Analysis | Cl | J Cons | solidat | ed Un | drain | ed Tr | iaxial | ı | |
| 3) G | eouelic el | evalions surveyed using a SORRIA GOAZ RECEIVER. | | | | P | | ermeability | y U | J Unco C Unco | onfine | d Com | | | ırıaxıa | I | |
| | | | | | | K | Lab Pe | rmeability | | S Direc | t She | ar | | | | | |
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| | | Marion Street, Dorchester, ON | | DAT | ES: E | Excava | ation | May 12 | | | | | | | | eve | el | | | |
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| ОШ₽Т | Ā T | STRATA | X | ן t | Ţ | N N | Ö | VALUE (blows) | E | L | | | | 40 | | | | 80 ķ | | |
| п | Ò | DESCRIPTION | P | LOG | Y P E | | Ė | or | DE NS- | | At | terk | perç | | | sar / V | | loist | ure | |
| (m) | (m) | | Þ | G | | R | (mm) | RQD (%) | ţ | ١. | SP | ΤN | Val | - | -0 | — | 1 | mic (| Con | e |
| (''') - 0 - | 269.0 | TOPSOIL - 300 mm | 7.1 1×. 1/2 | | | | (%) | | (kN/m3) | <u> </u> | ''' | 10 | ++ | 20 | | 3 | | 40 | | \dashv |
| L | 268.7 | TOPSOIL - 300 mm | 1/2 : 3 : 1/2 | | | | | | | Ħ | | \parallel | | \parallel | | | | | | Ш |
| L | 200.7 | CLAYEY SILT - brown, soft to firm, moist | 1717 | | \forall | | | | | L | | Ħ | | Ш | | | | Ш | | Ш |
| | | | | | ∬GB | SA 1 | | | | H | | + | > | H | | | | | | Ш |
| | | | 1212 | | \Box | | | | | H | Н | + | + | $^{+}$ | $^{+}$ | | | | + | Н |
| | 268.0 | | | | | | | | | H | | \blacksquare | | H | | | | | | \mathbb{H} |
| -1 | 200.0 | SILT TILL - brown, stiff, moist | | | | | | | | H | Ш | \blacksquare | Ħ | Ħ | H | | | | | \square |
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| _ | 000 5 | | | | | | | | | Ħ | Ш | | | Ħ | | | | | | Ш |
| | 266.5 | SAND and GRAVEL - brown/grey, trace cobble, | 0.50 | | \forall | | | | | H | | \pm | \pm | Ħ | Ħ | | | Ш | \pm | Ш |
| | | compact, wet | 0.00 | | | SA 3 | | | | H | | 0 | + | + | | | | | + | Н |
| | | | 0.0.0 | | \square | | | | | H | Н | + | \mathbf{H} | H | Н | | | | + | \mathbb{H} |
| - 3 | | | 000 | | | | | | | H | Н | \blacksquare | + | Ħ | Ħ | | | | | \square |
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| - | | | 0.00 | | | | | | | H | | + | + | H | \mathbf{H} | | | | | H |
| -4 | 265.0 | End of test pit at 4.0 m bgs. | 0.0.0 | | | | | | | Н | | | | | | | | | | Щ |
| - | | | | | | | | | | | | | | | | | | | | |
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| NO: | TES | | | | | | | EGEND jer Samp | ole 🖾 | S | S Sp | lit S | nod | on – | | | TS | helby | Tu | be |
| 1) T | est pit inte | erpretation requires assistance by EXP before use b | y others | s. Test | pit log | □ F | Rock Č | ore (eg. | | | | • | - 50 | | | | | ane s | | |
| 2) T | nust be re est pit is b | ad in conjunction with EXP Report LON-21008138- pased on observations of the excavator resistance. | Å0. | | | GS | ER TE | Gravity | | | nsoli | | | | | | | | | |
| 3) To | est pit cav gs denote | red and water observed near 3.0 m bgs upon comple s below ground surface. | etion of | excava | ation. | HH | ydrome eve An | eter | | | | | | | | | iaxia Tria | | | |
| 5) G | eodetic el | evation surveyed using a SOKKIA GCX2 Receiver. | | | | γ υ | nit Wei | | Ül | υŪ | | nsol | idat | ed l | Und | rain | ed T | riaxia | al | |
| | | | | | | K La | ab Perr | neability | , DS | | irect | | | JU11 | .p.e | JJIU | | | | |
| | | | | | | | ER LE Apparei | | ▼ M | eas | urec | i | | Ā | , | Arte | sian | (see | Not | es) |

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TP11Sheet 1 of 1

| PR | OJECT | Hunter Farm | | | | | | | | PR | OJE | СТ | NO. | | LON | -210 | 0813 | B-A0 | |
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| CLIENT Auburn Developments Inc. LOCATION Marion Street, Dorchester, ON DATES: Excavation May 12, 2021 Water Level | | | | | | | | | | | | | | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DATI | ES: | : E | xcava | ation _ | May 12 | | | | | | | | | | |
| DE | шшы | | STRATA | W E L L | | | | PLES R E C | N | BU LK | | Fie | | ane ' | Test | | | ivity) | |
| DHPHI | 4T-OZ | STRATA DESCRIPTION | A PLO | L L O G | Y | ך ב | NUMBER | RECO>ERY | (blows) or RQD | DEIX%- | - 4 | Atter | berg | | nits a | | 80 ķ Moist i | | |
| (m) -0 - | (m) 267.7 | | Ť | , | | | | (mm) or (%) | (%) | T Y (kN/m3) | | PT N 10 | N Val | ue 20 | | Dyna 30 | mic (| | |
| - 0 | | TOPSOIL - organic fill, 500 mm | | | | | | | | | | | | | | | | | - |
| - | 267.2 | 0.7.7 | <u>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</u> | | Ц | | | | | | | | | | | | | | - |
| - | | SILT TILL - grey, some clay, wet sand layering, cobbles, compact, moist | | | \bigvee | GB | SA 1 | | | | | | | | | | | | |
| -1 | | | | | \wedge | | | | | | | | | | | | | | - |
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| - | | | | | | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | | | | | | |
| - 2 | 265.7 | SAND - grey, fine to medium grained, compact, wet | 911.X | | \bigvee | | | | | | | | | | | | | | _ |
| - | | | | | \bigwedge | GB | SA 2 | | | | | | | | | | | | - |
| - | | | | | | | | | | | | | | | | | | | - |
| - -3 | 264.7 | | | | | | | | | | | | | | | | | | |
| - | | End of test pit at 3.0 m bgs. | | | | | | | | | | | | | | | | | - |
| - | | | | | | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | | | | | | |
| -4 | | | | | | | | | | | | | | | | | | | - |
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| - | | | | | | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | | | | | | |
| SAMPLE LEGEND ☑ AS Auger Sample ☑ SS Split Spoon ■ ST Shelby Tube | | | | | | | | | | | | | | | | | | | |
| 1) T | est pit inte | erpretation requires assistance by EXP before use by | others | . Test | pit I | log | | | ore (eg. | | | | υμυσ | 11 | | | | Sample | |
| 2) T 3) T | est pit is b est pit cav | ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. ed and 0.3 m of water observed upon completion of | ∙∪. excava | tion. | | | G Sp H Hy | oecific ydrome | Gravity eter | CI | Conso Con | solid | lated | | | | | | |
| 4) bgs denotes below ground surface. 5) Geodetic elevation surveyed using a SOKKIA GCX2 Receiver. S Sieve Analysis Y Unit Weight P Field Permeability K Lab Permeability D S Direct Shear | | | | | | | | | | | | | | | | | | | |
| | P Field Permeability UC Unconfined Compression K Lab Permeability DS Direct Shear WATER LEVELS ▼ Apparent ▼ Measured ★ Artesian (see Notes) | | | | | | | | | | | | s) | | | | | | |

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TP12

| PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | | |
|---|---|---|----------------|-------------|----------|------|--------|-------------------|-----------------------|---------------|---|---|-----------|------------|---|-----------|-------------------|----------|---------------|--|
| | · · · · · · | uburn Developments Inc. Marion Street, Dorchester, ON | | DAT | EQ. | E | (C2)/2 | tion | Mov 12 | | | | | | | ovol | | | | |
| | | manon direct, Borchester, ON | | I | LO. T | | | | | | Water Level SHEAR STRENGTH | | | | | | | | $\overline{}$ | |
| DHPTH | ZO1> <mr< td=""><td>STRATA DESCRIPTION</td><td>STRATA</td><td>WELL</td><td>TY</td><td></td><td>NUMBER</td><td>PLES RECOVERY</td><td>N VALUE (blows)</td><td>BULK DEXS-FY</td><td></td><td colspan="5">◆ S Field Vane Test ▲ Penetrometer ■ 40</td><td colspan="4">st (#=Sensitivity</td></mr<> | STRATA DESCRIPTION | STRATA | WELL | TY | | NUMBER | PLES RECOVERY | N VALUE (blows) | BULK DEXS-FY | | ◆ S Field Vane Test ▲ Penetrometer ■ 40 | | | | | st (#=Sensitivity | | | |
| | Ň | | P O | L O G | Ë | • | Ĕ | R Y | or RQD | S <u>I</u> | | | | | | WL | | | | |
| (m) -0 - | (m) 267.8 | | T | | | | | (mm) or (%) | (%) | Y kN/m3) | | | N Va 0 | alue 20 | | Dyr 30 | amic | Cor 0 | ne | |
| L | | TOPSOIL - 300 mm | 1/. 1/1/2. 1/1 | | | | | | | | Ш | | | | Ш | | | Ш | Ш | |
| - - - | 267.5 | SAND - brown, fine to medium sand, trace silt, compact, moist to very moist | | | | GB : | SA 1 | | | | | 0 | | | | | | | | |
| - - - | | | | | M | GB : | SA 2 | | | | | • | | | | | | | | |
| - 2 - | | | | | | GB : | SA 3 | | | | | | | Φ | | | | | - | |
| - - - 3 | 264.8 | End of test pit at 3.0 m bgs. | | | | | | | | | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | | | |
| - - - | | | | | | | | | | | | | | | | | | | | |
| 4 - - | | | | | | | | | | | | | | | | | | | - | |
| - - 5 | | | | | | | SAMI | ol E I i | EGEND | | | | | | | | | | | |
| 1) Te m 2) Te 3) Te 4) be | NOTES 1) Test pit interpretation requires assistance by EXP before use by others. Test pit log must be read in conjunction with EXP Report LON-21008138-A0. 2) Test pit is based on observations of the excavator resistance. 3) Test pit caved upon completion of excavation. 4) bgs denotes below ground surface. 5) Geodetic elevation surveyed using a SOKKIA GCX2 Receiver. SAMPLE LEGEND AS Auger Sample Rock Core (eg. BQ, NQ, etc.) OTHER TESTS G Specific Gravity H Hydrometer S Sieve Analysis Y Unit Weight F Field Permeability K Lab Permeability K Lab Permeability WATER LEVELS Apparent Artesian (see Notes) | | | | | | | | | | | | | | | | | | | |

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TP13

| PR | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | |
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| | | uburn Developments Inc. | | DAT | | | 4: | | | TUM <u>Geodetic</u> |
| LO | _ | Marion Street, Dorchester, ON | | DATI | ES: I | | | May 12 | | Water Level |
| | ZO−−1 ≻ <mr< td=""><td>STRATA DESCRIPTION</td><td>STRATA P</td><td>WELL L</td><td>TYPE</td><td>N U M B E R</td><td>PLES RECOVERY</td><td>N VALUE (blows) or</td><td>אררש ארכש</td><td>SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane 40 80 kPa Atterberg Limits and Moisture</td></mr<> | STRATA DESCRIPTION | STRATA P | WELL L | TYPE | N U M B E R | PLES RECOVERY | N VALUE (blows) or | אררש ארכש | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane 40 80 kPa Atterberg Limits and Moisture |
| (m) | (m) | | L O T | LOG | E | R | R Y (mm) or | RQD (%) | | W _P W W _L → O I SPT N Value × Dynamic Cone |
| -0- | 265.2 | TOPSOIL - 250 mm | 7 <u>1 1</u> 8. ·7/ | | | | (%) | | (kN/m3) | 10 20 30 40 |
| - | 265.0 | SILTY SAND - brown/grey, loose, wet | | | GE | SA 1 | | | | |
| - | 264.5 | SILT TILL - grey, some clay, wet sand layering, cobbles, compact, moist | 99 | | | SA 2 | | | | |
| -1 | | | | | \mathbb{N}^{G} | 5 3A 2 | | | | |
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| _ | | | | | | | | | | |
| _ | | | | | | | | | | |
| -4 | 261.2 | | | | | | | | | |
| | | End of test pit at 4.0 m bgs. | | | | | | | | |
| | | | | | | | | | | |
| _ | | | | | | | | | | _ |
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| | | | | | | | | | | |
| NOT | TES | | | | | ┪⊠⊢ | S Aug | EGEND er Samp | | SS Split Spoon ST Shelby Tube |
| 1) To m 2) To 3) To 4) bo | est pit intenset pit intenset be read to be set pit is be set pit openset per set pit openset pit open | rpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. In and water observed near 0.8 m bgs upon complet is below ground surface. evation surveyed using a SOKKIA GCX2 Receiver. | OTHE G Sp H Hy S Sid Y Ur P Fid K La | Rock Core (eg. BQ, NQ, etc.) OTHER TESTS G Specific Gravity H Hydrometer S Sieve Analysis CU Consolidated Drained Triaxial CU Consolidated Undrained Triaxial UU Unconsolidated Undrained Triaxial UU Unconsolidated Undrained Triaxial UU Unconsolidated Undrained Triaxial UC Unconfined Compression K Lab Permeability K DS Direct Shear | | | | | | |
| | | | ✓ Apparent ✓ Measured 🛣 Artesian (see Notes | | | | | | | |

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TP14

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|---|---|---|---|------------------|------------------|---|--|--|----------------------|--|---|---------------------------------|--|----------------|--------------------|------------|----|--|--|--|--|
| PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | | | |
| | | Marion Street, Dorchester, ON | | DAT | ES: | Excava | ation | May 12, | | | | | | Leve | l | | | | | | |
| | Ē | | Τ. | | | | IPLES | | | SHEAR STRENGTH | | | | | | | | | | | |
| DHPTH | Ш ₩₩₩₩₩₩₩₩ | STRATA | ST RAT A | W E L L | Ţ | NUM | RECOVERY | N VALUE (blows) | BULK DE | ▲ P | ▲ Penetrometer | | | | 40 , 80 ķPa | | | | | | |
| - | Ó N | DESCRIPTION | P | LOG | T Y P E | NUMBER | Ė | ` or ´ | DEZS-TY | A | tterb | | erg Limits and Moisture W _P W W _I | | | | | | | | |
| (m) -0 - | (m) 263.1 | | P A | G | | R | (mm) or (%) | RQD (%) | † Y kN/m3) | _ | PT N ' | Value | · · • | \rightarrow | − ⁄nami | с Со 40 | ne | | | | |
| | 262.8 | TOPSOIL - 300 mm | 17 · 71·17 7/1/2 · 7/1/2 | | | | | | | | # | | | | | | ₩. | | | | |
| - - - | 202.0 | SILTY SAND - brown, trace gravel, weathered, loose, moist | | | G | B SA 1 | | | | | o | | | | | | | | | | |
| - −1 | | - becoming grey, compact, very moist to wet near | | | | | | | | | | | | | | | - | | | | |
| - | | 1.0 m bgs | | | G | B SA 2 | | | | | | | 0 | | | | | | | | |
| - | | | | | | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | - | | | | |
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| | | | | | | | | | | | | | | | | | | | | | |
| - | 260.4 | | | | | | | | | | | | | | | | | | | | |
| -3 - - | 260.1 | End of test pit at 3.0 m bgs due to unstable sidewalls. | <u> </u> | | | | | | | | | | | 111 | | | | | | | |
| - 4 | | | | | | | | | | | | | | | | | - | | | | |
| - - | | | | | | | | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| m | est pit inte oust be re | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- | others | s. Test | pit lo | 9 OTH | AS Aug Rock C ER TE | | BQ, NC | , | | | | | T She N Var | | | | | | |
| 2) To 3) To 4) bo | est pit is b est pit cav gs denote | passed on observations of the excavator resistance. The and 1.8 m of water observed upon completion of solelow ground surface. The evation surveyed using a SOKKIA GCX2 Receiver. | | ation. | | H H S Si Y U P Fi K La | ydrome eve Ar nit We eld Per ab Perr | nalysis ight rmeability neability | CI CU UU UU | Conso D Cons J Cons J Unco C Unco S Direc | solidat solidat onsolio onfine | ted D ted U dated d Co | ndra I Und | ined draine | Triaxia ed Tria | | | | | | |
| | | | WATER LEVELS | | | | | | | | otes) | | | | | | | | | | |

TP15

| PR | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | |
|-------------------------|---|--|--|--|--|--|---------------------------------------|--|---|--|----------|--------------------------------------|-----------------------|--|--|--|--|--|--|
| | | uburn Developments Inc. | DATUM <u>Geodetic</u> | | | | | | | | | | | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: E | Excava | ation _ | May 12 | | Water Level | | | | | | | | | |
| DWP-T | Э 2О-⊣⊳<шгп | STRATA DESCRIPTION | שות בוסו | ₩ ⊔⊔ 100 | T Y E | SAM NUM BER | PLES RECOVERY (mm) | N VALUE (blows) or RQD (%) | あつしょ ひにこのートン | ◆ S Field Vane ▲ Penetromete 40 Atterberg Lii | mits and | Sensiti orvane 80 kF Moistu | re | | | | | | |
| (m) -0 - | 266.5 | TOPSOIL - 300 mm | 74 1×. 1/1 | | | | or (%) | | (kN/m3) | | 30 | 40 | 1111 | | | | | | |
| _ | 266.2 | 10PSOIL - 300 mm | 7. · 7. · 7. · . · . · . · . · . · . · . | | | | | | | | | | ## - | | | | | | |
| - | | SAND and GRAVEL - grey, looset to compact, very moist to wet | | | GB | SA 1 | | | | | | | - | | | | | | |
| 1 - - | 265.5 | SILT TILL - grey, some clay, trace gravel, occassional cobble and boulder, wet sand layering, compact, moist to very moist | | | GB | SA 2 | | | | | | | - | | | | | | |
| - 2 - | | | 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | | | | | | | | | | - | | | | | | |
| - - -3 - | 263.0 | | TO THE STATE OF TH | | | | | | | | | | - | | | | | | |
| _ | 200.0 | End of test pit at 3.5 m bgs. | .9.N.X. | | | | | | | | | | | | | | | | |
| - -4 - - | | | | | | | | | | | | | - - - - - | | | | | | |
| 2) To 3) To 4) bo | est pit intenust be rea est pit is be est pit cav | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. ed and water observed near 1.0 m bgs upon completed below ground surface. evation surveyed using a SOKKIA GCX2 Receiver. | | ☑ A □ F OTHE G Sp H Hy S Sie Y Ur P Fie K La WAT | S Aug Rock Co ER TES Decific Idrome Pereve An Orit Wei Orit Peres | ore (eg. I STS Gravity eter alysis ight rmeability velS | BQ, NQ C CI CU UU / DS | SS Split Spoon a, etc.) Consolidation Consolidated Dra J Consolidated Un J Unconsolidated U C Unconfined Com S Direct Shear | VN Inned Trial drained Trial Jndrained pression | riaxial d Triaxial | ample | | | | | | | | |

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TP16Sheet 1 of 1

| PR | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | |
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| | | uburn Developments Inc. | | | | | | | | TUM <u>Geodetic</u> | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Excava | ation _ | May 12 | | Water Level | |
| P | ELEV. | | STRATA | W E L L | | | PLES R E | N | B U L K | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane | |
| DEPTH | ĀT-ON | STRATA DESCRIPTION | P | L LOG | T Y P E | NUMBER | KHCO>HK> | VALUE (blows) or | DEINS-TY | 40 80 kPa Atterberg Limits and Moisture | |
| (m) | (m) 255.8 | | L T | Ğ | | Ř | (mm) or (%) | RQD (%) | T Y (kN/m3) | W _P W W _L → O IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII | |
| -0- | | TOPSOIL - 400 mm | 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7 | | | | | | | | |
| | 255.4 | | : <u>7 (7 : 7</u> | | | | | | | | |
| - | | FILL - SAND AND GRAVEL - dark brown/grey, loose, wet | | | GI | 3 SA 1 | | | | o | |
| - | | | | | \square | | | | | | |
| -1 | | | | | | | | | | - | |
| - | 254.5 | FILL - CLAYEY SILT - dark grey/black, organics, | | | Ц | | | | | - | |
| | 254.2 | firm, wet | | | X GI | 3 SA 2 | | | | Φ | |
| | | CLAYEY SILT TILL - grey, some sand and gravel, occassional cobble and boulder, wet sand | | | \bigcup | | | | | | |
| | | layering, stiff, moist | | | X GI | SA 3 | | | | | |
| -2 | | | | | \vdash | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| _ | | | | | | | | | | | |
| -3 | 252.8 | | | | | | | | | | |
| - | | End of test pit at 3.0 m bgs. | | | | | | | | | |
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| 5 | | | | | | | | EGEND | | | |
| 1) Te | est pit inte | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- | others | . Test | pit lo | ຸ □ F | | er Samp ore (eg. STS | | SS Split Spoon ST Shelby Tube VN Vane Sample | |
| 2) Te 3) Te 4) bo | est pit is b est pit cav gs denote: | ased on observations of the excavator resistance. assed on observations of the excavator resistance. ed and water observed near 1.3 m bgs upon comple s below ground surface. evation surveyed using a SOKKIA GCX2 Receiver. | ation. | ↑ Unit Weight UU Unconsolidated Undrained Triaxial P Field Permeability UC Unconfined Compression | | | | | | | |
| | | | | K Lab Permeability DS Direct Shear WATER LEVELS ▼ Apparent ■ Measured ▲ Artesian (see Notes | | | | | | | |

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TP16A

| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | T 6 1 4 | | _ | | 040 | 0044 | | | | | |
|--------|--|---|--|------------------|------------------|------------|------------------|-------------------|--------------|--------------|----------------|-------|----------------|----------------|------------|----------------|--------------|----------|----------|------------------|
| | _ | Hunter Farm | | | | | | | | | | | | | | ·210 | <u>U813</u> | 8-8 | <u> </u> | - |
| | · · · · · · | Auburn Developments Inc. | | D 4 T | FO: | | _4: | | | ATU | M _ | | | | | 1 | | | | - |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | E5: | | | May 12 | | | | | | | | | | | | |
| | E L | | ļ ş | | | SAM | IPLES | ı | BULK | | S F | | | | TRE est | | TH Sens | itivit | lv) | Ш |
| P | ZO1> <mr< td=""><td></td><td>ST R A T</td><td>W E L L</td><td></td><td>١</td><td>RECOVERY</td><td>N</td><td>k</td><td></td><td></td><td>etro</td><td></td><td></td><td></td><td></td><td>vane</td><td></td><td>.,</td><td>Ш</td></mr<> | | ST R A T | W E L L | | ١ | RECOVERY | N | k | | | etro | | | | | vane | | ., | Ш |
| ОШР⊢Т | Ť | STRATA | Ā | | Ţ | N | Ö | VALUE | ₽ | | | | | 10 | | 1 | 80 | | | ╛╽ |
| н | Ö | DESCRIPTION | l P | LOG | T Y P E | NUMBER | Ě | (blows) or | N S | | Att | erbe | _ | | | | Mois | ture | | Ш |
| | (m) | | þ | Ğ | | Ř | (mm) | RQD (%) | ロ田区の一下と | | o Da | | | ⊢- | W ' | ⊣- | ! - | O | | Ш |
| (m) | 256.0 | | ' | | | | or (%) | 1 | Y (kN/m3) | | | | | | | | | Con 0 | le ' | |
| -0- | | TOPSOIL - 300 mm | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | | | | | | | Н | \blacksquare | Н | \blacksquare | \blacksquare | | \blacksquare | Н | Н | H | П |
| | 255.7 | | <u> </u> | | Ц | | | | | Щ | | Ш | | | | | ш | Ш | Ħ | 11 |
| - | | SAND and GRAVEL - grey, trace silt, compact, moist | 0.00 | | M_{-} | | | | | Ш | | Ш | \pm | | | | Ш | | \pm | ┨┨ |
| - | | | 0.00 | | \ Gi | SA 1 | | | | Н | $^{+}$ | Н | + | + | Н | + | | Н | + | ┨┨ |
| - | | | 0.000 | | \vdash | | | | | Ш | | Ш | Ħ | Ħ | | | | Ш | Ħ | 14 |
| -1 | | | 0.000 0.000 | | | | | | | Ш | | Ш | Ш | | | | | | Ш | ┨ |
| ' | | | 0 0 | | | | | | | Н | + | Н | + | + | Н | + | + | Н | + | $\ \ $ |
| | 254.7 254.6 | SILT TILL, grey, trace to some clay, wet sand | 97 | | | | | | | Ш | | Ш | Ħ | | | | | | Ħ | 11 |
| | 234.0 | layering, compact, moist to very moist | | | | | | | | Ш | | ш | | | ш | | | ш | | Ħ |
| - | | End of test pit at 1.4 m bgs. | | | | | | | | | | | | | | | | | | $ \cdot $ |
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| -4 | | | | | | | | | | | | | | | | | | | | - |
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| - | | | | | | | | | | | | | | | | | | | | $ \cdot $ |
| 5 | | | | | | SAM | PLF! | EGEND | | <u> </u> | | | | | | | | | | 니 |
| NO1 | TES . | | | | | | AS Aug | jer Samp | | SS | | t Sp | oon | | | | Shelb | | | |
| 1) To | est pit inte | erpretation requires assistance by EXP before use b | y others | s. Test | pit lo | n I | Rock C ER TE | ore (eg. STS | BQ, NG | ≀, etc | .) | | | | Ш | VN ' | √ane | San | nple | , |
| 2) To | iust be rea est pit is b | ad in conjunction with EXP Report LON-21008138- ased on observations of the excavator resistance. | AU. | | | G S | pecific | Gravity | | Cons | | | | ! | - J | F! | :_1 | | | |
| (3) To | est pit cav gs denote | ased on observations of the excavator resistance. ed and water observed near 1.3 m bgs upon comples below ground surface. | etion of | excava | ation. | | ydrome eve Ar | | | D Co J Co | | | | | | | ial axial | | | |
| [5) G | eodetic el | evation surveyed using a SOKKIA GCX2 Receiver. | | | | γ υ | nit We | | Ul | | con | solid | lated | d Ur | ıdrai | ned | Triax | ial | | |
| | | | | K La | ab Perr | neability | | S Dir | | | | unpl | U331 | σΠ | | | | | | |
| | | | | WATER LEVELS | | | | | | | | tes) | , | | | | | | | |

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TP16B

| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | |
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| | · · · · · · | auburn Developments Inc. | | | | _ | | | | TUM <u>Geo</u> | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | DAT | ES: | Excava | ation _ | May 12 | | Mater Level | | | | | | | |
| ₽ | ZO1> <mr< td=""><td></td><td>ST RATA</td><td>¥</td><td></td><td>SAM</td><td>IPLES R</td><td>N</td><td>ארכש</td><td></td><td>AR STRENGTH ane Test (#=Sensitivity) eter Torvane</td></mr<> | | ST RATA | ¥ | | SAM | IPLES R | N | ארכש | | AR STRENGTH ane Test (#=Sensitivity) eter Torvane | | | | | |
| DEPTH | Ą | STRATA | 🛣 | W L L | I | N | မြ | VALUE | Б | | 40 , 80 kPa | | | | | |
| Ĥ | ő | DESCRIPTION | P | L OG | T Y P E | NUMBER | RECOVERY | (blows) | NZ0 | | Limits and Moisture | | | | | |
| | | | 뉴 | Ğ | - | Ř | | RQD | ロயヱめート> | 1 | W _P W W _L | | | | | |
| (m) | (m) 255.8 | | ' | | | | (mm) or (%) | (%) | Y (kN/m3) | SPT N Val | ue X Dynamic Cone 20 30 40 | | | | | |
| -0 - | | TOPSOIL - 300 mm | 71 18 17 | | | | | | , | | | | | | | |
| - | 255.5 | | 1 | | Ц | | | | | | | | | | | |
| - | | FILL - SILTY SAND - dark brown/black, loose/compact, moist | | | M | | | | | | | | | | | |
| - | | , | | | ∭GE | SA 1 | | | | | | | | | | |
| _ | | | | | \Box | | | | | | | | | | | |
| | | | \bowtie | | | | | | | | | | | | | |
| -1 | 254.6 | | \bowtie | 1 | | | | | | | | | | | | |
| - | | SILT TILL, grey, trace to some clay, wet sand | | | | | | | | | | | | | | |
| | 254.4 | layering, compact, moist to very moist End of test pit at 1.4 m bgs. | | 1 | | | | | | | | | | | | |
| - | | End of test pit at 1.4 in bgs. | | | | | | | | | | | | | | |
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| 1.5 | | | | | | | | EGEND Jer Samp | le Ø | SS Split Spoor | n ST Shelby Tube | | | | | |
| 1) Te | | erpretation requires assistance by EXP before use by | others | : Test | nit lo | , | Rock Č | ore (eg. l | | | ☐ VN Vane Sample | | | | | |
| m | nust be rea | ad in conjunction with EXP Report LON-21008138-A | \0. | . 1 UOL | hir iof | ΊΟΙΗ | ER TE | STS Gravity | <u></u> | Consolidation | | | | | | |
| 3) T | est pit cav | ased on observations of the excavator resistance. ed and water observed near 1.3 m bgs upon comple s below ground surface. | tion of | excava | ation. | HH | ydrome | eter | CE | O Consolidated | Drained Triaxial | | | | | |
| 4) by 5) G | gs denote: leodetic el | s below ground surface. evation surveyed using a SOKKIA GCX2 Receiver. | | | | S Si | Undrained Triaxial ed Undrained Triaxial | | | | | | | | | |
| | | | | | | Y Unit Weight P Field Permeability K Lab Permeability WATER LEVELS UU Unconsolidated Undrained Triaxial UC Unconfined Compression DS Direct Shear | | | | | | | | | | |
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| | | | | Appare | | ▼ Me | easured | ▲ Artesian (see Notes) | | | | | | | | |

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| PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | | | | |
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| CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | | | | | |
| | | Marion Street, Dorchester, ON | Excav | ation _ | Augus | | | | | | | | | eve | _ | | | | _ | | | |
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| Н | A T O N | DESCRIPTION | P Q T | LOG | Y P E | NUMBER | RECOVERY | (blows) or | DE NS- | | A | tte | rbei | | | | an W | | lois | ture |) | $ \ $ |
| () | (m) | | R | (mm) | RQD (%) | | ١. | SF | РТ | N V | | H | ╼ | - | | mic | Col | ne | $ \ $ | | | |
| (m) −0 − | 255.2 | TOPOO! 400 mm | 74 15. 14 | | ļ.,. | | (%) | 1 | (kN/m3) | | - '- | 10 | | | 20 | -` | 30 | | | 0 | ╧ | Ц |
| - | | TOPSOIL - 400 mm | 1/. 11/ | | | | | | | Ħ | | Ħ | | Ħ | Ħ | \sharp | # | | | | Ш | 1] |
| - | 254.8 | | 1.11 | | | | | | | Ħ | | Ħ | | Ħ | Ħ | \sharp | # | | | | Ш | 1 |
| _ | | SAND and GRAVEL -grey, coarse-grained, loose to compact, moist to very moist | 0.00 | | | | | | | Ħ | | Ħ | \parallel | | \parallel | \pm | \pm | | | | Ш | <u> </u> |
| | | | 0.00 | | | | | | | Ħ | | H | \parallel | | | \pm | \pm | | | | Ш | <u> </u> |
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| <u> </u> | | | 0.0.0 | | | | | | | H | | H | H | H | H | \pm | \pm | \parallel | | | Ш | <u> </u> |
| | | | 0000 | | | | | | | H | | | | | | \pm | \pm | | | | Ш | $\frac{1}{2}$ |
| | 253.7 | End of test pit at 1.5 m bgs. | i i i | | | | | | | Н | | | | | | Ш | Ш | | | | Ш | \mathbb{H} |
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| <u>NO1</u> | <u>ES</u> | | | | | ⊣ ⋈ / | AS Aug | ger Samp ore (eg. | | | | plit | Spc | on | | | | | helb /ane | | ube mple | |
| ĺ'n | nust be re | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- <i>i</i> | others | s. Test | pit lo | g oth | ER TE | STS | | | | | | | | <u>ڪا</u> | . v | . • V | ai ic | Jai | ipic | |
| 2) Te 3) Te | est pit is b est pit ope | pased on observations of the excavator resistance. | | | | HH | ydrome | | CI | D C | cons | soli | | d E | | | d Tri | | | | | |
| 4) bo | gs denote | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | γ υ | eve Ar nit We | ight | Ül | Uυ | Inco | ons | olida | ate | d U | ndr | aine | ed T | axial Triax | | | |
| | | | | | | P Fi | P Field Permeability UC Unconfined Compression K Lab Permeability DS Direct Shear | | | | | | | | | | | | | | | |
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| | DRO IECT Munter Form | | | | | | | | | | | | | | | | | | | | |
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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | | | | | |
| CLIENT Auburn Developments Inc. DATUM Geodetic LOCATION Marion Street, Dorchester, ON DATES: Excavation August 4, 2021 Water Level | | | | | | | | | | | - | | | | | | | | | | |
| | CATION | Marion Street, Dorchester, ON | xcava | auon _ | Augus | | 21 | | | | | | | | | | | ᅱ | | | |
| | E L | | ş | | | SAM | IPLES | | BULK | ١. | s ı | | | | | REN st (# | | | itivi | itv) | Ш |
| P | Ž. | | ST RAT | W E L L | | ١ | R | N | k | | | netr | | | | | | /ane | | ٠٠, | Ш |
| DEPTH | M-M>40z | STRATA | I | t | Ţ | N | Ö | VALUE (blows) | P | | | | | 40 | | | | 80 I | | | ╛ |
| H | Ó N | DESCRIPTION | P L OT | LOG | T P E | NUMBER | RECOVERY | or | ロ田区の一下と | | At | terb | erg | | | an W | | loist | ture | • | Ш |
| | (m) | | G | | R | (mm) | RQD (%) | ļţ | | SP | TN | Val | Ė | -0 | , D) | _ | mic | Col | ne | Ш | |
| (m) -0 - | 255.9 | | 1.47. % | | | | `or ´ (%) | | (kN/m3) | | | 10 | Va. | 20 | | 30 | | | 0 | | Ц |
| | | TOPSOIL - 300 mm | \(\frac{1}{2}\frac{1}{ | | | | | | | Н | + | + | ${\mathbb H}$ | Н | | H | $^{+}$ | + | | Н | $\ \ $ |
| | 255.6 | SILTY SAND , brown, trace gravel, trace | | | | | | | | Н | + | + | ${\mathbb H}$ | Н | + | \mathbb{H} | $^{+}$ | | | Н | + |
| - | | cobbles, loose to compact, moist | | | | | | | | П | \blacksquare | $\downarrow \downarrow$ | Ħ | Ħ | | | \parallel | | | | 11 |
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| - | | | | | | | | | | Н | + | + | H | Н | | | $^{+}$ | | | | 11 |
| -1 | 254.9 | SANDY SILT , grey, fine-grained, trace clay, | | | | | | | | Н | + | + | H | \mathbb{H} | | \mathbf{H} | + | | | \blacksquare | \dashv |
| - | | loose to compact, moist | | | | | | | | П | | Ħ | Ħ | Ħ | 1 | | Ħ | | | Ш | 14 |
| _ | 054.4 | | | | | | | | | Ш | | | Ħ | Ш | | | П | | | | 11 |
| | 254.4 | End of test pit at 1.5 m bgs. | 1.1.1. | | | | | | | Н | | | | Ш | | | Ш | | | Ш | \dagger |
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| lím | ust be re | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- | y others 40. | s. rest | pit log | ОТН | ER TE | STS | • | | , | الماما | | | | | | | | • | |
| 2) Te 3) Te | est pit is b est pit ope | pased on observations of the excavator resistance. en and dry upon completion of excavation. s below ground surface. | | | | G Specific Gravity H Hydrometer S Sieve Analysis Unit Weight C Consolidation CD Consolidated Drained Triaxial CU Consolidated Undrained Triaxial UU Unconsolidated Undrained Triaxial | | | | | | | | | | | | | | | |
| 4) bo 5) G | js denote eodetic el | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver | | | | | | | | | | | | | | | | | | | |
| | 5, SSSSSSS SISTABOTO SULTOYOU GOTT OF TOO TOO TOO TOO TOO TOO TOO TOO T | | | | | | | | P Field Permeability UC Unconfined Compression K Lab Permeability DS Direct Shear | | | | | | | | | | | | |
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| PR | PROJECT_Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | _ | | |
| CL | IENT _A | Auburn Developments Inc. | | | | TUM _ | | etic | | | _ | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Exc | avation | Augus | t 4, 202 | 21 | _ Wa | ter Lev | /el | | _ |
| D | ELEV | STRATA | w | | S | AMPLES R | S | B U L K | | eld Var | e Test | ENGTH (#=Sensi | | | |
| DHPTH | | | À | W E L | ۱. | | RECOVERY | N VALUE | l | ▲ Pene | | | Torvane | | Ш |
| Ť H | AT-OZ | STRATA DESCRIPTION | | | Y P E | N N E | ĬΙΑ | (blows) | DENS-TY | Atte | | 0 imits a | 1 08 and Moist | | H |
| | Ň | | <u>P</u> | G F | E | | | or RQD | Ŝ | 7 1110 | _ | V _P W | | | Ш |
| (m) | (m) 256.6 | | P | | | ' | (mm or (%) | (%) | T Y (kN/m3) | • SPT 10 | | _ | ─l Dynamic 30 4 | | |
| -0- | | TOPSOIL - 300 mm | 1/. 1/. | | | | (70) | | ,, | | | | | | П |
| | 256.3 | SILTY SAND , brown, fine to medium-grained, | | | | | | | | | \mathbb{H} | | | | $\left\{ \ ight]$ |
| _ | | moist grained, | | | | | | | | | | | | | 11 |
| - | | -becoming grey, fine-grained and very moist at 0.6 | | | | | | | | | Ш | | | | 11 |
| - | | m bgs | | | | | | | | | Ш | | | | 11 |
| -1 | 255.6 | End of test pit at 1.0 m bgs. | | | | | | | | | ш | | | | Н |
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| NO1 | ES | | | | | $\neg \mid \boxtimes$ | AS Au | .EGEND ger Samp | | SS Split | Spoon | | ST Shelb | | |
| 1) Te | est pit inte | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | others | s. Test | pit Ic | |] Rock (THER TE | Core (eg. ESTS | BQ, NG | , etc.) | | Ш | VN Vane | Sample | |
| 2) Te | est nit is h | ad in conjunction with EAP Report LON-21008138-A pased on observations of the excavator resistance. an and dry upon completion of excavation. | ιυ. | | | G | Specific | Gravity | | Consolida | | rained ⁻ | Triavial | | |
| 4) bo | as denote: | en and dry upon completion of excavation. s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | s | H Hydrometer CD Consolidated Drained Triax S Sieve Analysis CU Consolidated Undrained Tr | | | | | | | | |
| J) G | couelic el | evalions surveyed using a SURNIA GUAZ RECEIVER. | | | | Y Unit Weight UU Unconsolidated Undrained T P Field Permeability UC Unconfined Compression | | | | | | | | ıaı | |
| | | | | | | | Lab Per ATER LI | meability =VFLS | DS | S Direct S | hear | | | | |
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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | |
| | ` | <u>-</u> | | | | letic | _ | | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Ex | cava | ition _ | Augus | t 4, 202 | 21 Wa | ater Level | - | |
| , | ZOIV <mr< td=""><td></td><td>;</td><td>SAM</td><td>PLES R</td><td></td><td>BU LK</td><td>S Field Va</td><td>AR STRENGTH ne Test (#=Sensitivity)</td><td>П</td></mr<> | | ; | SAM | PLES R | | BU LK | S Field Va | AR STRENGTH ne Test (#=Sensitivity) | П | | | | |
| Ошр⊢т | V A | | ST RAT | ¥ L L | _ | | N | RHCONHRY | N VALUE | l | ▲ Penetrome | | | |
| Ť | Ĭ | STRATA DESCRIPTION | A | | Y P E | | ZUEBUR | Ϋ́ | (blows) | DENS-TY | | 40 , 80 kPa Limits and Moisture | 1 | |
| | Ň | BEOGIAI NON | P Q | L OG | E | | E | Ŕ | or RQD | Ŝ | | W _P W W _L | | |
| (m) | (m) | | ¥ | | | | | (mm) or | (%) | | SPT N Value | | | |
| -0- | 255.2 | TOPSOIL - 300 mm | 74 1×. ·7 | <u> </u> | + | + | | (%) | | (kN/m3) | 10 ; | 20 30 40 | Н | |
| - | 254.9 | | 17. 11.17 | | | | | | | | | | $\mid \cdot \mid$ | |
| - | 201.0 | SILTY SAND , grey, fine to medium-grained, | | | | | | | | | | | | |
| _ | 254.6 | loose to compact, very moist | | | | | | | | | | | | |
| | | SAND AND GRAVEL , grey, fine-grained, loose to compact, wet | 0.00 | | | | | | | | | | | |
| | | , . | 0 - 0 0 0 0 | | | | | | | | | | $\lfloor $ | |
| − 1 | 254.0 | | 0000 | | | | | | | | | | | |
| | 204.0 | End of test pit at 1.2 m bgs. | e · · · · o | | | | | | | | | | Ħ | |
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| - | | | | | | | | | | | | | - | |
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| -2 | | | | | | | | | | | | | $ \cdot $ | |
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| -4 | | | | | | | | | | | | | $ _{\perp}$ | |
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| 5 | | <u> </u> | | | | | | | EGEND | I | l | | 닉 | |
| <u>NO1</u> | | | | | | | | | er Samp ore (eg. | | SS Split Spoon O. etc.) | ST Shelby TubeVN Vane Sample | | |
| lím | nust be rea | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138 | ÁΩ | s. Test | t pit lo | og | OTHE | R TE | STS | | • | | | |
| 2) To 3) W | est pit is b /ater obse | ased on observations of the excavator resistance. Fived near 0.6 m bgs upon completion of excavation s below ground surface. | | | | | H Hy | /drome | | CI | Consolidation Consolidated [| | | |
| 4) bo 5) G | gs denote eodetic el | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver | <u>.</u> | | | | | eve An nit Wei | ialysis ight | | | Jndrained Triaxial d Undrained Triaxial | | |
| ĺ | | · - | | | | | ΡFie | eld Per | meability neability | y U | C Unconfined Co S Direct Shear | | | |
| | | | | | | ١ | NATI | ER LE | VELS | | | _ | | |
| | | | | | | | ∇ A | ppare | nt | ▼ Me | easured | Artesian (see Notes) | | |

| • | * | (| О. |
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TP205

| PR | OJECT | Hunter Farm | | | | | | | PF | ROJECT NO. LON-21008138-A0 |
|-------------------------------|---|---|--|------------------|------------------|--|---|---|----------------------------------|---|
| | ` | auburn Developments Inc. | | | | | | | | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: E | | | Augus | | |
| Đ | | | STRAT | W E L L | | | PLES R E | N | B U L K | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) Penetrometer Torvane |
| DHPLI | AT-ON | STRATA DESCRIPTION | A P | LL LOG | T Y P E | NUMBER | RECOVERY | VALUE (blows) or | DENS- | 40 80 kPa Atterberg Limits and Moisture W _P W W _L |
| (m) -0 - | (m) 255.4 | | Ď T | G | | R | (mm) or (%) | RQD (%) | † Y (kN/m3) | SPT N Value |
| - - - - | 254.2 | PEAT , black, fibrous, wet | \$ | | | | | | | |
| - - - - - - | | MARL , grey, mixed alluvial clay/silt, wet | \$ | | | | | | | |
| - -3 - | 251.9 251.8 | SAND AND GRAVEL, grey, wet | 8.555555555555555555555555555555555555 | | | | | | | |
| - -4 - - | | End of test pit at 3.6 m bgs. | | | | | | | | - - - - - |
| 5 | | | 1 | | | | | EGEND | lo [7] | CC Colit Cocoo |
| 1) To m 2) To 3) W 4) bo 5) G | rES est pit intended to the content of the content | erpretation requires assistance by EXP before use be ad in conjunction with EXP Report LON-21008138-, assed on observations of the excavator resistance, erved near 1.2 m bgs, test pit caved upon completions below ground surface. evations surveyed using a SOKKIA GCX2 Receiver | y others A0. n of exca | avation | pit log | OTHI GSI HH! SSI YUI PFI KLa | Rock C ER TE: pecific ydrome eve An nit Wei eld Per | Gravity eter alysis ight meability NELS | BQ, NG CI CI UI y US | SS Split Spoon ST Shelby Tube VN Vane Sample Consolidation Consolidated Drained Triaxial U Consolidated Undrained Triaxial U Unconsolidated Undrained Triaxial C Unconfined Compression S Direct Shear Artesian (see Notes) |

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TP206

| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 | | | | | | | | | | | | | | | | |
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| | - | | | | | | | | | | | | | 2100 | 8138 | -A0 | _ |
| | ` | uburn Developments Inc. | | D 4 T | | | 4: | _ | | TUM | | | | | | | - |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | E5: I | Excava | ation _ | Augus | | 21 | Water Level SHEAR STRENGTH | | | | | | |
| DEPTH | ™>⊄⊢−OZ | | STRAT | W E L L | | | PLES RECOVERY | N | BULK | | Field | Vane 1 meter | Test (| (#=Se Torv | ensiti vane | • • | |
| 1 | I | STRATA DESCRIPTION | Å | | T Y P E | ÜM | ν | (blows) | E | A4 | 40.000 | 40 | ito o | _ | 80 kP | | - |
| •• | N | DESCRIPTION | P | C | E | NUMBER | R | or | ロயヱめート≻ | Αι | .terbei | rg Lim W _P | w \ | | oistui | re | |
| (m) -0 - | (m) 255.5 | | ቅ | | | K | (mm) or (%) | (%) | Ť Y (kN/m3) | | T N V | alue 20 | | ⊣ ¯ Dynar 30 | nic C | one | |
| | | PEAT , black, fibrous, wet | \$ \$ \$ \$ \$ \$ \$ \$ | | | | | | | | | | | | | | ┧╽ |
| | | | \$ \$ \$ | | | | | | | | | | \mathbf{H} | Н | | +H | + |
| | | | \$ | | | | | | | | | Ш | | | Ш | Ш |] [|
| - | | | \$ | | | | | | | | | +++ | \mathbf{H} | | +++ | +H | 11 |
| - | | | <pre></pre> | | | | | | | | | | Ш | Ш | | \blacksquare | 74 |
| -1 | | | \$ | | | | | | | | | Ш | Ш | | | Ш | ╛╛ |
| | | | \$ | | | | | | | | | | ++ | ++ | | + | + |
| - | | | \$ \$ \$ \$ | | | | | | | | | Ш | | | | | 1 1 |
| - | 254.0 | | \$ \$ \$ \$ \$ \$ | | | | | | | | | | | | | +H | - |
| - | | MARL , grey, mixed alluvial clay/silt, wet | \$ \$ \$ \$ \$ \$ | | | | | | | | | Ш | | | | | 4 |
| | | | \$ \$ \$ \$ | | | | | | | | | | | | | | ╛╻ |
| | | | <pre>{</pre> | | | | | | | | | | \mathbf{H} | ++ | | $+\!\!+\!\!+\!\!+$ | -11 |
| -2 | | | <pre></pre> | | | | | | | | | | Ш | Ш | | Ш | 11 |
| - | | | <pre></pre> | | | | | | | | | | | | | + | ┨┨ |
| - | | | \$ | | | | | | | | | | | | Ш | Ш | 4 |
| | | | \$ \$ \$ \$ \$ \$ | | | | | | | | | Ш | Ш | ++ | +++ | +H | 11 |
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| -3 | | | <pre></pre> | | | | | | | | +++ | +++ | ++ | ++ | +++ | + | |
| - | | | <pre></pre> | | | | | | | | | | Ш | | | Ш | 1 1 |
| | | | \$ \$ \$ \$ \$ \$ | | | | | | | | | | | | | | 1] |
| | 252.0 251.9 | SAND AND GRAVEL , grey, wet | \$ | | | | | | | | | | | | | +H | 41 |
| | 201.0 | End of test pit at 3.6 m bgs. | .0.5.0 | | | | | | | | | | | | | | $\dagger \dagger$ |
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| 5_ | | | | | | | | EGEND Jer Samp | | SS 5~ | dit Cna | or | | ST SI | helby | Tubo | |
| <u>NO1</u> | | repretation requires essistance by EVD before the | oth c | T4 | nit I - | IШБ | | ore (eg. l | | SS Sp , etc.) | ли Эро | OH | | | ane S | | |
| m | nust be rea | rpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | 0. 0. | i. rest | pit ioc | ТОТН | ER TE | | 0 | 0 1 | | | | | | | |
| 2) Te 3) W | est pit is b /ater obse | ased on observations of the excavator resistance. rved near 1.5 m bgs, test pit caved upon completion | of exc | avatior | ١. | HH | /drome | | | Consoli) Conso | | | ned T | riaxia | ıl | | |
| 4) bo | gs denotes | rved near 1.5 m bgs, test pit caved upon completion s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | S Sieve Analysis CU Consolidated Undrained Triaxial Y Unit Weight UU Unconsolidated Undrained Triaxial | | | | | | | | | | | |
| ", " | .5546116 GI | S.a Our repositioning a Contract COME MODIVER. | | | | P Field Permeability UC Unconfined Compression | | | | | | | | | | | |
| | | | | | | K Lab Permeability DS Direct Shear WATER LEVELS | | | | | | | | | | | |
| | | | | | | | ER LE Apparei | | ▼ Me | easured | t | Ī | Arte | esian | (see l | Notes | ;) |

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TP207

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|--------------|---|--|--|-------------|-------------|---------------|--------------------|-------------------|-------------|----------------------------------|--|--|--|
| | PROJECT Hunter Farm Project No. LON-21008138-A0 | | | | | | | | | | | | |
| CL | IENT _A | uburn Developments Inc. | | | | | | | _ DA | TUM <u>Geod</u> | letic | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: E | Excava | ation _ | Augus | t 4, 202 | <u>21</u> Wa | ater Level | | |
| | Ę | | | SAM | IPLES | | B | | AR STRENGTH | | | | |
| ₽ | M-M>4H-OZ | | ST RAT | ¥ | | | R | | BULK | ■ S Field Val ■ Penetrome | ne Test (#=Sensitivity) ter ■ Torvane | | |
| Оше⊢т | Å | STRATA | ^ | W L L | Т. | N | RECOVERY | N VALUE | | | 40 , 80 kPa | | |
| н | i | DESCRIPTION | A P | I | T P E | NUMBER | ΙĚ | (blows) | N E | | Limits and Moisture | | |
| | | | Ē | L OG | E | Ē | R Y | or RQD | DEZS-TY | ' | N _P W W _L | | |
| (m) | (m) | | Ť | | | | (mm) | (%) | - | SPT N Value 10 | | | |
| -0- | 255.0 | TOPSOIL - 500 mm | ~ ~ ~ | | П | | (%) | | (kN/m3) | 10 ; | 20 , 30 , 40 | | |
| F | | | \\ \times \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ | | | | | | | | | | |
| _ | | | ~ ~ | | | | | | | | | | |
| | 254.5 | MARL , grey, mixed alluvial clay/silt, wet | \$ 8 8 | | | | | | | | | | |
| | | , 3 , | ~ ~ | | | | | | | | | | |
| - | 254.0 | | \$\$\$\$\$ \$\$\$\$\$ | | | | | | | | | | |
| -1 | 254.0 | SILTY SAND , brown, loose, very moist to wet | | 1 | | | | | | | | | |
| | 253.8 | End of test pit at 1.2 m bgs. | 1344 | 1 | | | | | | | | | |
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| 5 | | | | | | SAM | | GEND | | | | | |
| NOT | TES | | | | | $\boxtimes A$ | AS Aug | er Samp | | SS Split Spoon | | | |
| 1) T | est pit inte | erpretation requires assistance by EXP before use by | | s. Test | pit log | | Rock C ER TE: | ore (eg. STS | BQ, NG | l, etc.) | VN Vane Sample | | |
| 2) T | est pit is b | ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. | | | | G S | pecific | Gravity | | Consolidation | Project Trickiel | | |
| 3) W 4) b | ater obse gs denote | rved near 0.5 m bgs, test pit caved upon completions below ground surface. | of exc | avatior | 1. | S Si | ydrome eve An | alysis | Cl | | Indrained Triaxial | | |
| 5) G | eodetic el | evations surveyed using a SOKKIA GCX2 Receiver. | | | | | nit Wei eld Per | igȟt meabilitv | | J Unconsolidated C Unconfined Co | d Undrained Triaxial Impression | | |
| | | | | | | K La | b Perr | neability | , DS | S Direct Shear | | | |
| | | | | | | | ER LE Apparei | | ▼ Me | easured | ▲ Artesian (see Notes) | | |

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TP208

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| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic | | | | | | | | | | | | | | | | | | |
| | ` | Marion Street, Dorchester, ON | | DAT | EQ. [| - - - - | ation | Augus | | | _ | | | | _eve | | | | _ |
| | | Manor Street, Dorchester, ON | | Augus | | <u>. </u> | _ | | | | | | _ | | = | | | | |
| | ZO1> <mr< td=""><td></td><td>SAM</td><td>PLES</td><td></td><td>אררא</td><td>• 9</td><td>3 Fi</td><td></td><td></td><td></td><td></td><td>NGTI #=Se</td><td>H ensiti</td><td>ivity)</td><td></td></mr<> | | SAM | PLES | | אררא | • 9 | 3 Fi | | | | | NGTI #=Se | H ensiti | ivity) | | | | |
| Ē | Ž | | STRAT | W E L L | | N. | RHCO>HR> | N | k | | | etro | | | | Torv | | • | |
| ОШР⊢Т | Î | STRATA | X | E | Ţ | Ü | Ö | (blows) | E | | | | 4(| | | | 80 ķF | | . ∐ |
| н | Ö | DESCRIPTION | P | LOG | T P E | NUMBER | Ė | or | N Ş | 4 | Atte | erbei | | | san V W | | oistu | re | |
| | (m) | | 호 | G | | R | (mm) | RQD (%) | DWZ%-FY | . ا | e DT | N V | H | · | \rightarrow | I — | nic C | `ono | |
| (m) - 0 - | 255.4 | | · | | | | `or´ (%) | | ı (kN/m3) | | 1(| | 20 | | 3 | | 40 | | Ш |
| | | PEAT , black, fibrous, wet | \$ | | | | | | | \vdash | Н | | Н | + | | $+\!\!+$ | ₩ | | + |
| Ī | | | \$ | | | | | | | | \blacksquare | | | \blacksquare | | + | \Box | | $\exists 1$ |
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| - | | | \$ | | | | | | | \vdash | Н | + | | + | | + | Н | | \mathbb{H} - |
| -1 | | | \$ | | | | | | | Ш | Щ | | | Ħ | | # | Щ | | |
| _ | 254.2 | | \$ \$ \$ | | | | | | | Ш | Ш | | Ш | \dagger | | # | Ш | | |
| | | MARL , grey, mixed alluvial clay/silt, wet | \$ \$ \$ \$ \$ \$ | | | | | | | \vdash | Н | + | Н | $^{+}$ | | + | ₩ | | + |
| | | | \$ \$ \$ \$ \$ \$ | | | | | | | H | П | \perp | Н | \blacksquare | | 4 | Ш | | $\exists 1$ |
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| - | | | \$ \$ \$ \$ \$ \$ \$ | | | | | | | | H | | П | Ħ | | # | Щ | | 7 |
| -3 | | | \$ \$ \$ \$ \$ \$ \$ \$ | | | | | | | Ш | Ш | | Ш | # | | # | Ш | | |
| - | | | \$ \$ \$ \$ \$ \$ \$ \$ | | | | | | | \vdash | Н | | Н | + | | \pm | Н | | H |
| - | | | \$ \$ \$ \$ | | | | | | | \vdash | Н | | | \blacksquare | | + | \mathbf{H} | | |
| - | 251.7 | | \$ \$ \$ \$ \$ \$ | | | | | | | | П | | П | \sharp | | # | Ш | | ┨. |
| | 251.6 | SANDY SILT , brown, loose, very moist | ∴ ∴ ∴ . ∴ . | | | | | | | Ш | Ш | | Ш | \parallel | | 1 | Ш | | Ш |
| , | | End of test pit at 3.75 m bgs. | | | | | | | | | | | | | | | | | |
| - 4 | | | | | | | | | | | | | | | | | | | |
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| 5 | | | | | | CARA | | EGEND | | | | | | | | | | | Щ |
| NOT | TES | | | | | \boxtimes A | S Aug | er Samp | | SS S | | Spo | on | | | | nelby | | |
| 1) T | est pit inte | erpretation requires assistance by EXP before use by | others | . Test | pit log | | Rock C ER TE | ore (eg. STS | BQ, NQ | , etc. |) | | | ļ | ШV | N Va | ane S | ampl | е |
| l 2) T | est pit is b | ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. | | | | GS | pecific | Gravity | | Cons | | | | oin : | .d T | iord- | J | | |
| 3) V 4) b | rater obse | rved near 1.2 m bgs, test pit caved upon completion s below ground surface. | ydrome eve An | alysis | Cl | D Cor J Cor | nsoli | idate | d Ur | ndra | ined | Tria | xial | | | | | | |
| [5) G | ieodetic el | evations surveyed using a SOKKIA GCX2 Receiver. | Y Unit Weight UU Unconsolidated Undrained Triaxial P Field Permeability UC Unconfined Compression | | | | | | | | | | | | | | | | |
| | | | | | | K Lab Permeability DS Direct Shear | | | | | | | | | | | | | |
| | | | | | | | ER LE | | ▼ Me | easur | red | | Ī | | Artes | sian | (see | Notes | s) |

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TP209

| | _ | Hunter Farm | | | | | | | | | LON-21008138-A | <u> </u> |
|--|--------------|---|---|-------------|------------------|--------|-------------------|--------------------------------|--------------|--|---|--------------|
| | | Auburn Developments Inc. | | | | | | | | ATUM <u>Geo</u> | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Excava | ation _ | Augus | t 4, 202 | <u>21</u> W | ater Level | |
| | Ē | | | SAN | IPLES | | B U L K | | AR STRENGTH | | | |
| Б | M-M-02 | | ST RATA | W | | | R | N | L K | ■ S Field Va | ne Test (#=Sensitivit eter ■ Torvane | ty) |
| DHPH | Ă | STRATA | 🛊 | W L L | т | N | Ş | VALUE | l | | 40 80 kPa | |
| Ĥ | Ö | DESCRIPTION | P | | T Y P E | NUMBER | RECOVERY | (blows) or | K | Atterberg | Limits and Moisture | _ |
| | | | P | L O G | = | E | | RQD | DENS-TY | | W _P W W _L | |
| (m) | (m) 255.4 | | | | | | (mm) or (%) | (%) | Ý (kN/m3) | SPT N Valu | ue × Dynamic Con 20 30 40 | ne |
| -0 - | 200.4 | TOPSOIL - 300 mm | 7/1/2 · · · · · · · · · · · · · · · · · · · | | | | (70) | | (KIWIIIO) | | | |
| - | 255.1 | | 17. 71.17 | 1 | | | | | | | | - - |
| - | | SILTY SAND , brown, loose to compact, very | 1:1 |] | | | | | | | | Ш- |
| _ | | moist | | | | | | | | | | Ш. |
| | | | | 1 | | | | | | | | \coprod |
| | 254.4 | | | | | | | | | | | \mathbb{H} |
| _1 | 201.1 | End of test pit at 1.0 m bgs. | 1 | | | | | | | | | *** |
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| J | | | | | | | | EGEND Jer Samp | | SS Split Spoor | n ■ ST Shelby Tu | ıhe |
| NOT | | erpretation requires assistance by EXP before use b | nv other | s Toet | nit lo | . Ⅲ F | Rock C | ore (eg. | BQ, NC | | ☐ VN Vane San | |
| ĺm | ust be rea | ad in conjunction with EXP Report LON-21008138- based on observations of the excavator resistance. | -A0. | ∍. 1€Sl | ριι Ι <i>Ο</i> (| ТОІН | ER TE | STS Gravity | C | Consolidation | | |
| 3) Te | est pit ope | nased on observations of the excavator resistance. and dry upon completion of excavation. | | | | HH | ydrome | eter | CI | D Consolidated I | | |
| 4) bo | is aenote: | s pelow ground surface. | r | | | | | | | | | |
| 4) bgs denotes below ground surface. 5) Geodetic elevations surveyed using a SOKKIA GCX2 Receiver. S Sieve Analysis | | | | | | | | | | | | |
| 0, 0 | eodetic el | evations surveyed using a SOKKIA GCX2 Receiver | | | | PFi | eld Pei | ignt meability neability | y U | O Unconsolidate C Unconfined Co S Direct Shear | | |

TP210

| | _ | Hunter Farm | | | | | | | | ROJECT NO. <u>LON-21008138-A0</u> |
|-----------------|---|--|---------------------------------|-------------|------------------|----------|-------------------|------------------------------------|------------------|--|
| CL | IENT _A | uburn Developments Inc. | | | | | | | | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Exc | avatior | Augus | t 4, 202 | 21 Water Level |
| , | ZO1> <mr< td=""><td></td><td>STRAT</td><td>w</td><td></td><td>S</td><td>AMPLE</td><td></td><td>B U L K</td><td>SHEAR STRENGTH S Field Vane Test (#=Sensitivity)</td></mr<> | | STRAT | w | | S | AMPLE | | B U L K | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) |
| ОШР⊢Н | V A | | A | W E L | l _ | ١, | RECOVERY | N | | ▲ Penetrometer ■ Torvane |
| Ή | I | STRATA DESCRIPTION | Å | | T Y P E | | ۸ آ ۱ | (blows) | Ĕ | 40 , 80 kPa Atterberg Limits and Moisture |
| | N | DESCRIPTION | P | G C | E | | N COVERY | or RQD | DENS-TY | W _P W W _L |
| (m) | (m) | | P P | | | ' | (mn | 1) (%) | ΙŢ | ● SPT N Value × Dynamic Cone |
| -0 - | 256.4 | DEAT block fibrous wet | ~ <i>~</i> | | +- | | (% | <u> </u> | (kN/m3) | 10 20 30 40 |
| | | PEAT , black, fibrous, wet | \$ | | | | | | | |
| | | | \$ | | | | | | | |
| | | | \$ | | | | | | | |
| - | | | 5 5 5 6 | | | | | | | |
| - | | | <pre></pre> | | | | | | | |
| -1 | 255.4 | MARL , grey, mixed alluvial clay/silt, wet | \$ \$ \$ \$ | | | | | | | |
| - | | marke, groy, mixed and viai didy/one, wee | <pre>\$ { { } { } { } { }</pre> | | | | | | | |
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| -3 | | | \$ | | | | | | | |
| - | | | 5 | | | | | | | |
| - | 252.9 | | \$ \$ \$ \$ | | | | | | | |
| | 252.8 | SILTY SAND , brown, loose, wet End of test pit at 3.6 m bgs. | | | ++ | | | | | |
| - | | Zild of toot pit at 0.0 iii ogo. | | | | | | | | - |
| -4 | | | | | | | | | | - |
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| 5 | | | | | | | | LEGEND | | |
| <u>NO1</u> | | | | | | ΙП | | uger Sam _l Core (eg. | | SS Split Spoon ST Shelby Tube VN Vane Sample |
| l m | nust he rea | rpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | Λ | | | o. | THER T | ESTS | | |
| (2) To (3) W | est pit is b /ater obse | ased on observations of the excavator resistance. rved near 1.0 m bgs, test pit caved upon completion s below ground surface. | of exc | avatio | n. | | l Hydroi | | CI | Consolidation Consolidated Drained Triaxial |
| 4) bo 5) G | gs denote: ieodetic el | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | S | Sieve / Unit W | Analysis /eight | | J Consolidated Undrained Triaxial J Unconsolidated Undrained Triaxial |
| | | - | | | | l P | Field F | ermeabilit ermeability | y U | C Unconfined Compression S Direct Shear |
| | | | | | | W | ATER I | EVELS | | |
| | | | | | | ∇ | Appa | rent | ▼ M | easured Ā Artesian (see Notes) |

| ex | 0. |
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TP211

| PR | OJECT | Hunter Farm | | | | | | | PE | | IFC | т | NO | , | 1. | ON. | -210 | 081 | 38-/ | <u></u> | \dashv |
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| | - | Auburn Developments Inc. | | | | | | | | | | | Ge | _ | | | <u>-2 IL</u> | <i>,</i> 00 I | 30- | 10 | - |
| | | Marion Street, Dorchester, ON | | DAT | ES: | Excav | ation _ | Augus | | | | | | | | Le | /el | | | | _ |
| | E | | ٦ | | | SAN | IPLES | | В | | | | SH | ΕA | R S | TRI | ENG | тн | | | П |
| ₽ | шш | | STRAT | Ψ | | | | | l L K | | | | ld \ tron | | | | | Sens rvan | | ty) | |
| DEPTH | Å T | STRATA | 1 | W E L L | I | Ŋ | Ğ | N VALUE | l | | | | | 4 | | _ | | | ķPa | | |
| Ĥ | ZO- | DESCRIPTION | ^ P | LOG | T P E | NUMBER | RECOVERY | (blows) or | DE NS- | | Αı | ter | ber | | | | | Mois | ture |) | 11 |
| | (m) | | <u> </u> | Ğ | - | Ŕ | (mm) | RQD (%) | ¦ | | 95 | т т | N Va | H | _ | W 0 | ⊣_ | amic | · Cai | 20 | |
| (m) -0 - | 255.9 | | | | | | `or´ (%) | 1 | (kN/m3) | | <u>ا</u> ت | 10 | • • • | 2 | _ | | 30 | | 40 | | Ш |
| _ | 055.0 | TOPSOIL - 300 mm | 17 · 71·14 | | | | | | | Ħ | | | | | | Ш | | | Ш | Ш | 11 |
| | 255.6 | SAND AND GRAVEL , brown, loose to compact, | 0.00 | | | | | | | L | | | | _ | | | | | Ш | Ш | 1 |
| | | wet | 0.00 | | | | | | | H | | | | | | | | | \coprod | | 1] |
| | | | 0.000 | | | | | | | L | | | \blacksquare | | | Н | \parallel | | \coprod | \pm | }] |
| 1 | 254.9 | | 0000 | | | | | | | \vdash | | | Н | | | \mathbb{H} | + | | ++ | + | $\ \ $ |
| | | End of test pit at 1.0 m bgs. | | | | | | | | | | | | | | | | | | | |
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| _5_ | | | | | | 0.41 | DI E | FOEND | | | | | | | | | | | | | Ц |
| NOT | TES . | | | | | → 🖂 A | AS Aug | EGEND ger Samp | | | | olit S | Spo | on | | | | Shell | | | |
| 1) T | est pit inte | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- | others | s. Test | pit lo | ור | Rock C ER TE | ore (eg. STS | BQ, NG | ≀, et | C.) | | | | | Ш | ۷N | Vane | : Sar | mple | ' |
| l 2) T | est pit is b | ad in conjunction with EXP Report LON-2 1006 136-7 pased on observations of the excavator resistance. Prived near 0.3 m bgs upon completion of excavation. | | | | GS | | Gravity | | | | | tion late | | rain | ed ⁻ | Γriax | tial | | | |
| 4) b | gs denote | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | S Si | eve Ar nit We | nalysis | CI | U C | ons | olid | late | U b | ndra | aine | d Tr | iaxial Triax | | | |
| ´ | | , , , | | | | PFi | eld Pe | rmeability neability | y U | CU | nco | nfir | | Cor | | essi | | u/ | | | |
| | | | | | | WAT | ER LE | VELS | | | | | ıcaı | _ | - | | • | , | | | |
| | | | | | | | ⊏r ∟⊏ Appare | | ▼ M | eas | ure | d | | 7 | Š. | Art | esia | n (se | e No | otes) | , |

TP212

| | _ | Hunter Farm | | | | | | | | OJEC | | | | -2100 | 08138 | 3-A0 | |
|-----------------|---|---|----------------------|------------------|------------------|------------------------------------|--|---|------------------------|---|--|--------------------------------------|------------------|-----------|-----------------|-------------|--------------|
| | · · · · · · · · · · · · · · · · · · · | uburn Developments Inc. | | | | | | | | TUM | | | | | | | — |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Exca | ation ₋ | Augus | t 4, 202 | 21 | | Wate | r Le | /el _ | | | |
| D | ZOID <mr< td=""><td></td><td>STRATA</td><td>м</td><td></td><td>SAI</td><td>MPLES R</td><td></td><td>BULK</td><td></td><td>Field</td><td>HEAR Vane meter</td><td>Test</td><td>(#=S</td><td></td><td>ivity)</td><td></td></mr<> | | STRATA | м | | SAI | MPLES R | | BULK | | Field | HEAR Vane meter | Test | (#=S | | ivity) | |
| Ошр⊢н | Ă | CTDATA | Ā | W E L L | ١. | N | 5 | N VALUE | | ^ P6 | Helio | | | ı ı or | | ٦- | |
| H | ˈˈ | STRATA DESCRIPTION | 1 | | T Y P E | M | ĮΫ | (blows) | Ĕ | Δ1 | tterbe | 4 <u>0</u> rg Li n | nits a | nd M | 80 ķl Ioistu | | - |
| | Ň | | <u>P</u> | L OG | Ē | NUMBER | RECOVERY | or RQD | ロ田宮のートと | '`` | | - | W | | .0.0 | | |
| (m) | (m) | | Þ | | | `` | (mm) or | (%) | Y | ● SF | T N V | ⊢ ′alue | ×ι | ⊣ Dyna | mic C | one | |
| - 0- | 254.9 | DEAT block fibrous wat | ~ ~ | | . | | (%) | | (kN/m3) | . | 10 | 20 | 111 | 30 | 40 | | Н |
| L | | PEAT , black, fibrous, wet | \$ \$ \$ | | | | | | | | | | | | Ш | Ш | Ш |
| | | | ~ ~ | | | | | | | | +++ | | + | + | ₩ | Н | H |
| - | | | \$ \$ \$ | | | | | | | | | Ш | Ш | Ш | Ш | Ш | #1 |
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| 4 | | | \$ \$ \$ | | | | | | | \mathbb{H} | Ш | +++ | +H | + | +++ | ++ | Н |
| -1 | 253.7 | | \$ \$ \$ \$ \$ \$ | | | | | | | | | Ш | | | | Ш | |
| - | 233.1 | MARL, grey, mixed alluvial clay/silt, wet | \$ \$ | | | | | | | | | | | | Ш | Ш | ĦŦ |
| - | | | \$ \$ \$ | | | | | | | | +++ | +++ | + | +++ | +++ | ₩ | \mathbb{H} |
| _ | | | ~ ~ | | | | | | | | Ш | Ш | | Ш | Ш | Ш | Ħ. |
| | | | \$ \$ \$ \$ \$ \$ | | | | | | | | +++ | +HH | +H | | +H | Ш | H |
| _ | | | \$ \$ \$ \$ \$ \$ | | | | | | | | | | | Ш | | Ш | #1 |
| -2 | | | ~ ~ | | | | | | | +++ | +++ | +++ | + | + | +++ | H | H |
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| - | | | \$ \$ \$ | | | | | | | | | | Ш | Ш | Ш | Ш | #1 |
| - | | | \$ \$ \$ \$ \$ \$ | | | | | | | | +++ | | + | + | +++ | Н | H + |
| -3 | 251.9 | Ford of Assat with a 4.0.0 we have done to a server | ~ ~ | | | | | | | | | | | | | | Щ |
| - | | End of test pit at 3.0 m bgs due to cave. | | | | | | | | | | | | | | | - |
| -4 | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | | | | | | |
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| 5 | | | | | | | | EGEND | | _ | | | _ | | | | |
| m | est pit inte nust be rea | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138-A | others | s. Test | pit lo | g OTH | Rock Č IER TE | ger Samp Fore (eg. l STS Gravity | BQ, NC | SS Sp (, etc.) Consol | · | | | | helby ane s | | |
| 3) W 4) bo | /ater obse gs denote: | ased on observations of the excavator resistance. In excavate beyond 3.0 In below ground surface. In evations surveyed using a SOKKIA GCX2 Receiver. | _ | due to | o cav | e. H F S S Y U P F | lydrome lieve Ar Jnit We lield Pe | eter nalysis | CI Cl Ul / UC | Consol Cons Cons Unco Unco Direc | olidate olidate nsolid nfined | ed Dra ed Und ated U I Comp | draine Indrai | d Tria | axial | ıl | |
| | | | | | | | TER LE Appare | | ▼ Me | easure | d | Ā | Art | esian | (see | Notes | s) |

| ex | 0. |
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TP213

| | _ | Hunter Farm | | | | | | | | ROJECT NO. <u>LON-21008138-A0</u> |
|--|--|---|----------------------|-------------|------------------|-------------------|---|--|----------------------------------|--|
| | | Auburn Developments Inc. | | | | | | _ | | ATUM <u>Geodetic</u> |
| LO | CATION | Marion Street, Dorchester, ON | | DAI | ES: | Exca | vation | Augus | | 21 Water Level |
| | ZOD< | | STRATA | w | | SA | MPLES | ; | BULK | SHEAR STRENGTH S Field Vane Test (#=Sensitivity) |
| DE PTH | Ā | | 🍒 | W E L | ١_ | N | RECOVERY | N VALUE | l | ▲ Penetrometer ■ Torvane |
| ΤH | Ĭ | STRATA DESCRIPTION | | | T Y P E | NUMBER | 2 | (blows) | DENS-TY | 40 80 kPa Atterberg Limits and Moisture |
| | Ň | 2-20-1 | <u>P</u> | G C | Ė | | R | or RQD | S L | W _P W W _L |
| (m) | (m) | | Þ | | | -` | (mm) | | - | SPT N Value |
| -0 | 254.7 | PEAT , black, fibrous, wet | ~ ~ ~ | | + | | (%) | | (kN/m3) |) 10 20 30 40 |
| - | | ,,, | \$ \$ \$ \$ | | | | | | | |
| - | 254.2 | | \$ \$ \$ \$ | | | | | | | |
| | 234.2 | MARL , grey, mixed alluvial clay/silt, wet | 2 2 | 1 | | | | | | |
| | | | \$ \$ \$ \$ \$ \$ | | | | | | | |
| | 253.7 | | \$ \$ \$ | | | | | | | |
| 1 | | End of test pit at 1.0 m bgs. | 1 | | | | | | | |
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| 5-1 | | <u> </u> | <u> </u> | <u> </u> | 1 | SA | <u> </u> | <u> </u> EGEND | L | |
| NO1 | | | | | | _ I □ | | ger Samp Core (eg. | | SS Split Spoon ST Shelby Tube Q. etc.) ST Shelby Tube D. VN Vane Sample |
| ĺm | iust be rea | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- | y others 40. | s. Test | t pit lo | ^{og} o⊤ | HER TE | STS | • | · |
| 2) Te | est pit is b ater obse | pased on observations of the excavator resistance. Brived near 0.5 m bgs, test pit caved upon completion | | avatio | n. | Н | Hydrom (| eter | CI | D Consolidated Drained Triaxial |
| 4) bo | gs denote: | s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | S | Sieve Ar Unit We | nalysis eight | | U Consolidated Undrained Triaxial U Unconsolidated Undrained Triaxial |
| | | | | | | ΙÞ | Field Pe | rmeabilit | y U | C Unconfined Compression |
| | | | | | | W | ATER LE | EVELS | | |
| - - - - 1) Te 2) Te 3) W | est pit inte just be rea est pit is b ater obse as denote: | ad in conjunction with EXP Report LON-21008138- <i>i</i> assed on observations of the excavator resistance. erved near 0.5 m bgs, test pit caved upon completions below ground surface. | A0. of exc | | | OT GHS PK | AS Aug Rock C HER TE Specific Hydrom Sieve Ar Unit We Field Per Lab Per | ger Samp Core (eg. STS Gravity eter nalysis eight rmeability EVELS | BQ, NC CI CI UI y UC | Q, etc.) Consolidation D Consolidated Drained Triaxial U Consolidated Undrained Triaxial U Unconsolidated Undrained Triaxial |

TP214

| | PROJECT Hunter Farm PROJECT NO. LON-21008138-A0 CLIENT Auburn Developments Inc. DATUM Geodetic DOCATION Marion Street, Dorchester, ON DATES: Excavation August 4, 2021 Water Level | | | | | | | | | | | | | | | | | | | | | |
|--------------------|--|---|---|------------------|-------------|----------------------|--|----------------------------|-----------------|-----------------------------|---------------|-----------------------------|---------------|--------|--|--|--|--|--|--|--|--|
| | | | | | | _ | | | | | | | | | | | | | | | | |
| LO | CATION | Marion Street, Dorchester, ON | | DAI | ES: | Exc | avatio | n <u>Augus</u> | | | 1 Water Level | | | | | | | | | | | |
| | E | | Ş | | | S | AMPLI | _ | B U K | S S Field | | STREN | | ivity) | | | | | | | | |
| P | ™>4⊢−0 z | | ST RATA | W E L L | | | F | N | k | ▲ Penetro | | • | | vity, | | | | | | | | |
| ОШР⊢Т | Ť | STRATA | Î | E | Ţ | | ן ל | VALUE | ₽ | 1 | 40 | | 80 ķF | | | | | | | | | |
| н | Ö | DESCRIPTION | l P | LOG | Y P E | : | FINANCE NAME OF THE PROPERTY O | (blows) or | Ñ S | Atterbe | | its and W W _I | l Moistu | re | | | | | | | | |
| | (m) | | 卢 | Ğ | | i | ₹ Y (m) | | DENS-TY | ● SPT N \ | . ⊢ | | | | | | | | | | | |
| (m) -0 - | 256.7 | | <u>L'</u> | | | | (% | r (/9) | t (kN/m3) | | 20 | 30 | namic C 40 | | | | | | | | | |
| ١ | | PEAT , black, fibrous, wet | \$ \$ \$ | | | | | | | | +++ | | | | | | | | | | | |
| | | | \$ \$ \$ \$ \$ \$ \$ | | | | | | | | | | | | | | | | | | | |
| - | 256.2 | | ~ ~ | | | | | | | | Ш | | | ш | | | | | | | | |
| - | | SILTY SAND , grey, loose, wet | 1. | i | | | | | | | +++ | | | | | | | | | | | |
| - | | | | | | | | | | | | | | | | | | | | | | |
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| -2 | 254.7 | | | | | | | | | | | | | шЦ | | | | | | | | |
| _ | | End of test pit at 2.0 m bgs. | | | | | | | | | | | | | | | | | | | | |
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| _5_ | | | <u> </u> | | Ш | 1 | 11/2: | 1.505::5 | | | | | | | | | | | | | | |
| NOT | TES. | | | | | | 1 AS A | LEGEND Auger Samp | | SS Split Sp | oon | ■ ST | Shelby | Tube | | | | | | | | |
| 1) To | est pit inte | rpretation requires assistance by EXP before use by | others | s. Test | pit lo | ي ا | Rock | Core (eg. | | | | | Vane S | | | | | | | | | |
| 2) T | nust be rea est pit is b | ad in conjunction with EXP Report LON-21008138-A ased on observations of the excavator resistance. | | | Speci | TESTS fic Gravity | | Consolidatio | | | | | | | | | | | | | | |
| 3 W | ater obse | rved near 0.5 m bgs, test pit caved upon completion s below ground surface. | H Hydrometer CD Consolidated Drained Triaxial S Sieve Analysis CU Consolidated Undrained Triaxial | | | | | | | | | | | | | | | | | | | |
| 5) G | eodetic el | evations surveyed using a SOKKIA GCX2 Receiver. | | | | γ | Unit V | Veight | Ül | J Unconsolio | lated U | ndraine | d Triaxia | I | | | | | | | | |
| | | | | | | | | Permeabilit ermeability | | C Unconfine S Direct She | | ression | | | | | | | | | | |
| | | | | | | W | ATER | LEVELS | | | _ | | | | | | | | | | | |
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| | | Auburn Developments Inc. | | | | | | | | | | G | | | | <u></u> | | 100 | 7.0 | |
| | | Marion Street, Dorchester, ON | | DAT | ES: I | Excava | ation _ | Augus | | | | | | | | evel | | | | |
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| | ELEVA | CTDATA | ST RA T | W E L L | Ţ | Ņ | RECOVERY | N VALUE | K | • | S F Per | ield | ome | eter | Tes | t (#= ■ T | orva | - | | |
| H | A T O N | STRATA DESCRIPTION | A P | | T Y P E | NUMBER | ¥ | (blows) | DE NS- | H | Att | erbe | | 40 Lim | nits | and | | 0 kP istur | | ┨ |
| | | | É | L OG | E | R | | or RQD | S T | | | | | <u> </u> | ╼- | W _L | _ | | | |
| (m) | (m) 266.5 | | Т | | | | (mm) or (%) | (%) | Ť Y (kN/m3) | | | ΓΝ\ Ι <mark></mark> 0 | | је 20 | × | Dyı 30 | nam | ic Co 40 | one | |
| -0- | 266.3 | TOPSOIL - 200 mm | 17. 19.17 | | | | | | | Н | \mathbb{H} | \mathbf{H} | | + | | oxdapprox | Н | \blacksquare | + | \mathbb{H} |
| _ | | SILTY SAND , brown, trace gravel, loose to compact, moist to very moist | 1.3 | | | | | | | H | \mathbb{H} | H | + | + | H | \mathbf{H} | | \mathbb{H} | + | \mathbb{H}^{-} |
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| -3 | | | | | | | | | | Ш | \pm | Ш | | \pm | | | | Ш | | <u> </u> |
| _ | | - becoming wet at 3.0 m bgs | | | | | | | | Ш | Н | Ш | | \pm | | \pm | Ш | Ш | | ∄. |
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| | 263.0 | End of test pit at 3.5 m bgs. | | | \vdash | | | | | Ш | | | | Ш | | | | | | 4 |
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| NO | | | _ | | | | AS Aug | ger Samp ore (eg. | | | | it Sp | oon | 1 | | | | elby ⁻ ne Sa | | |
| ĺ'n | nusť be re | erpretation requires assistance by EXP before use bad in conjunction with EXP Report LON-21008138- | pit log | у отн | ER TE | STS | | | - | م المحاد | _ | | | | | , | -1- | | | |
| (3 X | Vater obse | pased on observations of the excavator resistance. erved near 3.0 m bgs upon completion of excavation | | HH | ydrome | | CI | O Co | onso | | ed [| | | l Tria | | , | | | | |
| 4) b 5) G | gs denote Seodetic el | s below ground surface. evations surveyed using a SOKKIA GCX2 Receivel | · <u>.</u> | | | γ υ | eve Ar nit We | ight | Ul | J Ur | ncon | solic | date | d U | ndra | | d Tri | ial axial | | |
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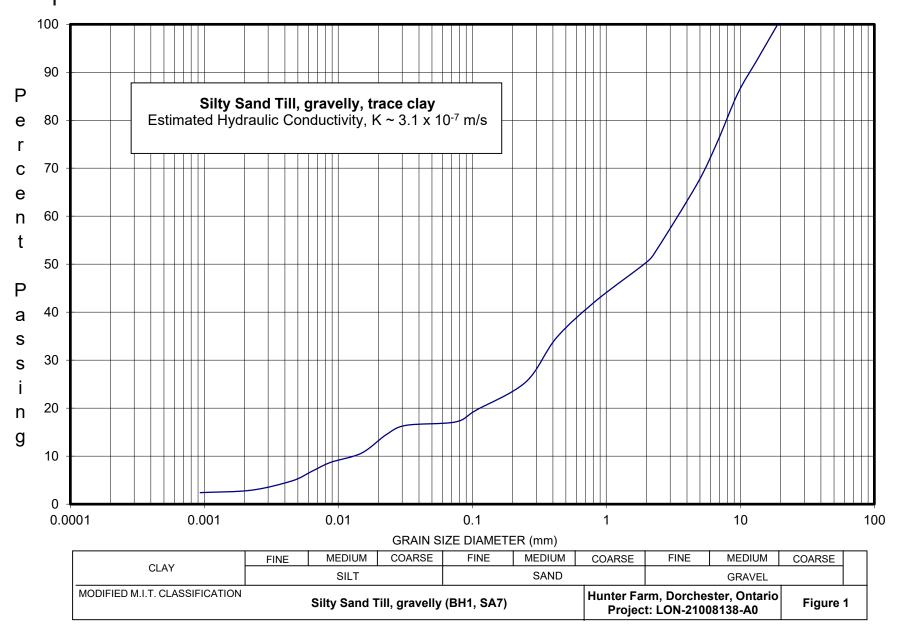
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| | - | Hunter Farm | | | | | | | PR | ROJECT NO. <u>LON-21008138-A0</u> | |
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| CL | IENT _ | uburn Developments Inc. | | | | | | | | ATUM <u>Geodetic</u> | |
| LO | CATION | Marion Street, Dorchester, ON | | DAT | ES: | Exca | vation | Augus | t 4, 202 | 21 Water Level | |
| | Ę | | s | | | SA | MPLES | 1 | В | SHEAR STRENGTH | |
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| Ĥ | Ö | DESCRIPTION | A | | T Y P E | NUMBER | RECOVERY | (blows) | K | Atterberg Limits and Moisture | |
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| (m) | (m) 267.3 | | T | | | | (mm) or (%) | (%) | Ϋ́ (kN/m3) | ● SPT N Value × Dynamic Cone 10 20 30 40 | |
| -0- | | TOPSOIL - 200 mm | 7/ 1/N . · 7/ | | T | | (%) | | (KIWIIIO) | | |
| - | 267.1 | SILTY SAND , brown, trace gravel, trace clay, | 1/. \\ /. | 1 | | | | | | <u> </u> | |
| - | | loose to compact, moist to very moist | | 1 | | | | | | | |
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| -4 | 263.3 | End of toot nit at 4.0 m has | <u>lii.</u> E | | | | _ | | | | |
| _ | | End of test pit at 4.0 m bgs. | | | | | | | | | |
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| 5 | | | 1 | | | SAI | <u> </u> MPLF I | EGEND | | <u> </u> | |
| NO | TES | | | | | | AS Aug | ger Samp | | SS Split Spoon ST Shelby Tube VN Vane Sample | |
| ľm | nust be re | erpretation requires assistance by EXP before use by ad in conjunction with EXP Report LON-21008138- <i>A</i> | t pit lo | g _{OTI} | HER TE | Core (eg. STS | uw, ING | t, etc.) | | | |
| 2) T | est pit is b | ased on observations of the excavator resistance. an and dry upon completion of excavation. below ground surface. | | | | G Specific Gravity C Consolidation H Hydrometer CD Consolidated Drained Triaxial | | | | | |
| 4) b | gs denote | n and dry upon completion of excavation. s below ground surface. evations surveyed using a SOKKIA GCX2 Receiver. | | | | S | Sieve Ar | nalysis | Cl | U Consolidated Undrained Triaxial | |
| | COUCIIC EI | ovacións surveyed using a SOMMA GOAZ NECEIVEL. | | | | ΡĖ | | rmeability | y UC | U Unconsolidated Undrained Triaxial C Unconfined Compression | |
| | | | | | | | | meability | DS | S Direct Shear | |
| | | | | | | | TER LE Appare | | ▼ Me | easured Ā Artesian (see Notes) | |

Appendix E – Grain Size Analyses

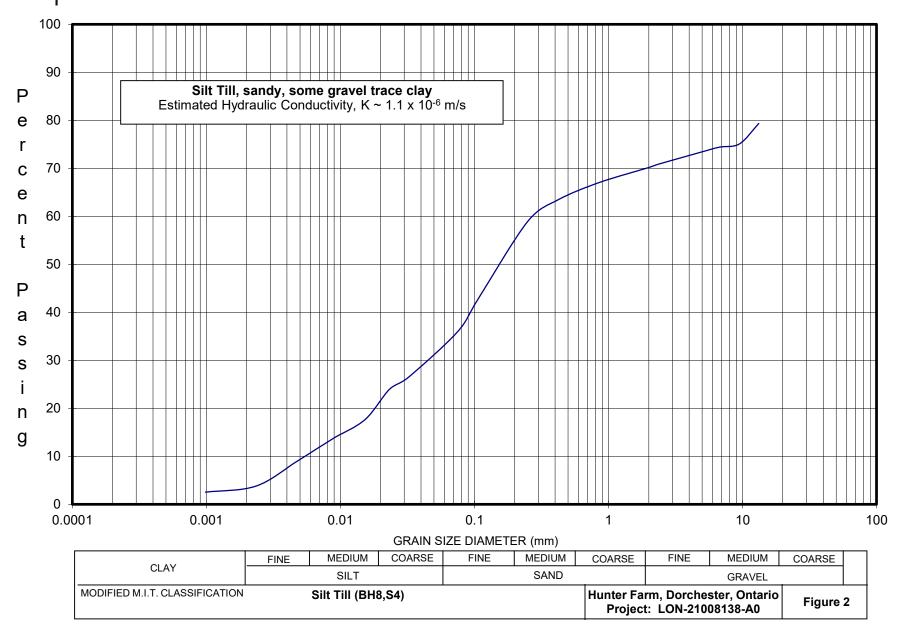
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MECHANICAL GRAIN SIZE ANALYSIS



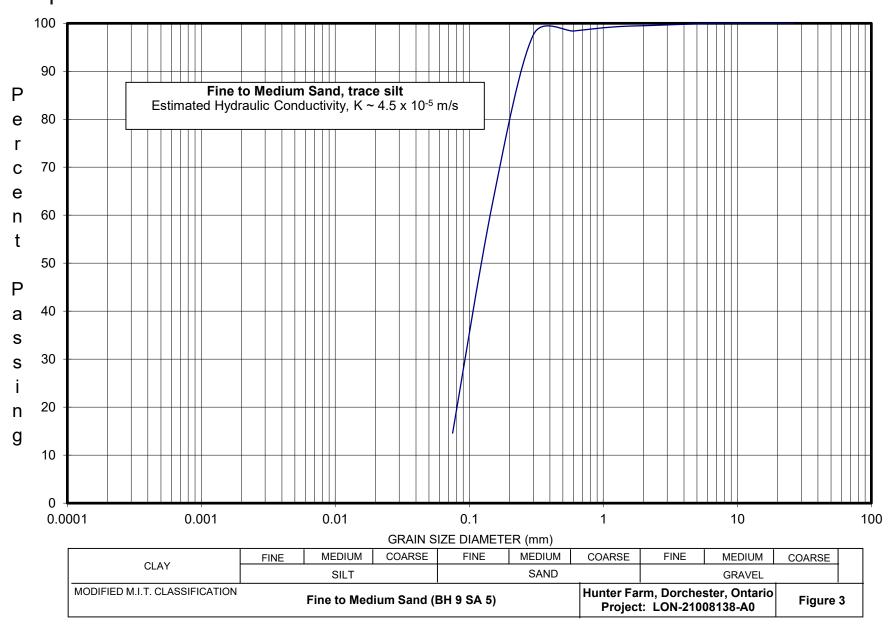
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MECHANICAL GRAIN SIZE ANALYSIS



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MECHANICAL GRAIN SIZE ANALYSIS



Appendix F – MECP Water Well Record Summary

Sunday, September 5, 2021

8:20:55 PM

| TOWNSHIP CON LOT | UTM | DATE CNTR | CASING DIA | WATER | PUMP TEST | WELL USE | SCREEN | WELL | FORMATION |
|-------------------------------------|------------------------|--------------|------------|---------|--------------|----------|---------|----------------------------------|---|
| NORTH DORCHESTER TOW | 17 495037 4759176 W | 2013/03 6809 | 0.75 | | | МО | 0097 10 | 7219087 (Z164808) A135911 | BRWN SAND GRVL 0022 GREY CLAY TILL 0082 GREY SAND GRVL 0102 |
| NORTH DORCHESTER TOW | 17 493597 4759957 W | 2008/12 7238 | | | | | | 7117778 (Z90466) A069682 A | |
| NORTH DORCHESTER TOW | 17 493620 4760020 W | 6607 | 2.00 | 0020 | | MN | 0015 13 | 7115588 (Z86898) A069682 | BRWN SAND SLTY 0003 BRWN SILT SNDY 0010 GREY SILT 0021 GREY SILT 0028 |
| NORTH DORCHESTER TOW | 17 495178 4759247 W | 2005/10 7190 | 0.79 | | | | 0010 10 | 4116326 (Z25566) A029302 | BRWN SAND 0020 |
| NORTH DORCHESTER TOW 04 008 | 17 493699 4759607 W | 2008/06 6607 | 0.75 | UK 0003 | | МО | | 7116490 (M01798) A067294 | BRWN SILT LOAM 0004 BRWN SILT SAND 0005 BRWN SAND SILT GRVL 0007 GREY SILT SAND GRVL 0007 |
| NORTH DORCHESTER TOW TR N 03 007 | 17 493514 4760058 W | 1965/09 3009 | 6 6 | FR 0088 | 22/27/10/4:0 | DO | | 4102868 () | CLAY STNS 0056 BRWN LMSN 0060 FSND 0079 BRWN LMSN 0089 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493534 4760013 W | 1962/03 3117 | 6 | FR 0058 | 12/30/8/2:30 | DO | | 4102871 () | LOAM MSND 0008 HPAN STNS 0058 GRVL 0060 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493534 4760013 W | 1969/08 3009 | 5 5 | FR 0082 | 23/30/12/5:0 | DO | | 4104788 () | BRWN CLAY 0016 GREY CLAY MSND STNS 0045 GRVL 0046 GREY CLAY MSND 0079 GREY LMSN 0082 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493534 4760123 W | 1977/05 5466 | 5 | FR 0082 | 28/28/4/48:0 | DO | | 4108014 () | RED CLAY SNDY PCKD 0012 BRWN SAND GRVL CLAY 0020 GREY GRVL CLAY BLDR 0040 GREY GRVL SAND CLAY 0070 GREY GRVL SAND PORS 0082 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493534 4760143 W | 1977/04 5466 | 5 | FR 0085 | 30/37/4/48:0 | DO | | 4108013 () | RED CLAY SNDY PCKD 0015 BRWN SAND LOOS 0020 GREY GRVL CLAY SAND 0085 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493744 4760038 W | 1988/03 3009 | 5 | FR 0073 | 28/41/6/1:45 | DO | | 4111206 (23005) | BLCK LOAM 0001 BRWN SAND CLAY 0009 GREY CLAY SAND 0014 GREY CLAY SAND STNS 0070 GREY FGVL SAND SILT 0072 GREY CSND 0073 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493484 4760183 W | 1970/08 2607 | 36 | FR 0008 | 8///: | DO | | 4105190 () | BRWN MSND 0008 GRVL BLDR 0009 BLUE CLAY BLDR 0020 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493514 4760028 W | 1954/08 1708 | 4 | FR 0029 | 29/32/5/5:0 | DO | | 4103066 () | MSND GRVL 0010 HPAN BLDR 0068 GRVL 0069 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493554 4760183 W | 1963/06 3009 | 4 4 | FR 0103 | 50/55/10/3:0 | DO | | 4102872 () | LOAM MSND 0020 GRVL 0022 CLAY 0041 GRVL 0046 CLAY 0076 MSND 0081 GREY LMSN 0083 FSND 0088 CLAY MSND 0102 GREY LMSN 0104 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493774 4760103 W | 1961/01 1708 | 5 5 | FR 0062 | 35/44/5/8:0 | ST DO | | 4102870 () | LOAM 0004 BRWN CLAY 0030 CLAY GRVL 0050 CLAY MSND 0062 GRVL 0064 |

| TOWNSHIP CON LOT | UTM | DATE CNTR | CASING DIA | WATER | PUMP TEST | WELL USE | SCREEN | WELL | FORMATION |
|-------------------------------------|------------------------|--------------|------------|---------|---------------|----------|--------|---------------------------------|--|
| NORTH DORCHESTER TOW TR N 03 008 | 17 493534 4760053 W | 1972/06 3009 | 5 | FR 0084 | 26/33/10/2:0 | DO | | 4105974 () | CLAY SAND 0008 BRWN CLAY 0022 GREY SAND CLAY 0031 GREY CLAY SAND 0045 GREY SAND CLAY 0083 GREY SAND 0084 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493602 4760482 W | 2018/09 5466 | 6.25 | FR 0038 | 20//20/1: | DO | | 7328053 (Z282227) A255658 | BRWN SAND 0001 BRWN SAND GRVL 0014 GREY SAND GRVL 0028 GREY GRVL SAND CLAY 0030 GREY CLAY GRVL SAND 0038 |
| NORTH DORCHESTER TOW TR N 03 008 | 17 493559 4760223 W | 1988/03 5466 | 5 | SU 0102 | 48/76/6/24:0 | DO | | 4111398 (14340) | BRWN SAND PCKD 0017 GREY SAND CLAY 0023 GREY GRVL CLAY 0030 GREY BLDR HARD 0032 GREY GRVL CLAY 0075 GREY GRVL SAND 0080 GREY GRVL SAND CLAY 0098 GREY GRVL SAND 0100 GREY LMSN HARD 0102 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494234 4760323 W | 1985/12 5466 | 6 6 | FR 0068 | 18/46/4/12:0 | DO | | 4110509 (NA) | BLCK LOAM PORS 0001 BRWN SAND STNS CLAY 0015 GREY CLAY STNS DNSE 0022 GREY CLAY GRVL 0038 GREY CLAY STNS DNSE 0052 GREY GRVL CLAY 0066 GREY LMSN HARD 0069 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494374 4760463 W | 1979/06 2607 | 36 | FR 0008 | 8/14/3/: | DO | | 4108834 () | SAND 0014 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494354 4760503 W | 1980/03 5466 | 5 | FR 0050 | 10/38/5/2:0 | DO | 0049 3 | 4109439 () | BRWN SAND PCKD 0007 BRWN GRVL CLAY 0015 BRWN CLAY SAND 0025 BRWN GRVL CLAY 0048 BRWN GRVL PORS 0052 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494314 4760363 W | 1980/03 5466 | 5 5 | FR 0077 | 12/34/5/16:0 | DO | | 4109440 () | BRWN SAND PCKD 0007 BRWN GRVL SAND 0018 BRWN CLAY SAND 0027 BRWN GRVL CLAY 0069 BRWN GRVL PORS 0075 BRWN LMSN HARD 0077 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494394 4760403 W | 1983/08 5466 | 5 5 | FR 0068 | 6/30/13/14:0 | DO | | 4110011 () | BRWN SAND PCKD 0010 BRWN SAND 0020 GREY CLAY DNSE 0025 GREY GRVL CLAY 0060 GREY GRVL PORS 0067 BRWN LMSN HARD 0068 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494064 4761023 W | 1955/07 2801 | 8 | | | | | 4103070 () | FSND 0013 MSND CLAY GRVL 0020 BLUE CLAY MSND GRVL 0045 BLUE CLAY 0064 BLUE CLAY FSND 0070 FSND GRVL 0077 MSND GRVL 0082 BLUE CLAY GRVL 0100 ROCK 0102 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494434 4760403 W | 1976/04 5466 | 5 5 | MN 0063 | -4/16/15/24:0 | DO | | 4107600 () | RED SAND LOOS 0006 BLUE CLAY DNSE 0020 GREY GRVL CLAY LYRD 0050 GREY GRVL PORS 0061 BRWN LMSN HARD PORS 0063 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494084 4760273 W | 1962/09 1708 | 5 5 | SU 0092 | 60/65/8/8:0 | ST DO | | 4102873 () | LOAM 0006 MSND 0022 GREY CLAY 0057 HPAN 0078 CLAY 0088 LMSN 0092 |
| NORTH DORCHESTER TOW TR N 03 009 | 17 494284 4760353 W | 1988/03 5466 | 5 5 | FR 0078 | 28/63/6/1:0 | DO | | 4111255 (03895) | BRWN SAND CLAY PCKD 0004 BRWN SAND PCKD 0020 GREY SAND CLAY PCKD 0035 GREY GRVL CLAY 0074 BRWN LMSN HARD 0078 |
| NORTH DORCHESTER TOW TR N 03 010 | 17 494214 4760363 W | 1983/04 5466 | 5 | FR 0075 | 15/46/5/4:0 | DO | | 4109922 () | BRWN SAND PCKD 0005 BRWN CLAY GRVL 0010 GREY CLAY SAND 0029 GREY GRVL CLAY 0071 BRWN LMSN HARD 0075 |
| NORTH DORCHESTER TOW TR N 03 010 | 17 495014 4760618 W | 1971/03 1708 | 4 | FR 0064 | 34/61/9/8:0 | DO | 0065 4 | 4105393 () | LOAM 0001 BRWN CLAY MSND 0021 BRWN CLAY MSND 0043 GREY FSND 0060 GREY MSND CLAY 0064 GREY FSND 0069 GREY CLAY GRVL 0070 |
| NORTH DORCHESTER TOW TR N 03 010 | 17 494614 4760663 W | 1976/06 5466 | 5 5 | MN 0076 | 7/38/10/16:0 | ST | | 4107654 () | RED SAND LOOS 0004 GREY GRVL PORS 0025 GREY CLAY DNSE 0030 GREY GRVL CLAY LYRD 0065 GREY GRVL PORS 0073 BRWN LMSN HARD PORS 0076 |

| TOWNSHIP CON LOT | UTM | DATE CNTR | CASING DIA | WATER | PUMP TEST | WELL USE | SCREEN | WELL | FORMATION | |
|-------------------------------------|------------------------|--------------|------------|---------|---------------|----------|---------|---------------------------------|---|--|
| NORTH DORCHESTER TOW TR N 03 011 | 17 495154 4760703 W | 1967/08 3009 | 5 5 | FR 0135 | 40/132/6/6:0 | DO | | 4102876 () | CLAY MSND 0020 FSND 0062 CLAY MSND 0092 FSND 0107 LMSN 0110 MSND GRVL 0132 GREY LMSN 0135 | |
| NORTH DORCHESTER TOW TR N 03 011 | 17 495360 4760757 W | 2019/07 7090 | 6 6 | UT 0071 | 39/41/10/2: | DO | 0058 12 | 7338997 (Z299311) A258362 | BRWN CLAY SNDY 0013 BRWN FSND LOOS 0071 GREY CLAY SOFT 0075 | |
| NORTH DORCHESTER TOW TR N 03 011 | 17 495219 4760709 W | 2015/06 7090 | 6 6 | UT 0061 | 30/33/10/1:30 | DO | 0048 12 | 7254857 (Z201669) A170120 | BRWN CLAY STNS 0014 BRWN SAND 0060 GREY HPAN 0065 | |
| NORTH DORCHESTER TOW TR N 03 011 | 17 495283 4760742 W | 2018/07 7090 | 6 6 | UT 0042 | 35/40/10/1:30 | DO | 0052 12 | 7314845 (Z288559) A249256 | BLCK LOAM LOAM 0002 BRWN CLAY STNS SAND 0016 BRWN SAND FSND 0042 GREY SAND MSND 0064 GREY CLAY SOFT 0069 | |
| NORTH DORCHESTER TOW TR N 03 011 | 17 495134 4760743 W | 1967/02 1708 | 5 5 | FR 0064 | 33/62/7/8:0 | ST DO | 0060 3 | 4102875 () | BRWN CLAY 0008 BRWN CLAY MSND 0028 BRWN FSND 0064 BRWN CSND 0067 GREY CLAY 0068 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493974 4759213 W | 1962/08 2801 | 5 | | | | | 4102900 () | CLAY MSND 0003 MSND GRVL BLDR 0008 CLAY BLDR 0026 MSND GRVL 0028 WHIT CLAY BLDR 0031 ROCK 0036 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 494074 4759283 W | 1962/08 2801 | 5 | | | | | 4102898 () | FILL CLAY 0006 MSND GRVL 0011 CLAY BLDR 0026 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493514 4759961 W | 1961/05 3410 | 5 5 | FR 0082 | 17/24/6/3:0 | DO | | 4102896 () | LOAM 0002 YLLW MSND 0005 BLUE CLAY 0020 HPAN 0079 GREY LMSN 0084 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493639 4760008 W | 1962/01 1708 | 5 5 | FR 0071 | 28/33/8/8:0 | DO | | 4102897 () | BRWN CLAY 0015 BLUE CLAY 0017 CLAY GRVL 0069 GRVL SHLE 0071 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493674 4759963 W | 1975/05 1708 | 5 | FR 0066 | 24/42/13/8:0 | DO | | 4107535 () | LOAM 0001 BRWN CLAY STNS 0016 GREY CLAY GRVL 0042 GREY GRVL CMTD 0059 GREY CLAY SAND GRVL 0066 LMSN GRVL 0067 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493504 4759953 W | 1969/04 2607 | 36 | FR 0010 | 10/21/1/1:0 | DO | | 4104657 () | BRWN CLAY MSND 0008 BLUE CLAY MSND 0022 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493514 4759943 W | 1969/08 2607 | 36 | FR 0023 | 23/39/0/1:0 | DO | | 4104792 () | BRWN CLAY MSND 0012 BLUE CLAY BLDR 0040 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493750 4759660 W | 2003/11 6032 | 1.97 | | | NU | 0007 3 | 4115472 (Z05561) A005180 | BRWN SILT 0012 GREY GRVL TILL SILT 0015 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493803 4759643 L | 1997/09 3563 | 5 5 5 | FR 0123 | 32/90/12/2:0 | DO | | 4113726 (177836) | BRWN CLAY STNS 0018 BLUE CLAY 0053 SAND GRVL DRY 0061 GREY HPAN STNS 0098 GREY LMSN 0123 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493774 4760053 W | 1987/06 5466 | 5 4 | FR 0073 | 20/37/13/18:0 | DO | 0070 3 | 4110951 (03819) | BRWN CLAY STNS DNSE 0005 BRWN GRVL CLAY PCKD 0012 GREY CLAY GRVL PCKD 0020 GREY GRVL SAND CLAY 0060 GREY GRVL SAND 0070 GREY CSND LOOS 0073 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493534 4759963 W | 1985/12 5466 | 5 | FR 0061 | 15/31/12/2:0 | DO | 0058 3 | 4110402 () | BRWN CLAY STNS 0010 BRWN GRVL CLAY 0016 GREY GRVL CLAY 0054 GREY GRVL SAND CLAY 0058 GREY SAND GRVL LOOS 0061 | |
| NORTH DORCHESTER TOW TR N 04 008 | 17 493684 4759633 W | 1968/07 2607 | 36 | FR 0006 | 6/14/0/1:0 | PS | | 4104491 () | CLAY 0015 | |

| TOWNSHIP CON LOT | UTM | DATE CNTR | CASING DIA | WATER | PUMP TEST | WELL USE | SCREEN | WELL | FORMATION |
|-------------------------------------|------------------------|--------------|------------|---------|--------------|----------|--------|---------------------|---|
| NORTH DORCHESTER TOW TR N 04 009 | 17 494378 4759884 L | 2000/03 6824 | 5 | FR 0030 | 30/34/5/2:0 | DO | 0032 3 | 4114469 (212155) | BRWN FSND 0028 BLCK FSND 0040 GREY GRVL TILL 0055 |
| NORTH DORCHESTER TOW TR N 04 009 | 17 494484 4759603 W | 1952/07 3410 | 6 | SU 0063 | 12/40/15/: | DO | | 4102899 () | GRVL 0010 CLAY 0020 MSND 0027 HPAN 0062 GRVL 0063 |
| NORTH DORCHESTER TOW TR N 04 010 | 17 494914 4759783 W | 1953/09 4711 | 4 4 | FR 0059 | 15/20/4/5:0 | DO | | 4102902 () | LOAM 0003 YLLW CLAY 0006 GRVL HPAN 0020 STNS HPAN 0045 SHLE 0059 |
| NORTH DORCHESTER TOW TR N 04 010 | 17 494687 4760428 W | 1974/03 2801 | | | | MN | | 4106734 () | LOAM 0001 BRWN CLAY GRVL 0006 GREY CLAY 0019 GREY CLAY SILT 0030 GREY CLAY SAND SILT 0064 GREY LMSN 0065 GREY LMSN 0067 |
| NORTH DORCHESTER TOW TR N 04 010 | 17 495094 4760403 W | 1984/10 2552 | 36 | FR 0025 | 25/47/5/2:0 | DO | | 4110200 () | BRWN CLAY 0020 BRWN SAND 0048 |
| NORTH DORCHESTER TOW TR N 04 010 | 17 494954 4759743 W | 1947/06 3558 | 4 4 | SU | 16/19/6/4:0 | DO | | 4102901 () | BRWN CLAY STNS 0020 HPAN BLDR 0052 GREY ROCK 0057 |
| NORTH DORCHESTER TOW TR N 04 011 | 17 495234 4760343 W | 1966/11 2519 | 30 | FR 0012 | 12/20/3/1:0 | DO | | 4102903 () | LOAM 0001 BRWN CLAY 0011 BRWN MSND 0020 |
| NORTH DORCHESTER TOW TR S A 017 | 17 495394 4759563 W | 1948/10 3505 | 4 | SU 0088 | 30/35/6/7:0 | DO | | 4102944 () | LOAM 0004 BLDR CLAY 0020 GRVL STNS 0050 BLDR CLAY ROCK 0088 |
| NORTH DORCHESTER TOW TR S A 017 | 17 495354 4759283 W | 1953/03 2801 | 6 | | | | | 4102945 () | LOAM 0001 MSND GRVL 0015 BLDR MSND GRVL 0022 BLUE CLAY MSND GRVL 0027 GRVL MSND 0028 BLUE CLAY MSND GRVL 0039 GRVL MSND CLAY 0046 BLUE CLAY MSND GRVL 0065 BLUE CLAY GRVL MSND 0069 GRVL ROCK 0077 CLAY 0079 |
| NORTH DORCHESTER TOW TR S A 018 | 17 494744 4759328 W | 1949/08 3511 | 4 4 | | 60/70/5/12:0 | DO | | 4102949 () | BRWN CLAY 0020 HPAN STNS 0070 MSND 0080 LMSN 0084 |
| NORTH DORCHESTER TOW TR S A 018 | 17 494159 4759188 W | 1953/03 2801 | 4 4 4 | FR | 39/40/19/7:0 | NU | 0055 7 | 4102950 () | LOAM 0001 MSND GRVL CLAY 0045 MSND GRVL 0057 BLDR MSND GRVL 0062 MSND GRVL BLDR 0072 ROCK 0074 |
| NORTH DORCHESTER TOW TR S A 018 | 17 494744 4759333 W | 1955/11 4711 | 6 | FR 0079 | 30/60/2/5:0 | ST DO | | 4102951 () | LOAM 0001 MSND GRVL 0035 CLAY GRVL 0079 GRVL 0080 |
| NORTH DORCHESTER TOW TR S A 019 | 17 494374 4759343 W | 1985/10 4741 | 10 | SU 0064 | ///24:0 | | | 4110332 () | GRVL 0003 BRWN CLAY 0017 BLUE CLAY STNS 0045 GREY LMSN 0078 |
| NORTH DORCHESTER TOW TR S A 019 | 17 494454 4759263 W | 1985/05 4741 | 7 | | | | | 4110336 () | GRVL 0012 BRWN CLAY 0017 BLUE CLAY STNS 0040 |
| NORTH DORCHESTER TOW TR S A 019 | 17 494074 4759143 W | 1985/10 4741 | 5 | FR 0010 | 2/10/10/1:0 | | 0006 4 | 4110339 () A | BRWN CLAY SLTY 0006 BRWN GRVL 0010 |

TOWNSHIP CON LOT UTM DATE CNTR CASING DIA WATER PUMP TEST WELL USE SCREEN WELL FORMATION

SNDS SANDSTONE

SNDY SANDYOAPSTONE

Notes:

DRTY DIRTY

DRY DRY

UTM: DTM in Zone, Easting, Northing and Datum is NAD83; L: UTM estimated from Centroid of Lot; W: UTM not from Lot Centroid DATE CNTR: Date Work Completedand Well Contractor Licence Number

PEAT PEAT

PGVL PEA GRAVEL

CASING DIA: . @asing diameter in inches

WATER: Onit of Depth in Fee. See Table 4 for Meaning of Code

HARD HARD

HPAN HARDPAN

PUMP TEST: Static Water Level in Feet / Water Level After Pumping in Feet / Pump Test Rate in GPM / Pump Test Duration in Hour : Minutes

WELL USE: See Table 3 for Meaning of Code SCREEN: Screen Depth and Length in feet

WELL: WEL (AUDIT #) Well Tag . A: Abandonment; P: Partial Data Entry Only

FORMATION: See Table 1 and 2 for Meaning of Code

1. Core Material and Descriptive terms

| Code | Description | Code | Description | Code | Description | Code | Description | Code | Description |
|-------|----------------|--------------|--------------|------|----------------|------|----------------|--------------|----------------|
| BLDR | BOULDERS | FCRD | FRACTURED | IRFM | IRON FORMATION | PORS | POROUS | SOFT | SOFT |
| BSLT | BASALT | FGRD | FINE-GRAINED | LIMY | LIMY | PRDG | PREVIOUSLY DUG | SPST | SOAPSTONE |
| CGRD | COARSE-GRAINED | ${\tt FGVL}$ | FINE GRAVEL | LMSN | LIMESTONE | PRDR | PREV. DRILLED | STKY | STICKY |
| CGVL | COARSE GRAVEL | ${\tt FILL}$ | FILL | LOAM | TOPSOIL | QRTZ | QUARTZITE | STNS | STONES |
| CHRT | CHERT | FLDS | FELDSPAR | LOOS | LOOSE | QSND | QUICKSAND | STNY | STONEY |
| CLAY | CLAY | FLNT | FLINT | LTCL | LIGHT-COLOURED | QTZ | QUARTZ | THIK | THICK |
| CLN (| CLEAN | FOSS | FOSILIFEROUS | LYRD | LAYERED | ROCK | ROCK | THIN | THIN |
| CLYY | CLAYEY | FSND | FINE SAND | MARL | MARL | SAND | SAND | ${\tt TILL}$ | TILL |
| CMTD | CEMENTED | GNIS | GNEISS | MGRD | MEDIUM-GRAINED | SHLE | SHALE | UNKN | UNKNOWN TYPE |
| CONG | CONGLOMERATE | GRNT | GRANITE | MGVL | MEDIUM GRAVEL | SHLY | SHALY | VERY | VERY |
| CRYS | CRYSTALLINE | GRSN | GREENSTONE | MRBL | MARBLE | SHRP | SHARP | WBRG | WATER-BEARING |
| CSND | COARSE SAND | GRVL | GRAVEL | MSND | MEDIUM SAND | SHST | SCHIST | WDFR | WOOD FRAGMENTS |
| DKCL | DARK-COLOURED | GRWK | GREYWACKE | MUCK | MUCK | SILT | SILT | WTHD | WEATHERED |
| DLMT | DOLOMITE | GVLY | GRAVELLY | OBDN | OVERBURDEN | SLTE | SLATE | | |
| DNSE | DENSE | GYPS | GYPSUM | PCKD | PACKED | SLTY | SILTY | | |
| | | | | | | | | | |

2. Core Color

3. Well Use

| ded Demonstration ded Demonstration ded Demonstration | |
|---|-----|
| Code Description Code Description Code Description | |
| WHIT WHITE DO Domestic OT Other | |
| GREY GREY ST Livestock TH Test Hole | |
| BLUE BLUE IR Irrigation DE Dewatering | |
| GREN GREEN IN Industrial MO Monitoring | |
| YLLW YELLOW CO Commercial MT Monitoring TestH | ole |
| BRWN BROWN MN Municipal | |
| RED RED PS Public | |
| BLCK BLACK AC Cooling And A/C | |
| BLGY BLUE-GREY NU Not Used | |

4. Water Detail

| Code | Description | Code | Description |
|----------|--------------------|------|-------------|
| FR | Fresh | GS | Gas |
| SA | Salty | IR | Iron |
| SU | Sulphur | | |
| MN | Mineral | | |
| UK | Unknown | | |
| SU MN | Sulphur Mineral | TK | 11011 |

Appendix G – Water Levels and Hydrographs



LON-21008138-A0

Hunter Farm - Marion St, Dorchester

Groundwater Elevation Monitoring

| Well ID | BH1/MW | BH2/MW | BH3/MW | BH4/MW | BH5/MW | BH6/MW | BH7/MW-A | BH7/MW-B | BH8/MW | BH9/MW |
|-----------------------------------|--------|--------|--------|--------|--------|--------|----------|----------|--------|--------|
| Ground Surface Elevation (m amsl) | 260.80 | 256.00 | 256.04 | 256.03 | 257.64 | 268.06 | 264.30 | 264.28 | 257.53 | 266.14 |
| Top of Pipe Elevation (m amsl) | 261.60 | 256.90 | 256.89 | 256.85 | 258.57 | 268.90 | 265.08 | 265.11 | 258.43 | 266.96 |
| Groundwater Elevation (m amsl) | | | | | | | | | | |
| 17-May-21 | 256.18 | 255.01 | 254.79 | 254.59 | 256.87 | 258.87 | 263.69 | 263.75 | 257.03 | 264.84 |
| 30-Jul-21 | 256.03 | 255.14 | 254.49 | 254.73 | 256.96 | 258.61 | 263.26 | 263.22 | 257.09 | 264.81 |
| 17-Aug-21 | 255.97 | 254.99 | 254.37 | 254.60 | 256.82 | 258.59 | 262.98 | 262.93 | 256.95 | 264.60 |
| 28-Sep-21 | 256.30 | 255.26 | 255.03 | 254.85 | 257.01 | 258.38 | 263.65 | 263.57 | 257.12 | 264.92 |
| 13-Oct-21 | 256.41 | 255.35 | 254.99 | 254.77 | 257.27 | 258.53 | 263.90 | 263.86 | 257.19 | 264.97 |
| 10-Nov-21 | 256.43 | 255.23 | 254.61 | 254.75 | 257.03 | 258.90 | 263.85 | 263.90 | 257.19 | 264.99 |
| 20-Dec-21 | 256.46 | 255.24 | 254.02 | 254.78 | 257.07 | 259.37 | 264.08 | 264.20 | 257.19 | 264.40 |
| 18-Jan-22 | 256.45 | 255.20 | 253.97 | 254.80 | 257.13 | 259.33 | 264.10 | 264.06 | 257.20 | 264.45 |
| 24-Feb-22 | 256.59 | 255.46 | 255.27 | 255.09 | 257.23 | 259.24 | 264.15 | 264.32 | 257.25 | 265.30 |
| 17-Mar-22 | 256.47 | 255.26 | 255.10 | 254.82 | 257.19 | 259.22 | 264.20 | 264.20 | 257.15 | 265.14 |
| 26-Apr-22 | 256.46 | 255.24 | 254.04 | 254.78 | 257.07 | 259.18 | 264.06 | 264.21 | 257.13 | 265.13 |

Groundwater Level Monitoring

| Well ID | BH1/MW | BH2/MW | BH3/MW | BH4/MW | BH5/MW | BH6/MW | BH7/MW-A | BH7/MW-B | BH8/MW | BH9/MW |
|---------------------------|--------|--------|--------|--------|--------|--------|----------|----------|--------|--------|
| Groundwater Level (m bgs) | | | | | | | | | | |
| 17-May-21 | 4.62 | 1.00 | 1.25 | 1.44 | 0.77 | 9.18 | 0.61 | 0.53 | 0.50 | 1.30 |
| 30-Jul-21 | 4.77 | 0.87 | 1.55 | 1.30 | 0.68 | 9.44 | 1.04 | 1.06 | 0.44 | 1.33 |
| 17-Aug-21 | 4.83 | 1.02 | 1.67 | 1.43 | 0.82 | 9.46 | 1.32 | 1.35 | 0.58 | 1.54 |
| 28-Sep-21 | 4.50 | 0.75 | 1.01 | 1.18 | 0.63 | 9.67 | 0.65 | 0.71 | 0.41 | 1.22 |
| 13-Oct-21 | 4.39 | 0.66 | 1.05 | 1.26 | 0.37 | 9.53 | 0.40 | 0.42 | 0.34 | 1.17 |
| 10-Nov-21 | 4.37 | 0.78 | 1.43 | 1.28 | 0.61 | 9.15 | 0.45 | 0.38 | 0.34 | 1.15 |
| 20-Dec-21 | 4.34 | 0.77 | 2.02 | 1.25 | 0.57 | 8.68 | 0.22 | 0.08 | 0.34 | 1.74 |
| 18-Jan-22 | 4.35 | 0.81 | 2.07 | 1.23 | 0.51 | 8.72 | 0.20 | 0.22 | 0.33 | 1.69 |
| 24-Feb-22 | 4.21 | 0.55 | 0.77 | 0.94 | 0.41 | 8.81 | 0.15 | -0.04 | 0.28 | 0.84 |
| 17-Mar-22 | 4.33 | 0.75 | 0.94 | 1.21 | 0.45 | 8.83 | 0.10 | 0.08 | 0.38 | 1.00 |
| 26-Apr-22 | 4.34 | 0.77 | 2.00 | 1.25 | 0.57 | 8.87 | 0.24 | 0.07 | 0.40 | 1.01 |

Notes

- indicates not measured



LON-21008138-A0 Hunter Farm - Marion St, Dorchester

Water Elevation Monitoring

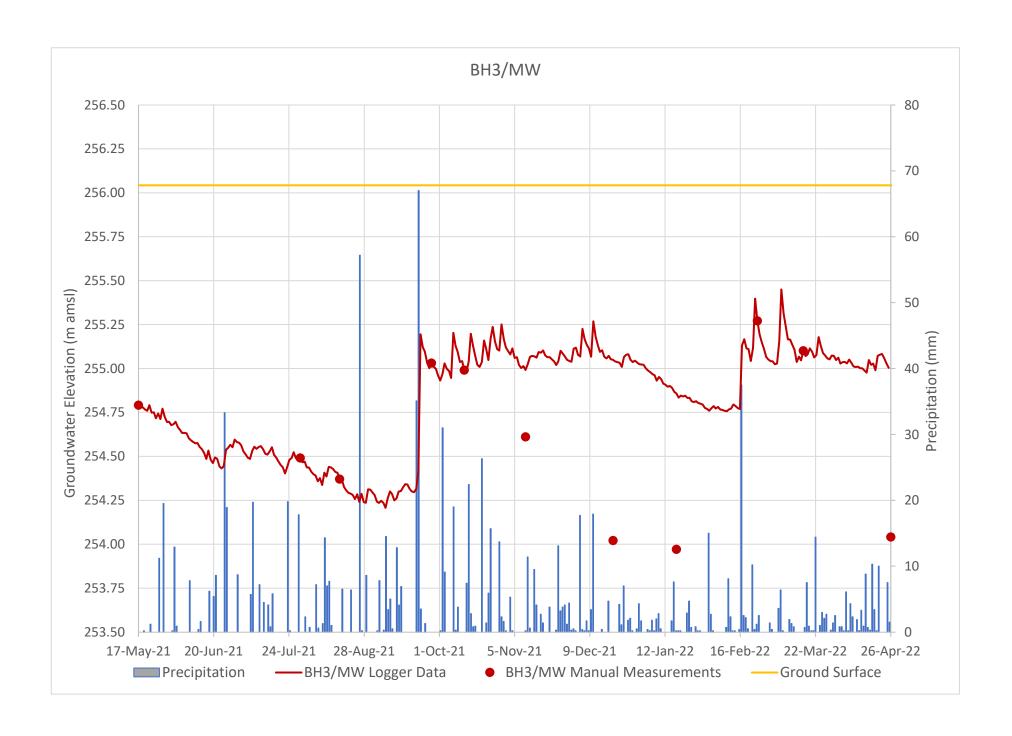
| Well ID | P1 Inside | P1 Outside | SG1 | P2 Inside | P2 Outside | SG2 | P3 Inside | P3 Outside | SG3 | P4 Inside | P4 Outside | SG4 | P5 Inside | P5 Outside | SG5 |
|---------------------------------|-----------|------------|--------|-----------|------------|--------|-----------|------------|--------|-----------|---------------|--------|-----------|---------------|--------|
| Ground Surface Elevation (masl) | 255.52 | 255.52 | 255.49 | 254.58 | 254.58 | 254.49 | 256.21 | 256.21 | 256.01 | 263.57 | 263.57 | 263.57 | 264.43 | 264.43 | 264.17 |
| Top of Pipe Elevation (masl) | 256.56 | 256.56 | - | 255.88 | 255.88 | - | 257.55 | 257.55 | - | 264.74 | 264.74 | - | 265.68 | 265.68 | - |
| Groundwater Elevation | | | | | | | | | | | | | | | |
| 30-Jul-21 | 255.16 | 255.63 | 255.60 | 254.65 | 254.67 | 254.72 | 256.27 | - | Dry | 262.96 | Dry | Dry | 264.56 | 264.68 | 264.56 |
| 17-Aug-21 | 255.22 | 255.66 | 255.60 | 254.68 | 254.70 | 254.71 | 256.25 | - | 256.27 | 262.78 | - | - | 264.54 | 264.65 | 264.56 |
| 28-Sep-21 | 255.46 | 255.58 | 255.59 | 254.89 | 254.75 | 254.79 | 256.52 | 256.25 | 256.35 | 262.76 | Dry | Dry | 264.69 | 264.66 | 264.57 |
| 13-Oct-21 | 255.66 | 255.46 | 255.63 | 254.89 | 254.75 | 254.85 | 256.51 | 256.36 | 256.41 | 263.29 | Dry | 263.71 | 264.70 | 264.69 | 264.63 |
| 10-Nov-21 | 255.44 | 255.64 | 255.63 | 254.71 | 254.69 | 254.78 | 256.63 | Dry | 256.40 | 263.68 | 263.75 | 264.10 | 264.62 | 264.69 | 264.62 |
| 20-Dec-21 | 255.56 | 255.65 | 255.64 | 254.77 | 254.66 | 254.77 | 256.54 | 256.31 | 256.38 | NM | NM | 264.27 | 264.71 | 264.54 | 264.64 |
| 18-Jan-22 | 255.54 | 255.61 | 255.62 | 254.75 | 254.64 | 254.78 | 256.50 | Dry | 256.37 | 263.70 | 263.75 | 263.95 | 264.69 | 264.70 | 264.61 |
| 24-Feb-22 | 255.60 | 255.81 | 255.75 | 255.28 | 254.83 | 254.94 | 256.60 | 256.38 | 256.48 | NM | 264.08 | 264.50 | 264.95 | 264.90 | 264.92 |
| 17-Mar-22 | 255.57 | 255.71 | 255.69 | 254.67 | 254.73 | 254.78 | 256.71 | 256.32 | 256.42 | 263.91 | 263.95 | 264.43 | 264.64 | 263.78 | 264.87 |
| 26-Apr-22 | 255.66 | 255.74 | 255.64 | 254.75 | 254.71 | 254.74 | 256.63 | 256.34 | 256.36 | NM | NM | 264.38 | 264.72 | 264.79 | 265.06 |

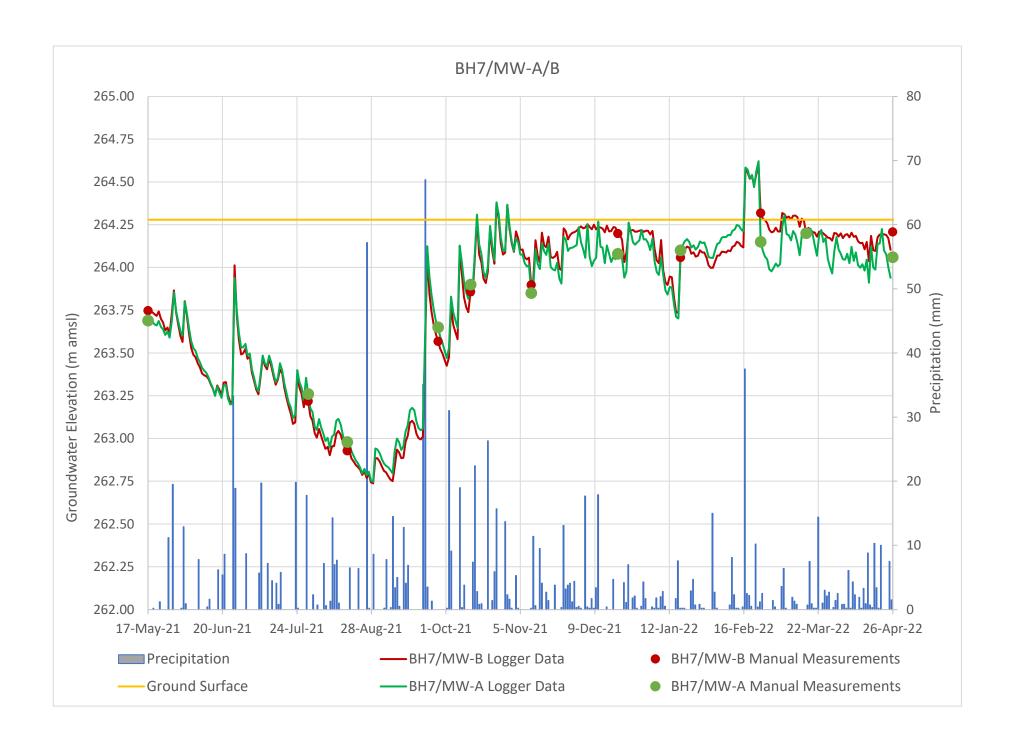
Water Level Monitoring

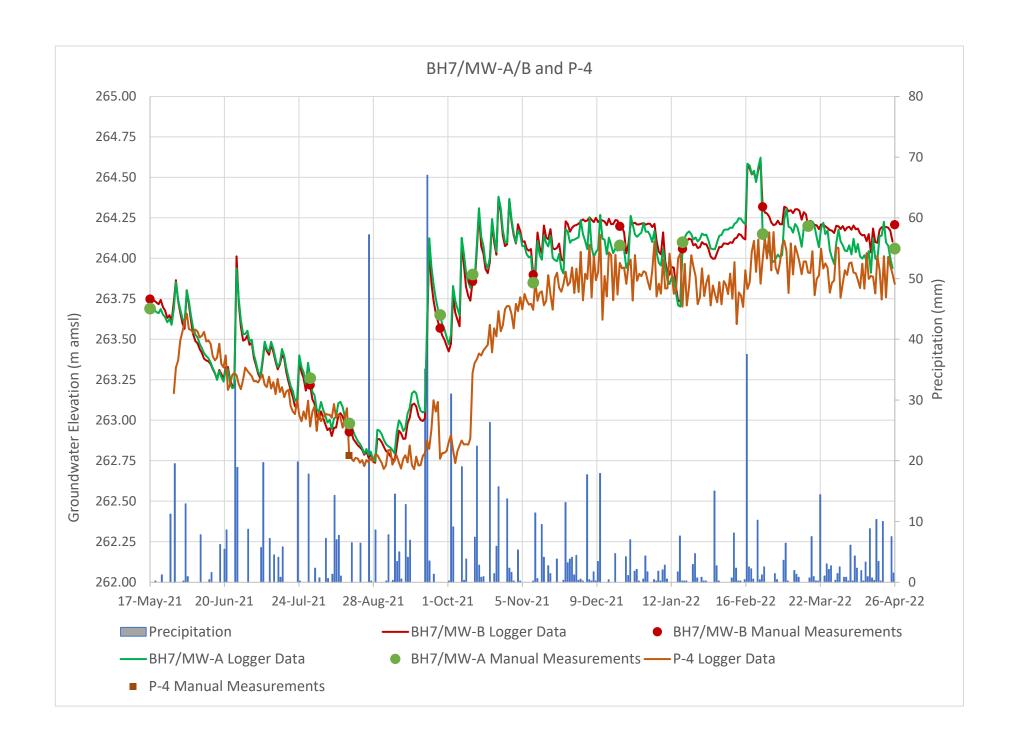
| Well ID | P1 Inside | P2 Inside | P3 Inside | P4 Inside | P5 Inside |
|---------------------------|-----------|-----------|-----------|-----------|-----------|
| Groundwater Level (m bgs) | | | | | |
| 30-Jul-21 | 0.36 | -0.07 | -0.06 | 0.60 | -0.13 |
| 17-Aug-21 | 0.30 | -0.10 | -0.04 | 0.78 | -0.11 |
| 28-Sep-21 | 0.06 | -0.31 | -0.31 | 0.80 | -0.26 |
| 13-Oct-21 | -0.14 | -0.31 | -0.30 | 0.27 | -0.27 |
| 10-Nov-21 | 0.08 | -0.13 | -0.42 | -0.12 | -0.19 |
| 20-Dec-21 | -0.04 | -0.19 | -0.33 | NM | -0.28 |
| 18-Jan-22 | -0.02 | -0.17 | -0.29 | -0.14 | -0.26 |
| 24-Feb-22 | -0.08 | -0.70 | -0.39 | NM | -0.52 |
| 17-Mar-22 | -0.05 | -0.09 | -0.50 | -0.35 | -0.21 |
| 26-Apr-22 | -0.14 | -0.17 | -0.42 | NM | -0.30 |

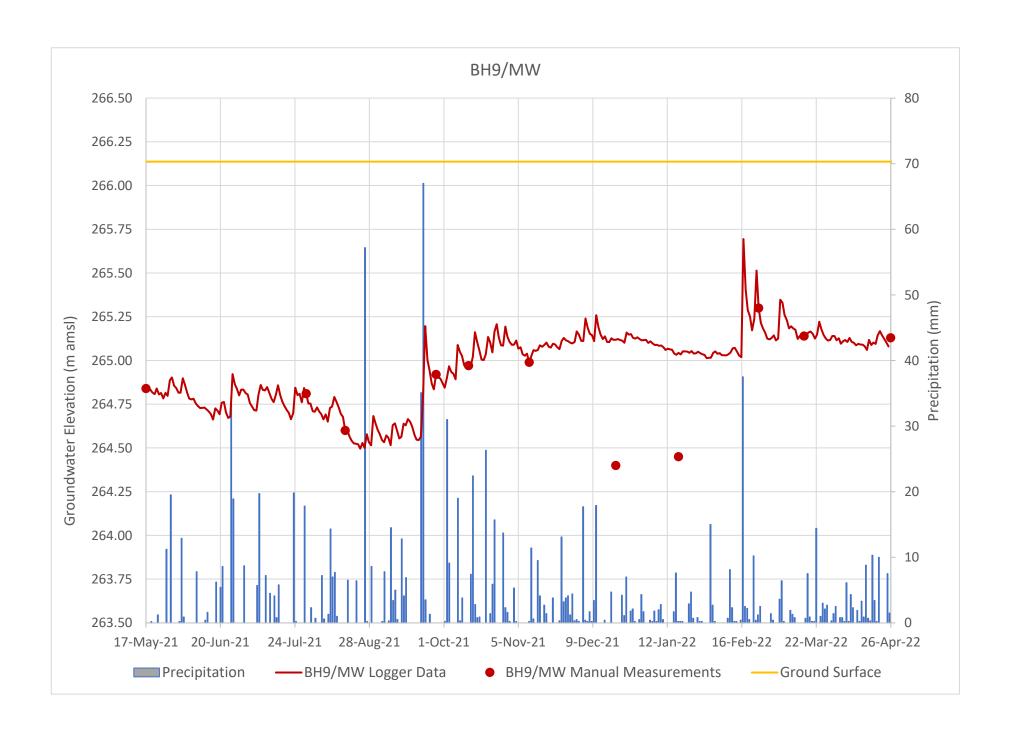
Notes:

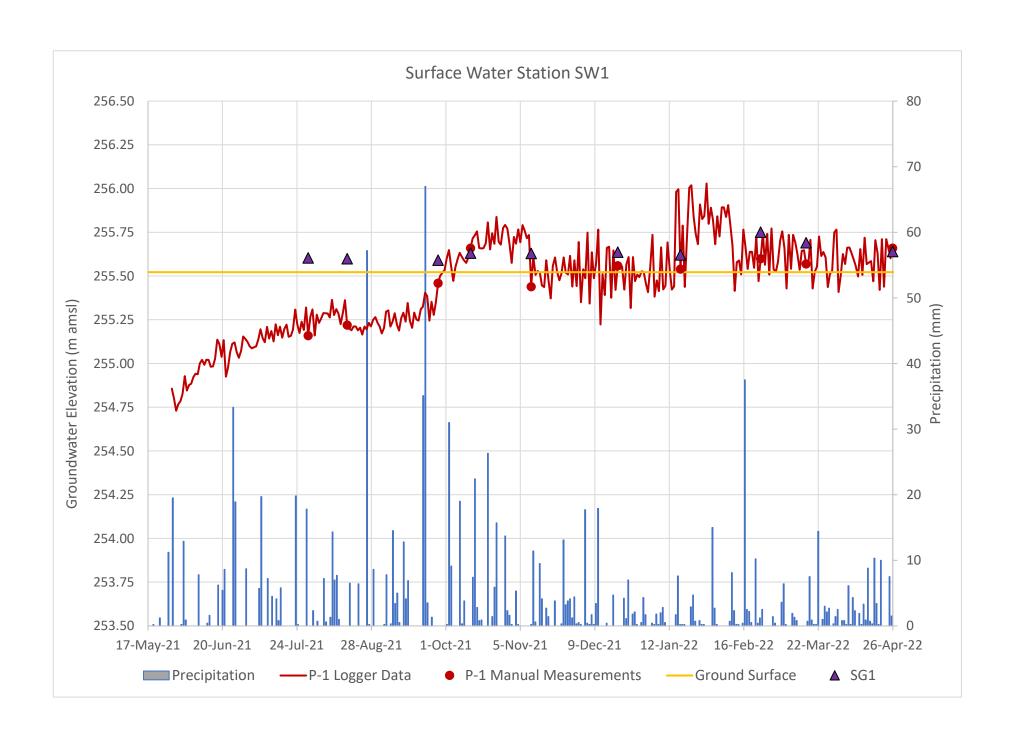
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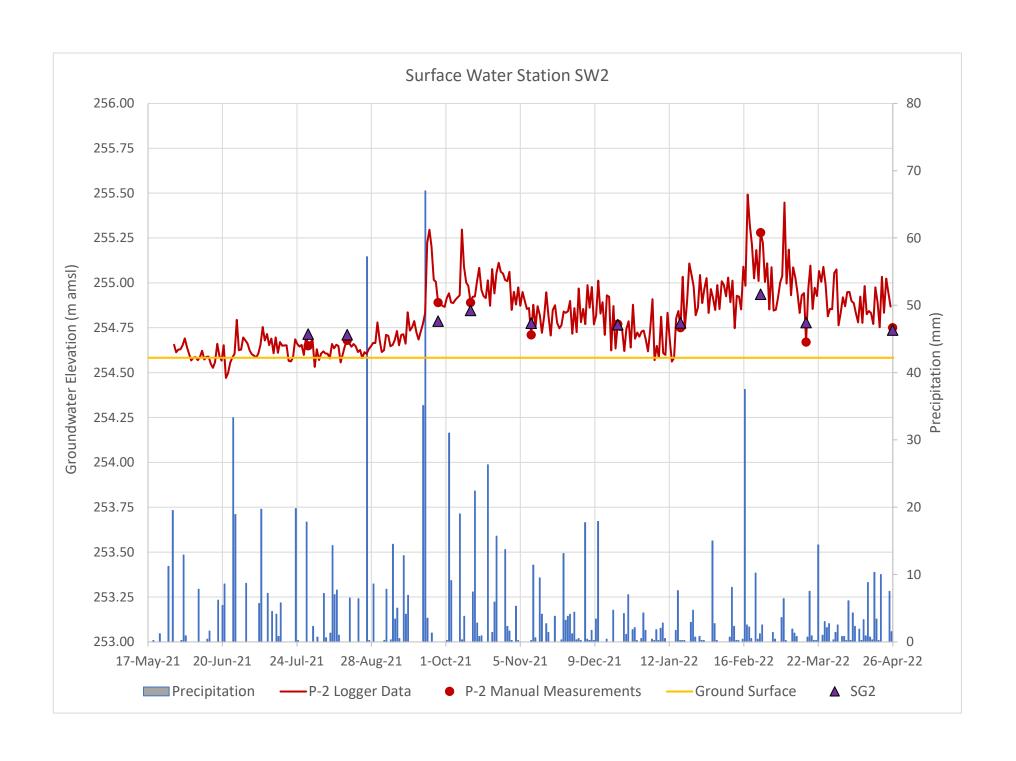


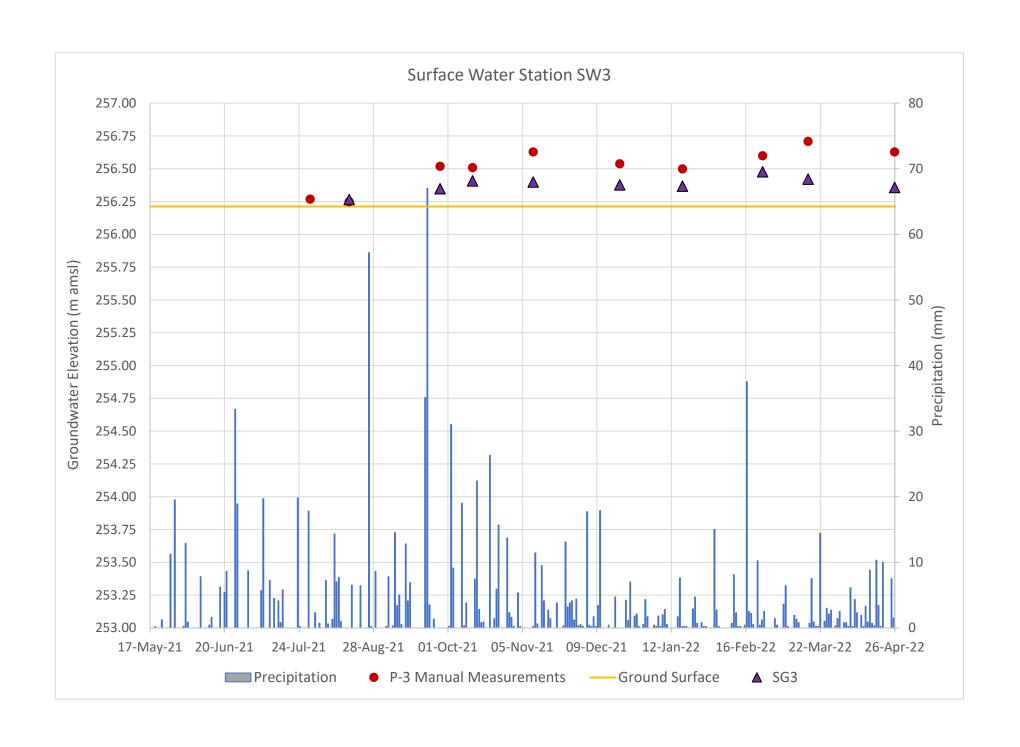


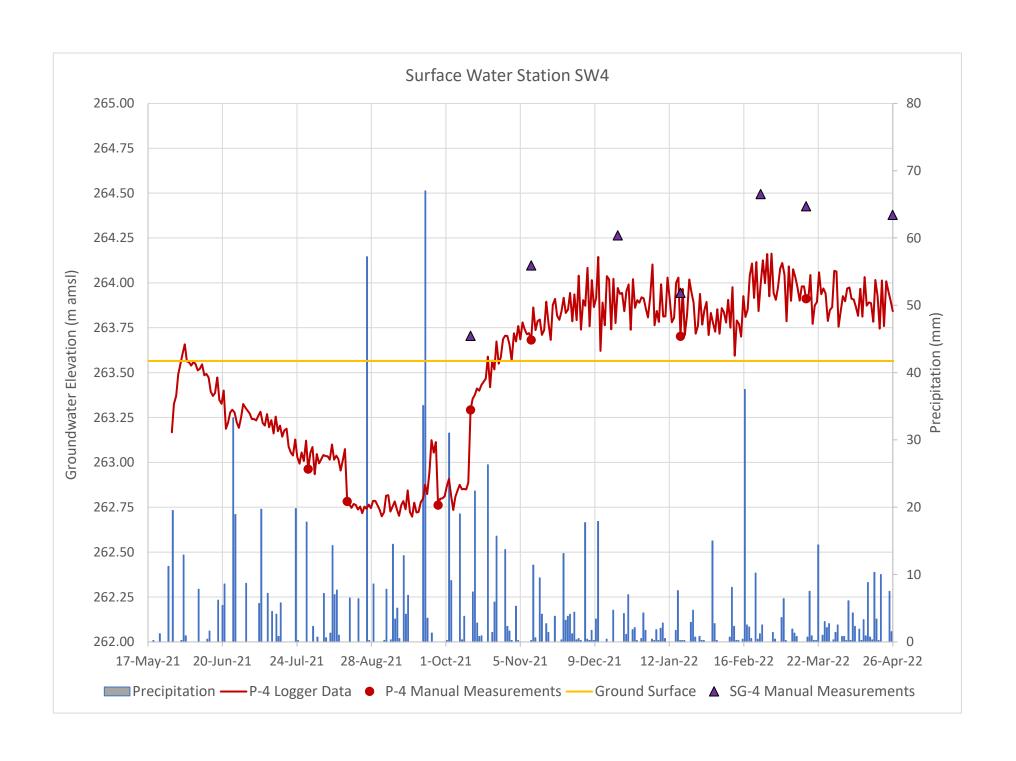


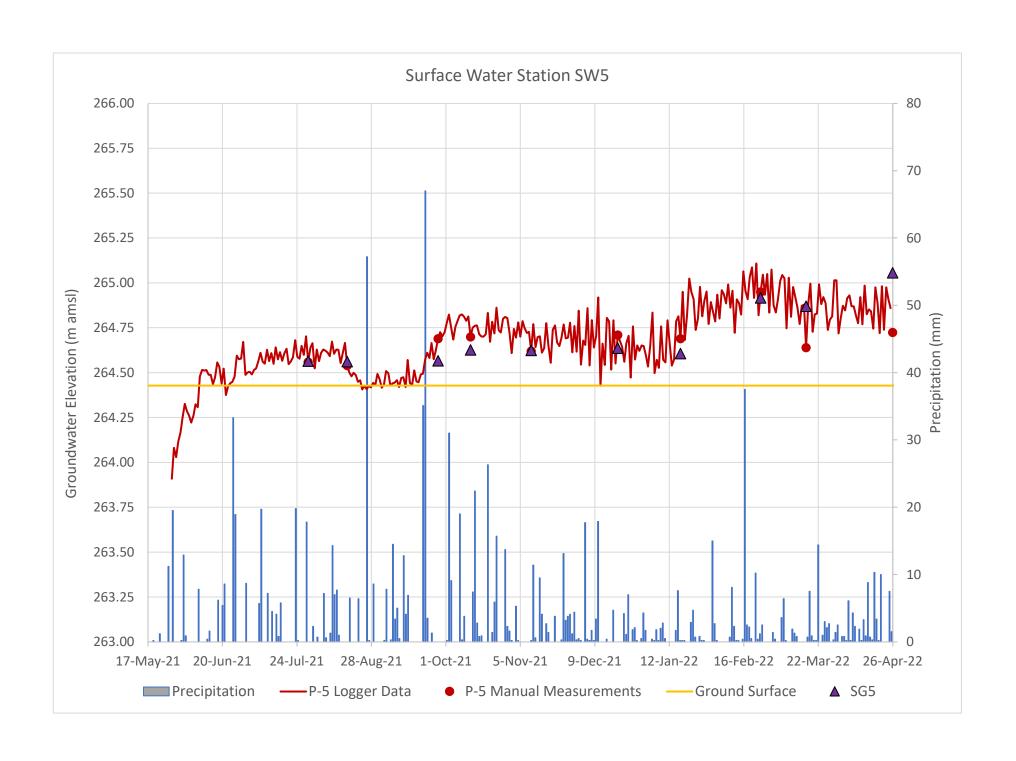




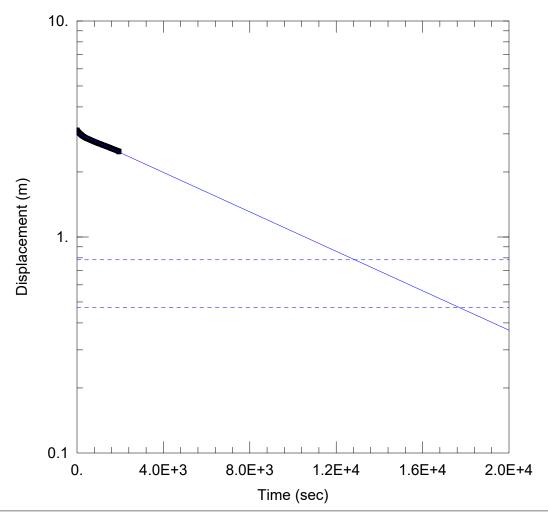








Appendix H – Single Well Response Test Data



Data Set: E:\LON\LON-21008138-A0\50 Input\Hydrogeological Work\SWRT Data\BH2MW.aqt

Date: 11/16/21 Time: 08:10:57

PROJECT INFORMATION

Company: EXP

Client: Auburn Developments Inc.

Project: LON-21008138 Location: Dorchester, Ontario Test Date: May 17 2021

AQUIFER DATA

Saturated Thickness: 5. m Anisotropy Ratio (Kz/Kr): 0.3

WELL DATA (BH2/MW)

Initial Displacement: 3.135 m

Total Well Penetration Depth: 3.53 m

Casing Radius: 0.0254 m

Static Water Column Height: 3.53 m

Screen Length: 1.524 m Well Radius: 0.1048 m

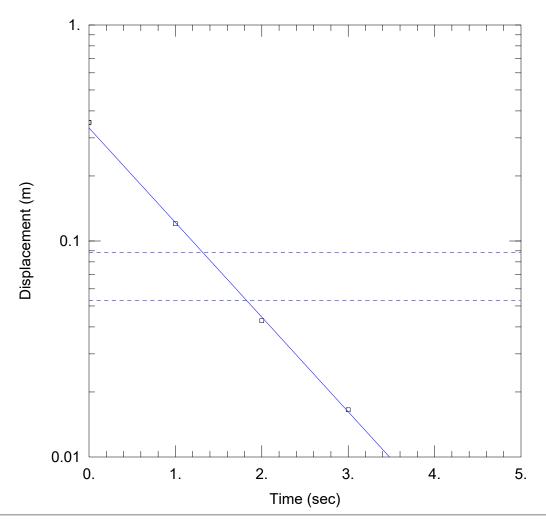
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 7.3E-8 m/sec

y0 = 3.03 m



Data Set: E:\LON\LON-21008138-A0\50 Input\Hydrogeological Work\SWRT Data\BH4MW.aqt

Date: 11/16/21 Time: 08:10:36

PROJECT INFORMATION

Company: EXP

Client: Auburn Developments Inc.

Project: LON-21008138 Location: Dorchester, Ontario Test Date: May 17 2021

AQUIFER DATA

Saturated Thickness: 2.74 m Anisotropy Ratio (Kz/Kr): 0.4

WELL DATA (BH4/MW)

Initial Displacement: 0.3536 m
Total Well Penetration Depth: 3.1 m

Casing Radius: 0.0254 m

Static Water Column Height: 3.1 m

Screen Length: 1.524 m Well Radius: 0.1048 m

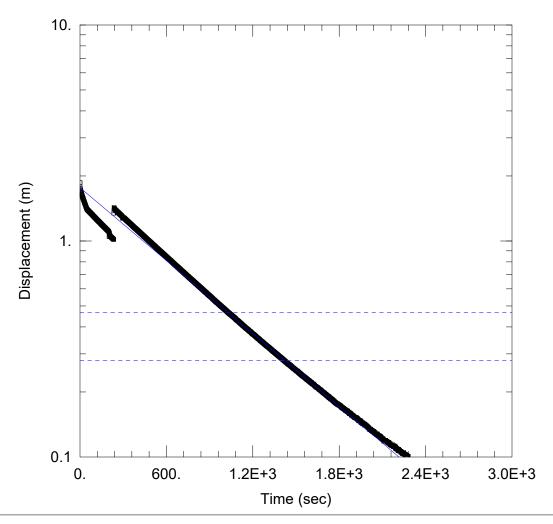
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0008171 m/sec

y0 = 0.3336 m



Data Set: E:\LON\LON-21008138-A0\50 Input\Hydrogeological Work\SWRT Data\BH7MW A.aqt

Date: 11/16/21 Time: 08:09:45

PROJECT INFORMATION

Company: EXP

Client: Auburn Developments Inc.

Project: LON-21008138 Location: Dorchester, Ontario Test Date: May 17 2021

AQUIFER DATA

Saturated Thickness: 6.71 m Anisotropy Ratio (Kz/Kr): 0.3

WELL DATA (BH7/MW-A)

Initial Displacement: 1.861 m

Static Water Column Height: 5.15 m

Total Well Penetration Depth: 5.15 m

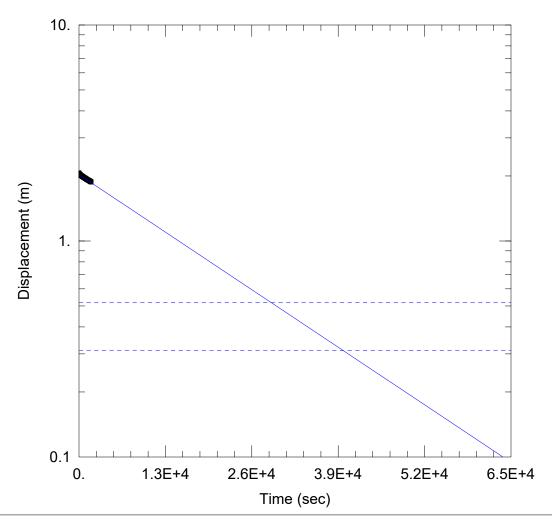
Screen Length: 1.524 m Well Radius: 0.1048 m

Casing Radius: 0.0254 m

SOLUTION

Aquifer Model: Unconfined Solution Method: Hvorslev

K = 9.0E-7 m/sec y0 = 1.765 m



Data Set: E:\LON\LON-21008138-A0\50 Input\Hydrogeological Work\SWRT Data\BH8MW.aqt

Date: 11/16/21 Time: 08:10:10

PROJECT INFORMATION

Company: EXP

Client: Auburn Developments Inc.

Project: LON-21008138 Location: Dorchester, Ontario Test Date: May 17 2021

AQUIFER DATA

Saturated Thickness: 3.6 m Anisotropy Ratio (Kz/Kr): 0.35

WELL DATA (BH8/MW)

Initial Displacement: 2.07 m

Total Well Penetration Depth: 3.21 m

Casing Radius: 0.0254 m

Static Water Column Height: 3.21 m

Screen Length: 1.524 m Well Radius: 0.1048 m

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 3.2E-8 m/sec y0 = 2.029 m

Appendix I – Water Quality Tables

Groundwater Quality Results Hunter Farm Development, Dorchester, ON Project No. LON-21008138



| | | | 28-Sep-21 | 17-Mar-22 | 28-Sep-21 | 17-Mar-22 | 28-Sep-21 | 17-Mar-22 | 28-Sep-21 | 17-Mar-22 |
|---|--------------|---------|---------------|-----------------|---------------|------------------|--------------|-----------------|-------------|--------------|
| CRITERIA | ODWQS | UNITS | | /MW | | MW-A | | MW-B | | /MW |
| Calculated Parameters | | | | | | | | | | |
| Anion Sum | - | me/L | 7.37 | 6.08 | 4.23 | 11.2 | 9.63 | 9.1 | 3.38 | 3.78 |
| Bicarb. Alkalinity (calc. as CaCO3) | - | mg/L | 280 | 220 | 140 | 450 | 400 | 380 | 130 | 180 |
| Calculated TDS | - | mg/L | 390 | 330 | 230 | 610 | 510 | 460 | 180 | 190 |
| Carb. Alkalinity (calc. as CaCO3) | - | mg/L | 2.6 | 2.8 | 1.1 | 2.9 | 3.4 | 1.6 | 1.4 | 2.1 |
| Cation Sum | - | me/L | 7.83 | 6.23 | 4.29 | 11.6 | 10.3 | 8.95 | 3.4 | 3.89 |
| Hardness (CaCO3) | - | mg/L | 330 | 290 | 180 | 350 | 490 | 420 | 140 | 190 |
| Ion Balance (% Difference) | - | % | 3.05 | 1.25 | 0.63 | 1.61 | 3.31 | 0.86 | 0.31 | 1.46 |
| Langelier Index (@ 20C) | - | N/A | 0.974 | 0.987 | 0.386 | 1 | 1.25 | 0.859 | 0.408 | 0.728 |
| Langelier Index (@ 4C) | - | N/A | 0.726 | 0.739 | 0.137 | 0.755 | 1 | 0.611 | 0.158 | 0.478 |
| Saturation pH (@ 20C) | - | N/A | 7.02 | 7.14 | 7.52 | 6.83 | 6.7 | 6.78 | 7.63 | 7.36 |
| Saturation pH (@ 4C) | - | N/A | 7.27 | 7.39 | 7.77 | 7.08 | 6.95 | 7.03 | 7.88 | 7.61 |
| Inorganics | | | | | | | | | | |
| Total Ammonia-N | - | mg/L | <0.050 | <0.050 | <0.050 | 0.29 | 0.097 | 0.12 | <0.050 | <0.050 |
| Conductivity | - | umho/cm | 690 | 570 | 410 | 1000 | 840 | 840 | 320 | 350 |
| Dissolved Organic Carbon | - | mg/L | 3.7 | 5.2 | 4.8 | 9.5 | 10 | 7 | 4.1 | 1.2 |
| Orthophosphate (P) | - | mg/L | <0.010 | <0.010 | <0.010 | 0.011 | <0.010 | <0.010 | <0.010 | <0.010 |
| рН | - | рН | 8 | 8.13 | 7.91 | 7.83 | 7.95 | 7.64 | 8.04 | 8.09 |
| Dissolved Sulphate (SO4) | - | mg/L | 27 | 24 | 37 | 69 | 39 | 22 | 18 | 2.2 |
| Alkalinity (Total as CaCO3) | - | mg/L | 290 | 230 | 140 | 460 | 410 | 390 | 130 | 190 |
| Dissolved Chloride (Cl-) | - | mg/L | 38 | 24 | 18 | 24 | 24 | 33 | 9 | <1.0 |
| Nitrite (N) | 1 | mg/L | <0.010 | <0.010 | 0.026 | <0.010 | 0.055 | <0.010 | 0.015 | <0.010 |
| Nitrate (N) | 10 | mg/L | 0.11 | 5.23 | 1.08 | <0.10 | 0.26 | <0.10 | 0.54 | <0.10 |
| Nitrate + Nitrite (N) | - | mg/L | 0.11 | 5.23 | 1.11 | <0.10 | 0.31 | <0.10 | 0.56 | <0.10 |
| Metals | _ | | | | | | | | | |
| Dissolved Aluminum (Al) | - | ug/L | <4.9 | 8 | 7.3 | 6.7 | 5.9 | <4.9 | 9.4 | 6.1 |
| Dissolved Antimony (Sb) | 6 | ug/L | <0.50 | <0.50 | 0.71 | 0.62 | <0.50 | <0.50 | 0.51 | <0.50 |
| Dissolved Arsenic (As) | 10 | ug/L | 5.4 | <1.0 | 1 | 1.9 | <1.0 | <1.0 | <1.0 | <1.0 |
| Dissolved Barium (Ba) | 1000 | ug/L | 79 | 29 | 32 | 36 | 72 | 44 | 17 | 14 |
| Dissolved Beryllium (Be) | - | ug/L | <0.40 | <0.40 | <0.40 | <0.40 | <0.40 | <0.40 | <0.40 | <0.40 |
| Dissolved Boron (B) | 5000 | ug/L | 28 | 11 | 17 | 41 | 16 | <10 | 16 | 11 |
| Dissolved Cadmium (Cd) | 5 | ug/L | <0.090 | <0.090 | <0.090 | <0.090 | <0.090 | <0.090 | <0.090 | <0.090 |
| Dissolved Calcium (Ca) | - | ug/L | 92000 | 86000 | 53000 | 100000 | 140000 | 120000 | 42000 | 57000 |
| Dissolved Chromium (Cr) | 50 | ug/L | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 |
| Dissolved Cobalt (Co) | - | ug/L | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | 0.55 | <0.50 | <0.50 |
| Dissolved Copper (Cu) | - | ug/L | 17 | 1.1 | 23 | 3.4 | 21 | 2.4 | 11 | 1.4 |
| Dissolved Iron (Fe) | - | ug/L | <100 | <100 | <100 | <100 | <100 | <100 | <100 | <100 |
| Dissolved Lead (Pb) | 10 | ug/L | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 |
| Dissolved Magnesium (Mg) | - | ug/L | 24000 | 18000 | 12000 | 24000 | 32000 | 28000 | 8800 | 12000 |
| Dissolved Manganese (Mn) | - | ug/L | 88 | 18 | 10 | 300 | 310 | 430 | <2.0 | <2.0 |
| Dissolved Molybdenum (Mo) | - | ug/L | 12 | 0.69 | 5.3 | 45 | 4.2 | 2 | 4.9 | <0.50 |
| Dissolved Nickel (Ni) | - | ug/L | 13 | <1.0 | 8.7 | 1 | 8.6 | 1.6 | 4.7 | <1.0 |
| Dissolved Phosphorus (P) | - | ug/L | <100 | <100 | <100 | <100 | <100 | <100 | <100 | <100 |
| Dissolved Potassium (K) | - | ug/L | 2800 | 2500 | 3500 | 1600 | 3600 | 2300 | 3100 | 1700 |
| Dissolved Selenium (Se) | 50 | ug/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| Dissolved Silicon (Si) | - | ug/L | 4700 | 2800 | 2000 | 6900 | 6900 | 3400 | 2500 | 2900 |
| Dissolved Silver (Ag) Dissolved Sodium (Na) | - | ug/L | <0.090 | <0.090 10000 | <0.090 | <0.090 100000 | <0.090 | <0.090 10000 | <0.090 | <0.090 |
| Dissolved Strontium (Sr) | <u> </u> | ug/L | 27000 | | 14000 | | 7300 | | 12000 | 1300 |
| Dissolved Thallium (TI) | - | ug/L | 180 <0.050 | 160 | 180 <0.050 | 140 <0.050 | 200 | 160 <0.050 | 120 | 81 <0.050 |
| Dissolved Titanium (Ti) | _ | ug/L | | <0.050 | | <0.050 | <0.050 | | <0.050 | |
| Dissolved Tranium (TI) | 20 | ug/L | <5.0 0.59 | <5.0 | <5.0 | <5.0 | <5.0 0.74 | <5.0 | <5.0 | <5.0 0.21 |
| , , | | ug/L | | 1.5 | 1.2 | 35 | 0.74 | 1.8 | 0.59 | 0.21 |
| Dissolved Vanadium (V) | - | ug/L | <0.50 59 | <0.50 <5.0 | <0.50 | 1.6 38 | 0.58 | <0.50 36 | <0.50 30 | <0.50 7 |
| Dissolved Zinc (Zn) | | ug/L | צכ | ₹ 5.0 | 110 | 30 | 44 | 30 | 30 | / |

TABLE NOTES:

 $\label{thm:compared} \textbf{Results compared to Ontario Drinking Water Quality Standards (ODWQS)}.$

Values highlighted GREY and bold exceed parameter guidelines

Surface Water Quality Results Hunter Farm Development, Dorchester, ON Project No. LON-21008138



| CRITERIA | PWQO | UNITS | 28-Sep-21 SW Stat | 17-Mar-22 tion1 | 28-Sep-21 SW Star | 17-Mar-22 tion 2 | 28-Sep-21 SW Stat | 17-Mar-22 ion 4 | 28-Sep-21 SW Stat | 17-Mar-22 ion 5 |
|--|--|--------------|----------------------|--------------------|----------------------|---------------------|----------------------|-----------------------|----------------------|--------------------|
| Calculated Parameters | | | | | | | | | | |
| Bicarb. Alkalinity (calc. as CaCO3) | - | mg/L | 390 | 570 | 250 | 220 | 70 | 38 | 120 | 220 |
| Calculated TDS | - | mg/L | 650 | 920 | 380 | 330 | 170 | 45 | 140 | 240 |
| Carb. Alkalinity (calc. as CaCO3) Hardness (CaCO3) | - | mg/L mg/L | 3.5 400 | 2.8 640 | 3.6 310 | 2.3 | <1.0 130 | <1.0 44 | <1.0 130 | <1.0 220 |
| Langelier Index (@ 20C) | - | N/A | 1.18 | 1.23 | 1.13 | 0.897 | -0.628 | -1.19 | 0.15 | 0.165 |
| Langelier Index (@ 4C) | - | N/A | 0.93 | 0.981 | 0.882 | 0.648 | -0.878 | -1.44 | -0.101 | -0.085 |
| Saturation pH (@ 20C) | - | N/A | 6.8 | 6.49 | 7.06 | 7.14 | 7.94 | 8.61 | 7.71 | 7.28 |
| Saturation pH (@ 4C) | - | N/A | 7.05 | 6.73 | 7.31 | 7.38 | 8.19 | 8.86 | 7.97 | 7.53 |
| Inorganics | | <u> </u> | | 1 | | 1 | T | | T | |
| Total Ammonia-N | - | mg/L | 0.082 | 0.29 | <0.050 | <0.050 | 0.14 | <0.050 | 0.093 | 1.2 |
| Conductivity Total Organic Carbon (TOC) | - | umho/cm | 1200 41 | 1700 30 | 640 8.9 | 590 5.4 | 280 17 | 89 3.9 | 260 24 | 440 23 |
| Total Organic Carbon (TOC) Orthophosphate (P) | - | mg/L mg/L | 0.012 | <0.010 | 0.026 | <0.010 | 0.4 | 0.017 | 0.082 | 0.1 |
| рН | 6.5 - 8.5 | pH | 7.98 | 7.71 | 8.19 | 8.03 | 7.32 | 7.42 | 7.86 | 7.44 |
| Total Phosphorus | - | mg/L | 1.9 | 0.41 | 0.043 | 0.026 | 0.46 | 0.09 | 0.64 | 1.5 |
| Dissolved Sulphate (SO4) | - | mg/L | <1.0 | <1.0 | 36 | 23 | 47 | <1.0 | <1.0 | <1.0 |
| Turbidity | - | NTU | 9.3 | 45 | 1.1 | 0.7 | 2.5 | 0.8 | 5 | 7.2 |
| Alkalinity (Total as CaCO3) | - | mg/L | 390 | 570 | 250 | 230 | 70 | 38 | 120 | 220 |
| Dissolved Chloride (Cl-) | - | mg/L | 150 | 200 | 30 | 25 | 14 | 2.9 | 9.7 | 12 |
| Nitrite (N) | - | mg/L | <0.010 | <0.010 | 0.031 | <0.010 | 0.039 | <0.010 | <0.010 | <0.010 |
| Nitrate (N) | - | mg/L | <0.10 | <0.10 | 5.26 | 5.8 | 0.45 | <0.10 | <0.10 | <0.10 |
| Metals Discaluad Calaium (Ca) | T . | /1 | 120 | 200 | ٥٢ | 0.7 | l 20 | 12 | l 27 | C1 |
| Dissolved Calcium (Ca) | - | mg/L | 130 21 | 200 35 | 95 17 | 87 16 | 38 7.3 | 13 2.7 | 37 7.9 | 61 16 |
| Dissolved Magnesium (Mg) Dissolved Potassium (K) | + - | mg/L mg/L | 5 | 35 | 4 | 2 | 7.3 | 2.7 | 7.9 | 16 5 |
| Dissolved Sodium (Na) | - | mg/L | 89 | 120 | 12 | 11 | 2.5 | 1.1 | 3.4 | 3.9 |
| Total Aluminum (AI) | 75 | ug/L | 1300 | 84 | 67 | 75 | 140 | 100 | 940 | 1100 |
| Total Antimony (Sb) | 20 | ug/L | <0.50 | <0.50 | <0.50 | <0.50 | <0.50 | <5.0 | <0.50 | <0.50 |
| Total Arsenic (As) | 5 | ug/L | 7.3 | 2.7 | <1.0 | <1.0 | <1.0 | <10 | 1 | 1.2 |
| Total Barium (Ba) | <u> </u> | ug/L | 160 | 150 | 41 | 30 | 8.5 | <20 | 31 | 35 |
| Total Beryllium (Be) | 1100 | ug/L | <0.40 | <0.40 | <0.40 | <0.40 | <0.40 | <4.0 | <0.40 | <0.40 |
| Total Boron (B) | 200 | ug/L | 43 | 15 | 22 | 11 | 44 | <100 | 23 | 12 |
| Total Calmium (Cd) | 0.5 | ug/L | <0.090 | <0.090 | <0.090 | <0.090 | 0.11 | <0.90 | <0.090 | <0.090 |
| Total Calcium (Ca) Total Chromium (Cr) | 8.9 | ug/L ug/L | 160000 <5.0 | 240000 <5.0 | 110000 <5.0 | 91000 <5.0 | 41000 <5.0 | 8900 <50 | 42000 <5.0 | 67000 <5.0 |
| Total Cobalt (Co) | 0.9 | ug/L ug/L | 2.3 | 2.4 | <0.50 | <0.50 | 0.5 | <5.0 | <0.50 | <5.0 1 |
| Total Copper (Cu) | 5 | ug/L ug/L | 4 | 4.9 | 2.5 | 1.6 | 2 | <9.0 | 2.2 | 7.7 |
| Total Iron (Fe) | 300 | ug/L | 39000 | 39000 | 130 | 190 | 230 | <1000 | 1400 | 6200 |
| Total Lead (Pb) | 5 | ug/L | 2 | <0.50 | <0.50 | <0.50 | <0.50 | <5.0 | 1.6 | 2.4 |
| Total Magnesium (Mg) | - | ug/L | 24000 | 36000 | 19000 | 18000 | 7600 | 1600 | 9000 | 18000 |
| Total Manganese (Mn) | - | ug/L | 1400 | 2700 | 30 | 40 | 210 | 410 | 76 | 450 |
| Total Molybdenum (Mo) | 40 | ug/L | 0.82 | <0.50 | 1.3 | 0.64 | 1.3 | <5.0 | 1.2 | 0.94 |
| Total Nickel (Ni) | 25 | ug/L | 3.8 | 3 | <1.0 | <1.0 | <1.0 | <10 | 1.1 | 1.8 |
| Total Potassium (K) | - | ug/L | 5100 | 2400 | 4000 | 2500 | 7800 | <2000 | 3700 | 5500 |
| Total Selenium (Se) | 100 | ug/L | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 | <20 | <2.0 | <2.0 |
| Total Silicon (Si) | 0.1 | ug/L | 9900 | 9400 | 4300 | 2800 | 1800 | <500 | 3500 | 3800 |
| Total Silver (Ag) Total Sodium (Na) | - 0.1 | ug/L ug/L | <0.090 93000 | <0.090 120000 | <0.090 14000 | <0.090 12000 | <0.090 1900 | < 0.90 1200 | <0.090 3000 | <0.090 4300 |
| Total Strontium (Sr) | - | ug/L | 280 | 390 | 190 | 150 | 44 | <10 | 57 | 77 |
| Total Thallium (TI) | 0.3 | ug/L | <0.050 | <0.050 | <0.050 | <0.050 | <0.050 | <0.50 | <0.050 | <0.050 |
| Total Titanium (Ti) | - | ug/L | 48 | 7.3 | 5.6 | 5.1 | 7.3 | <50 | 24 | 29 |
| Total Tungsten (W) | 30 | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | <1.0 | <10 | <1.0 | <1.0 |
| Total Uranium (U) | 5 | ug/L | 1.4 | 0.33 | 2.4 | 1.6 | 0.1 | <1.0 | 0.44 | 0.81 |
| Total Vanadium (V) | 6 | ug/L | 3.4 | 0.7 | 0.87 | 0.53 | 0.79 | <5.0 | 2.3 | 2.8 |
| Total Zinc (Zn) | 20 | ug/L | 26 | 43 | <5.0 | <5.0 | 5.4 | <50 | 18 | 80 |
| Total Zirconium (Zr) | 4 | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | <1.0 | <10 | <1.0 | <1.0 |
| Dissolved Metals Dissolved Aluminum (Al) | _ | ug/l | <4.9 | _ | 9.4 | - | 24 | - | 11 | |
| Dissolved Antimony (Sb) | + - | ug/L ug/L | <0.50 | - | <0.50 | - | <0.50 | - | <0.50 | - |
| Dissolved Artificity (3b) | - | ug/L ug/L | <1.0 | - | <1.0 | - | <1.0 | - | <1.0 | - |
| Dissolved Barium (Ba) | - | ug/L | 57 | - | 41 | - | 8 | - | 20 | - |
| Dissolved Beryllium (Be) | - | ug/L | <0.40 | - | <0.40 | - | <0.40 | - | <0.40 | - |
| Dissolved Bismuth (Bi) | - | ug/L | <1.0 | - | <1.0 | - | <1.0 | - | <1.0 | - |
| Dissolved Boron (B) | - | ug/L | 34 | - | 21 | - | 44 | - | 22 | - |
| Dissolved Calaium (Cd) | - | ug/L | <0.090 | - | <0.090 | - | 0.093 | - | <0.090 | - |
| Dissolved Calcium (Ca) | - | ug/L | 140000 | - | 100000 | - | 39000 | - | 41000 | - |
| Dissolved Chromium (Cr) Dissolved Cobalt (Co) | - | ug/L ug/L | <5.0 <0.50 | - | <5.0 <0.50 | - | <5.0 <0.50 | - | <5.0 <0.50 | - |
| Dissolved Copper (Cu) | - | ug/L ug/L | <0.50 | - | <0.50 1.9 | - | <0.50 1.7 | - | <0.50 | - |
| Dissolved Copper (Cu) | - | ug/L ug/L | <100 | - | <100 | - | 110 | - | 150 | - |
| Dissolved Lead (Pb) | - | ug/L | <0.50 | - | <0.50 | - | <0.50 | - | <0.50 | - |
| Dissolved Lithium (Li) | - | ug/L | <5.0 | - | <5.0 | - | <5.0 | - | <5.0 | - |
| Dissolved Magnesium (Mg) | - | ug/L | 25000 | - | 19000 | - | 7600 | - | 9000 | - |
| Dissolved Manganese (Mn) | - | ug/L | 18 | - | 20 | - | 200 | - | <2.0 | - |
| Dissolved Molybdenum (Mo) | - | ug/L | 0.63 | - | 1.4 | - | 1.6 | - | 1.2 | - |
| Dissolved Nickel (Ni) | - | ug/L | 2.4 | - | <1.0 | - | <1.0 | - | <1.0 | - |
| Dissolved Phosphorus (P) | - | ug/L ug/L | <100 5100 | - | 100 | - | 510 | - | 270 | - |
| Dissolved Potassium (K) Dissolved Selenium (Se) | - | ug/L ug/L | <2.0 | - | 4000 <2.0 | - | 8200 <2.0 | - | 3500 <2.0 | - |
| Dissolved Silicon (Si) | | ug/L ug/L | 7200 | - | 4300 | - | 1500 | - | 2500 | - |
| Dissolved Silver (Ag) | - | ug/L ug/L | <0.090 | - | <0.090 | - | <0.090 | - | <0.090 | - |
| Dissolved Sodium (Na) | - | ug/L | 98000 | - | 13000 | - | 1900 | - | 3000 | - |
| Dissolved Strontium (Sr) | - | ug/L | 260 | - | 190 | - | 45 | - | 54 | - |
| Dissolved Tellurium (Te) | - | ug/L | <1.0 | - | <1.0 | - | <1.0 | - | <1.0 | - |
| Dissolved Thallium (TI) | <u> </u> | ug/L | <0.050 | - | <0.050 | - | <0.050 | - | <0.050 | - |
| Dissolved Tin (Sn) | - | ug/L | <1.0 | - | <1.0 | - | <1.0 | - | <1.0 | - |
| Dissolved Titanium (Ti) | - | ug/L | <5.0 | - | <5.0 | - | <5.0 | - | <5.0 | - |
| Dissolved Tungsten (W) | - | ug/L | <1.0 | - | <1.0 | - | <1.0 | - | <1.0 | - |
| Dissolved Uranium (U) | - | ug/L | 1.4 | - | 2.3 | - | 0.1 | - | 0.29 | - |
| Dissolved Vanadium (V) Dissolved Zinc (Zn) | - | ug/L ug/L | <0.50 <5.0 | - | 0.56 <5.0 | - | <0.50 <5.0 | - | 0.91 <5.0 | - |
| Dissolved Zirc (Zn) Dissolved Zirconium (Zr) | - | ug/L ug/L | <5.0 <1.0 | - | <5.0 <1.0 | - | <5.0 <1.0 | - | <5.0 <1.0 | - |
| | 1 | √6/ L | `1.0 | 1 | `1.0 | <u> </u> | `1.0 | <u> </u> | `1.0 | |

TABLE NOTES:
Results compared to Provincial Water Quality Objectives (PWQO), Ministry of the Environment and Energy (1994, revised 1999)

Values highlighted GREY and bold exceed parameter guidelines

Value in **BOLD** indicates detection limit exceeds parameter guideline

Due to limited amount of sample available for analysis at SW4, a smaller than usual portion of the sample was analyzed and detection limits were adjusted accordingly

Appendix J – Laboratory Chain of Custody



Your Project #: KCH-21008183 Site Location: HUNTER FARMS Your C.O.C. #: 870268-01-01

Attention: Kelli Dobbin

exp Services Inc London Branch 15701 Robin's Hill Rd Unit 2 London, ON CANADA N5V 0A5

> Report Date: 2022/03/30 Report #: R7065870

Version: 1 - Final

CERTIFICATE OF ANALYSIS

BUREAU VERITAS JOB #: C272761 Received: 2022/03/17, 15:15

Sample Matrix: Water # Samples Received: 8

| " Jumples Received. 5 | | Date | Date | | |
|--|----------|------------|------------|--------------------------|----------------------|
| Analyses | Quantity | Extracted | Analyzed | Laboratory Method | Analytical Method |
| Alkalinity | 8 | N/A | 2022/03/23 | CAM SOP-00448 | SM 23 2320 B m |
| Carbonate, Bicarbonate and Hydroxide | 8 | N/A | 2022/03/24 | CAM SOP-00102 | APHA 4500-CO2 D |
| Chloride by Automated Colourimetry | 8 | N/A | 2022/03/23 | CAM SOP-00463 | SM 23 4500-Cl E m |
| Conductivity | 8 | N/A | 2022/03/23 | CAM SOP-00414 | SM 23 2510 m |
| Dissolved Organic Carbon (DOC) (1) | 4 | N/A | 2022/03/24 | CAM SOP-00446 | SM 23 5310 B m |
| Hardness (calculated as CaCO3) | 8 | N/A | 2022/03/24 | CAM SOP | SM 2340 B |
| | | | | 00102/00408/00447 | |
| Lab Filtered Metals Analysis by ICP | 3 | 2022/03/23 | 2022/03/24 | CAM SOP-00408 | EPA 6010D m |
| Lab Filtered Metals Analysis by ICP | 1 | 2022/03/25 | 2022/03/28 | CAM SOP-00408 | EPA 6010D m |
| Lab Filtered Metals by ICPMS | 4 | 2022/03/23 | 2022/03/24 | CAM SOP-00447 | EPA 6020B m |
| Total Metals Analysis by ICPMS | 3 | N/A | 2022/03/25 | CAM SOP-00447 | EPA 6020B m |
| Total Metals Analysis by ICPMS | 1 | N/A | 2022/03/30 | CAM SOP-00447 | EPA 6020B m |
| Ion Balance (% Difference) | 4 | N/A | 2022/03/24 | | |
| Anion and Cation Sum | 4 | N/A | 2022/03/24 | | |
| Total Ammonia-N | 8 | N/A | 2022/03/23 | CAM SOP-00441 | USGS I-2522-90 m |
| Nitrate & Nitrite as Nitrogen in Water (2) | 8 | N/A | 2022/03/23 | CAM SOP-00440 | SM 23 4500-NO3I/NO2B |
| рН | 8 | 2022/03/22 | 2022/03/23 | CAM SOP-00413 | SM 4500H+ B m |
| Orthophosphate | 8 | N/A | 2022/03/23 | CAM SOP-00461 | EPA 365.1 m |
| Sat. pH and Langelier Index (@ 20C) | 8 | N/A | 2022/03/24 | | Auto Calc |
| Sat. pH and Langelier Index (@ 4C) | 8 | N/A | 2022/03/24 | | Auto Calc |
| Sulphate by Automated Colourimetry | 8 | N/A | 2022/03/24 | CAM SOP-00464 | EPA 375.4 m |
| Total Dissolved Solids (TDS calc) | 8 | N/A | 2022/03/24 | | Auto Calc |
| Total Organic Carbon (TOC) (3) | 4 | N/A | 2022/03/23 | CAM SOP-00446 | SM 23 5310B m |
| Total Phosphorus (Colourimetric) | 4 | 2022/03/23 | 2022/03/24 | CAM SOP-00407 | SM 23 4500 P B H m |
| Turbidity | 4 | N/A | 2022/03/22 | CAM SOP-00417 | SM 23 2130 B m |

Remarks:

Bureau Veritas is accredited to ISO/IEC 17025 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by Bureau Veritas are based upon recognized Provincial, Federal or US method compendia such as CCME, MELCC, EPA, APHA.



Your Project #: KCH-21008183 Site Location: HUNTER FARMS Your C.O.C. #: 870268-01-01

Attention: Kelli Dobbin

exp Services Inc London Branch 15701 Robin's Hill Rd Unit 2 London, ON CANADA N5V 0A5

Report Date: 2022/03/30

Report #: R7065870 Version: 1 - Final

CERTIFICATE OF ANALYSIS

BUREAU VERITAS JOB #: C272761

Received: 2022/03/17, 15:15

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in Bureau Veritas' profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and Bureau Veritas in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

Bureau Veritas liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. Bureau Veritas has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by Bureau Veritas, unless otherwise agreed in writing. Bureau Veritas is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Results relate to samples tested. When sampling is not conducted by Bureau Veritas, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

Reference Method suffix "m" indicates test methods incorporate validated modifications from specific reference methods to improve performance.

- * RPDs calculated using raw data. The rounding of final results may result in the apparent difference.
- (1) Dissolved Organic Carbon (DOC) present in the sample should be considered as non-purgeable DOC.
- (2) Values for calculated parameters may not appear to add up due to rounding of raw data and significant figures.
- (3) Total Organic Carbon (TOC) present in the sample should be considered as non-purgeable TOC.

Encryption Key

Please direct all questions regarding this Certificate of Analysis to your Project Manager.

Christine Gripton, Senior Project Manager Email: Christine.Gripton@bureauveritas.com

Phone# (519)652-9444

This report has been generated and distributed using a secure automated process.

Bureau Veritas has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.

Total Cover Pages : 2 Page 2 of 26



Client Project #: KCH-21008183
Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - COMPREHENSIVE (LAB FILTERED)

| Bureau Veritas ID | | | | | SDE609 | | SDE610 | | |
|-------------------------------------|---------|-----|---------|----------|--------------|----------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | MW3 | QC Batch | MW7A | RDL | QC Batch |
| Calculated Parameters | - | | | · | • | <u> </u> | | - | |
| Anion Sum | me/L | - | - | - | 6.08 | 7896590 | 11.2 | N/A | 7894695 |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | - | - | - | 220 | 7896580 | 450 | 1.0 | 7894693 |
| Calculated TDS | mg/L | - | 500 | - | 330 | 7896579 | 610 | 1.0 | 7894701 |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | - | - | - | 2.8 | 7896580 | 2.9 | 1.0 | 7894693 |
| Cation Sum | me/L | - | - | - | 6.23 | 7896590 | 11.6 | N/A | 7894695 |
| Hardness (CaCO3) | mg/L | - | 80:100 | - | 290 | 7896344 | 350 | 1.0 | 7894046 |
| lon Balance (% Difference) | % | - | - | - | 1.25 | 7896589 | 1.61 | N/A | 7894694 |
| Langelier Index (@ 20C) | N/A | - | - | - | 0.987 | 7896591 | 1.00 | | 7894699 |
| Langelier Index (@ 4C) | N/A | - | - | - | 0.739 | 7896592 | 0.755 | | 7894700 |
| Saturation pH (@ 20C) | N/A | - | - | - | 7.14 | 7896591 | 6.83 | | 7894699 |
| Saturation pH (@ 4C) | N/A | - | - | - | 7.39 | 7896592 | 7.08 | | 7894700 |
| Inorganics | | | | | | | | | |
| Total Ammonia-N | mg/L | - | - | - | <0.050 | 7899195 | 0.29 | 0.050 | 7899195 |
| Conductivity | umho/cm | - | - | - | 570 | 7897446 | 1000 | 1.0 | 7897446 |
| Dissolved Organic Carbon | mg/L | - | 5 | - | 5.2 | 7900197 | 9.5 | 0.40 | 7897137 |
| Orthophosphate (P) | mg/L | - | - | - | <0.010 | 7897503 | 0.011 | 0.010 | 7897503 |
| рН | рН | - | 6.5:8.5 | 6.5:8.5 | 8.13 | 7897448 | 7.83 | | 7897448 |
| Dissolved Sulphate (SO4) | mg/L | - | 500 | - | 24 | 7897496 | 69 | 1.0 | 7897496 |
| Alkalinity (Total as CaCO3) | mg/L | - | 30:500 | - | 230 | 7897442 | 460 | 1.0 | 7897442 |
| Dissolved Chloride (Cl-) | mg/L | - | 250 | - | 24 | 7897487 | 24 | 1.0 | 7897487 |
| Nitrite (N) | mg/L | 1 | - | - | <0.010 | 7897511 | <0.010 | 0.010 | 7897511 |
| Nitrate (N) | mg/L | 10 | - | - | 5.23 | 7897511 | <0.10 | 0.10 | 7897511 |
| Nitrate + Nitrite (N) | mg/L | 10 | - | - | 5.23 | 7897511 | <0.10 | 0.10 | 7897511 |
| Metals | | | | | | | | | |
| Dissolved Aluminum (Al) | ug/L | - | 100 | - | 8.0 | 7900101 | 6.7 | 4.9 | 7900101 |
| Dissolved Antimony (Sb) | ug/L | 6 | - | 20 | <0.50 | 7900101 | 0.62 | 0.50 | 7900101 |

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives

Ref. to MOEE Water Management document dated Feb.1999

N/A = Not Applicable



Client Project #: KCH-21008183
Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - COMPREHENSIVE (LAB FILTERED)

| Bureau Veritas ID | | | | | SDE609 | | SDE610 | | |
|---------------------------|-------|------|--------|----------|--------------|----------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | MW3 | QC Batch | MW7A | RDL | QC Batch |
| Dissolved Arsenic (As) | ug/L | 10 | - | 100 | <1.0 | 7900101 | 1.9 | 1.0 | 7900101 |
| Dissolved Barium (Ba) | ug/L | 1000 | - | - | 29 | 7900101 | 36 | 2.0 | 7900101 |
| Dissolved Beryllium (Be) | ug/L | - | - | 11 | <0.40 | 7900101 | <0.40 | 0.40 | 7900101 |
| Dissolved Boron (B) | ug/L | 5000 | - | 200 | 11 | 7900101 | 41 | 10 | 7900101 |
| Dissolved Cadmium (Cd) | ug/L | 5 | - | 0.2 | <0.090 | 7900101 | <0.090 | 0.090 | 7900101 |
| Dissolved Calcium (Ca) | ug/L | - | - | - | 86000 | 7900101 | 100000 | 200 | 7900101 |
| Dissolved Chromium (Cr) | ug/L | 50 | - | - | <5.0 | 7900101 | <5.0 | 5.0 | 7900101 |
| Dissolved Cobalt (Co) | ug/L | - | - | 0.9 | <0.50 | 7900101 | <0.50 | 0.50 | 7900101 |
| Dissolved Copper (Cu) | ug/L | - | 1000 | 5 | 1.1 | 7900101 | 3.4 | 0.90 | 7900101 |
| Dissolved Iron (Fe) | ug/L | - | 300 | 300 | <100 | 7900101 | <100 | 100 | 7900101 |
| Dissolved Lead (Pb) | ug/L | 10 | - | 5 | <0.50 | 7900101 | <0.50 | 0.50 | 7900101 |
| Dissolved Magnesium (Mg) | ug/L | - | - | - | 18000 | 7900101 | 24000 | 50 | 7900101 |
| Dissolved Manganese (Mn) | ug/L | - | 50 | - | 18 | 7900101 | 300 | 2.0 | 7900101 |
| Dissolved Molybdenum (Mo) | ug/L | - | - | 40 | 0.69 | 7900101 | 45 | 0.50 | 7900101 |
| Dissolved Nickel (Ni) | ug/L | - | - | 25 | <1.0 | 7900101 | 1.0 | 1.0 | 7900101 |
| Dissolved Phosphorus (P) | ug/L | - | - | - | <100 | 7900101 | <100 | 100 | 7900101 |
| Dissolved Potassium (K) | ug/L | - | - | - | 2500 | 7900101 | 1600 | 200 | 7900101 |
| Dissolved Selenium (Se) | ug/L | 50 | - | 100 | <2.0 | 7900101 | <2.0 | 2.0 | 7900101 |
| Dissolved Silicon (Si) | ug/L | - | - | - | 2800 | 7900101 | 6900 | 50 | 7900101 |
| Dissolved Silver (Ag) | ug/L | - | - | 0.1 | <0.090 | 7900101 | <0.090 | 0.090 | 7900101 |
| Dissolved Sodium (Na) | ug/L | - | 200000 | - | 10000 | 7900101 | 100000 | 100 | 7900101 |
| Dissolved Strontium (Sr) | ug/L | - | - | - | 160 | 7900101 | 140 | 1.0 | 7900101 |
| Dissolved Thallium (TI) | ug/L | - | - | 0.3 | <0.050 | 7900101 | <0.050 | 0.050 | 7900101 |
| Dissolved Titanium (Ti) | ug/L | - | - | - | <5.0 | 7900101 | <5.0 | 5.0 | 7900101 |
| Dissolved Uranium (U) | ug/L | 20 | - | 5 | 1.5 | 7900101 | 35 | 0.10 | 7900101 |
| Dissolved Vanadium (V) | ug/L | - | ı | 6 | <0.50 | 7900101 | 1.6 | 0.50 | 7900101 |
| Dissolved Zinc (Zn) | ug/L | - | 5000 | 30 | <5.0 | 7900101 | 38 | 5.0 | 7900101 |

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level Exceeds both criteria/levels

RDL = Reportable Detection Limit QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives



Client Project #: KCH-21008183
Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - COMPREHENSIVE (LAB FILTERED)

| Bureau Veritas ID | | | | | SDE611 | | SDE612 | | |
|-------------------------------------|---------|-----|---------|----------|--------------|----------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | MW7B | QC Batch | MW9 | RDL | QC Batch |
| Calculated Parameters | · | | | · | • | · | | - | |
| Anion Sum | me/L | - | - | - | 9.10 | 7894695 | 3.78 | N/A | 7894695 |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | 1 | - | - | 380 | 7894693 | 180 | 1.0 | 7894693 |
| Calculated TDS | mg/L | 1 | 500 | - | 460 | 7894701 | 190 | 1.0 | 7894701 |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | 1 | - | - | 1.6 | 7894693 | 2.1 | 1.0 | 7894693 |
| Cation Sum | me/L | - | - | - | 8.95 | 7894695 | 3.89 | N/A | 7894695 |
| Hardness (CaCO3) | mg/L | - | 80:100 | - | 420 | 7894046 | 190 | 1.0 | 7894046 |
| Ion Balance (% Difference) | % | - | - | - | 0.860 | 7894694 | 1.46 | N/A | 7894694 |
| Langelier Index (@ 20C) | N/A | - | - | - | 0.859 | 7894699 | 0.728 | | 7894699 |
| Langelier Index (@ 4C) | N/A | - | - | - | 0.611 | 7894700 | 0.478 | | 7894700 |
| Saturation pH (@ 20C) | N/A | - | - | - | 6.78 | 7894699 | 7.36 | | 7894699 |
| Saturation pH (@ 4C) | N/A | - | - | - | 7.03 | 7894700 | 7.61 | | 7894700 |
| Inorganics | | | | | | | | | |
| Total Ammonia-N | mg/L | - | - | - | 0.12 | 7899195 | <0.050 | 0.050 | 7899195 |
| Conductivity | umho/cm | 1 | - | - | 840 | 7897464 | 350 | 1.0 | 7897446 |
| Dissolved Organic Carbon | mg/L | - | 5 | - | 7.0 | 7897137 | 1.2 | 0.40 | 7897137 |
| Orthophosphate (P) | mg/L | ı | 1 | - | <0.010 | 7897503 | <0.010 | 0.010 | 7897503 |
| рН | рН | 1 | 6.5:8.5 | 6.5:8.5 | 7.64 | 7897458 | 8.09 | | 7897448 |
| Dissolved Sulphate (SO4) | mg/L | ı | 500 | - | 22 | 7897496 | 2.2 | 1.0 | 7897496 |
| Alkalinity (Total as CaCO3) | mg/L | ı | 30:500 | - | 390 | 7897455 | 190 | 1.0 | 7897442 |
| Dissolved Chloride (Cl-) | mg/L | 1 | 250 | - | 33 | 7897487 | <1.0 | 1.0 | 7897487 |
| Nitrite (N) | mg/L | 1 | 1 | - | <0.010 | 7897511 | <0.010 | 0.010 | 7897511 |
| Nitrate (N) | mg/L | 10 | 1 | - | <0.10 | 7897511 | <0.10 | 0.10 | 7897511 |
| Nitrate + Nitrite (N) | mg/L | 10 | 1 | - | <0.10 | 7897511 | <0.10 | 0.10 | 7897511 |
| Metals | | | | | | | | | |
| Dissolved Aluminum (AI) | ug/L | ı | 100 | - | <4.9 | 7900101 | 6.1 | 4.9 | 7900101 |
| Dissolved Antimony (Sb) | ug/L | 6 | - | 20 | <0.50 | 7900101 | <0.50 | 0.50 | 7900101 |

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives

Ref. to MOEE Water Management document dated Feb.1999

N/A = Not Applicable



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - COMPREHENSIVE (LAB FILTERED)

| Bureau Veritas ID | | | | | SDE611 | | SDE612 | | |
|---------------------------|-------|------|--------|----------|--------------|----------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | MW7B | QC Batch | MW9 | RDL | QC Batch |
| Dissolved Arsenic (As) | ug/L | 10 | - | 100 | <1.0 | 7900101 | <1.0 | 1.0 | 7900101 |
| Dissolved Barium (Ba) | ug/L | 1000 | - | - | 44 | 7900101 | 14 | 2.0 | 7900101 |
| Dissolved Beryllium (Be) | ug/L | - | - | 11 | <0.40 | 7900101 | <0.40 | 0.40 | 7900101 |
| Dissolved Boron (B) | ug/L | 5000 | - | 200 | <10 | 7900101 | 11 | 10 | 7900101 |
| Dissolved Cadmium (Cd) | ug/L | 5 | 1 | 0.2 | <0.090 | 7900101 | <0.090 | 0.090 | 7900101 |
| Dissolved Calcium (Ca) | ug/L | - | - | - | 120000 | 7900101 | 57000 | 200 | 7900101 |
| Dissolved Chromium (Cr) | ug/L | 50 | - | - | <5.0 | 7900101 | <5.0 | 5.0 | 7900101 |
| Dissolved Cobalt (Co) | ug/L | - | 1 | 0.9 | 0.55 | 7900101 | <0.50 | 0.50 | 7900101 |
| Dissolved Copper (Cu) | ug/L | - | 1000 | 5 | 2.4 | 7900101 | 1.4 | 0.90 | 7900101 |
| Dissolved Iron (Fe) | ug/L | - | 300 | 300 | <100 | 7900101 | <100 | 100 | 7900101 |
| Dissolved Lead (Pb) | ug/L | 10 | - | 5 | <0.50 | 7900101 | <0.50 | 0.50 | 7900101 |
| Dissolved Magnesium (Mg) | ug/L | - | - | - | 28000 | 7900101 | 12000 | 50 | 7900101 |
| Dissolved Manganese (Mn) | ug/L | - | 50 | - | 430 | 7900101 | <2.0 | 2.0 | 7900101 |
| Dissolved Molybdenum (Mo) | ug/L | - | - | 40 | 2.0 | 7900101 | <0.50 | 0.50 | 7900101 |
| Dissolved Nickel (Ni) | ug/L | - | - | 25 | 1.6 | 7900101 | <1.0 | 1.0 | 7900101 |
| Dissolved Phosphorus (P) | ug/L | - | - | - | <100 | 7900101 | <100 | 100 | 7900101 |
| Dissolved Potassium (K) | ug/L | - | - | - | 2300 | 7900101 | 1700 | 200 | 7900101 |
| Dissolved Selenium (Se) | ug/L | 50 | - | 100 | <2.0 | 7900101 | <2.0 | 2.0 | 7900101 |
| Dissolved Silicon (Si) | ug/L | - | - | - | 3400 | 7900101 | 2900 | 50 | 7900101 |
| Dissolved Silver (Ag) | ug/L | - | - | 0.1 | <0.090 | 7900101 | <0.090 | 0.090 | 7900101 |
| Dissolved Sodium (Na) | ug/L | - | 200000 | - | 10000 | 7900101 | 1300 | 100 | 7900101 |
| Dissolved Strontium (Sr) | ug/L | - | - | - | 160 | 7900101 | 81 | 1.0 | 7900101 |
| Dissolved Thallium (TI) | ug/L | - | - | 0.3 | <0.050 | 7900101 | <0.050 | 0.050 | 7900101 |
| Dissolved Titanium (Ti) | ug/L | - | - | - | <5.0 | 7900101 | <5.0 | 5.0 | 7900101 |
| Dissolved Uranium (U) | ug/L | 20 | - | 5 | 1.8 | 7900101 | 0.21 | 0.10 | 7900101 |
| Dissolved Vanadium (V) | ug/L | - | - | 6 | <0.50 | 7900101 | <0.50 | 0.50 | 7900101 |
| Dissolved Zinc (Zn) | ug/L | - | 5000 | 30 | 36 | 7900101 | 7.0 | 5.0 | 7900101 |

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives



Client Project #: KCH-21008183
Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - SURFACE WATER (WATER)

| Bureau Veritas ID | | | | | SDE613 | | SDE614 | | |
|-------------------------------------|---------|-----|---------|----------|--------------|-------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | SW1 | RDL | SW2 | RDL | QC Batch |
| Calculated Parameters | | | | | | | | | |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | - | - | - | 570 | 1.0 | 220 | 1.0 | 7894693 |
| Calculated TDS | mg/L | - | 500 | - | 920 | 1.0 | 330 | 1.0 | 7894701 |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | - | - | - | 2.8 | 1.0 | 2.3 | 1.0 | 7894693 |
| Hardness (CaCO3) | mg/L | - | 80:100 | - | 640 | 1.0 | 280 | 1.0 | 7894046 |
| Langelier Index (@ 20C) | N/A | - | - | - | 1.23 | | 0.897 | | 7894699 |
| Langelier Index (@ 4C) | N/A | ı | - | - | 0.981 | | 0.648 | | 7894700 |
| Saturation pH (@ 20C) | N/A | - | - | - | 6.49 | | 7.14 | | 7894699 |
| Saturation pH (@ 4C) | N/A | - | - | - | 6.73 | | 7.38 | | 7894700 |
| Inorganics | • | | - | | | | | | • |
| Total Ammonia-N | mg/L | - | - | - | 0.29 | 0.050 | <0.050 | 0.050 | 7899195 |
| Conductivity | umho/cm | - | - | - | 1700 | 1.0 | 590 | 1.0 | 7897446 |
| Total Organic Carbon (TOC) | mg/L | ı | - | - | 30 | 0.40 | 5.4 | 0.40 | 7898671 |
| Orthophosphate (P) | mg/L | - | - | ı | <0.010 | 0.010 | <0.010 | 0.010 | 7897503 |
| рН | рН | - | 6.5:8.5 | 6.5:8.5 | 7.71 | | 8.03 | | 7897448 |
| Total Phosphorus | mg/L | 1 | ı | 0.01 | 0.41 | 0.02 | 0.026 | 0.004 | 7899137 |
| Dissolved Sulphate (SO4) | mg/L | 1 | 500 | 1 | <1.0 | 1.0 | 23 | 1.0 | 7897496 |
| Turbidity | NTU | - | 5 | - | 45 | 0.1 | 0.7 | 0.1 | 7896234 |
| Alkalinity (Total as CaCO3) | mg/L | 1 | 30:500 | ı | 570 | 1.0 | 230 | 1.0 | 7897442 |
| Dissolved Chloride (Cl-) | mg/L | 1 | 250 | 1 | 200 | 2.0 | 25 | 1.0 | 7897487 |
| Nitrite (N) | mg/L | 1 | 1 | ı | <0.010 | 0.010 | <0.010 | 0.010 | 7897511 |
| Nitrate (N) | mg/L | 10 | - | - | <0.10 | 0.10 | 5.80 | 0.10 | 7897511 |
| Metals | • | | - | | | | | | • |
| Dissolved Calcium (Ca) | mg/L | - | - | - | 200 | 0.05 | 87 | 0.05 | 7900083 |
| Dissolved Magnesium (Mg) | mg/L | - | - | 1 | 35 | 0.05 | 16 | 0.05 | 7900083 |
| Dissolved Potassium (K) | mg/L | - | - | 1 | 3 | 1 | 2 | 1 | 7900083 |
| Dissolved Sodium (Na) | mg/L | - | 200 | - | 120 | 0.5 | 11 | 0.5 | 7900083 |
| Total Aluminum (Al) | ug/L | - | 100 | - | 84 | 4.9 | 75 | 4.9 | 7903614 |

No Fill Grey Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical

Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - SURFACE WATER (WATER)

| Bureau Veritas ID | | | | | SDE613 | | SDE614 | | |
|-----------------------|-------|------|--------|----------|--------------|-------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | SW1 | RDL | SW2 | RDL | QC Batch |
| Total Antimony (Sb) | ug/L | 6 | - | 20 | <0.50 | 0.50 | <0.50 | 0.50 | 7903614 |
| Total Arsenic (As) | ug/L | 10 | - | 100 | 2.7 | 1.0 | <1.0 | 1.0 | 7903614 |
| Total Barium (Ba) | ug/L | 1000 | - | - | 150 | 2.0 | 30 | 2.0 | 7903614 |
| Total Beryllium (Be) | ug/L | - | - | 11 | <0.40 | 0.40 | <0.40 | 0.40 | 7903614 |
| Total Boron (B) | ug/L | 5000 | - | 200 | 15 | 10 | 11 | 10 | 7903614 |
| Total Cadmium (Cd) | ug/L | 5 | - | 0.2 | <0.090 | 0.090 | <0.090 | 0.090 | 7903614 |
| Total Calcium (Ca) | ug/L | - | - | 1 | 240000 | 200 | 91000 | 200 | 7903614 |
| Total Chromium (Cr) | ug/L | 50 | - | 1 | <5.0 | 5.0 | <5.0 | 5.0 | 7903614 |
| Total Cobalt (Co) | ug/L | - | - | 0.9 | 2.4 | 0.50 | <0.50 | 0.50 | 7903614 |
| Total Copper (Cu) | ug/L | - | 1000 | 5 | 4.9 | 0.90 | 1.6 | 0.90 | 7903614 |
| Total Iron (Fe) | ug/L | - | 300 | 300 | 39000 | 100 | 190 | 100 | 7903614 |
| Total Lead (Pb) | ug/L | 10 | - | 5 | <0.50 | 0.50 | <0.50 | 0.50 | 7903614 |
| Total Magnesium (Mg) | ug/L | - | - | 1 | 36000 | 50 | 18000 | 50 | 7903614 |
| Total Manganese (Mn) | ug/L | - | 50 | ı | 2700 | 2.0 | 40 | 2.0 | 7903614 |
| Total Molybdenum (Mo) | ug/L | - | - | 40 | <0.50 | 0.50 | 0.64 | 0.50 | 7903614 |
| Total Nickel (Ni) | ug/L | - | - | 25 | 3.0 | 1.0 | <1.0 | 1.0 | 7903614 |
| Total Potassium (K) | ug/L | - | - | 1 | 2400 | 200 | 2500 | 200 | 7903614 |
| Total Selenium (Se) | ug/L | 50 | - | 100 | <2.0 | 2.0 | <2.0 | 2.0 | 7903614 |
| Total Silicon (Si) | ug/L | - | - | 1 | 9400 | 50 | 2800 | 50 | 7903614 |
| Total Silver (Ag) | ug/L | - | - | 0.1 | <0.090 | 0.090 | <0.090 | 0.090 | 7903614 |
| Total Sodium (Na) | ug/L | - | 200000 | ı | 120000 | 100 | 12000 | 100 | 7903614 |
| Total Strontium (Sr) | ug/L | - | - | 1 | 390 | 1.0 | 150 | 1.0 | 7903614 |
| Total Thallium (Tl) | ug/L | - | - | 0.3 | <0.050 | 0.050 | <0.050 | 0.050 | 7903614 |
| Total Titanium (Ti) | ug/L | - | - | - | 7.3 | 5.0 | 5.1 | 5.0 | 7903614 |
| Total Tungsten (W) | ug/L | - | - | 30 | <1.0 | 1.0 | <1.0 | 1.0 | 7903614 |
| Total Uranium (U) | ug/L | 20 | - | 5 | 0.33 | 0.10 | 1.6 | 0.10 | 7903614 |
| Total Vanadium (V) | ug/L | - | - | 6 | 0.70 | 0.50 | 0.53 | 0.50 | 7903614 |
| Total Zinc (Zn) | ug/L | - | 5000 | 30 | 43 | 5.0 | <5.0 | 5.0 | 7903614 |

No Fill
Grey
Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical

Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - SURFACE WATER (WATER)

| Bureau Veritas ID | | | | | SDE613 | | SDE614 | | |
|----------------------|-------|-----|-----|----------|--------------|-----|--------------|-----|----------|
| Sampling Date | | | | | 2022/03/17 | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | SW1 | RDL | SW2 | RDL | QC Batch |
| Total Zirconium (Zr) | ug/L | - | - | 4 | <1.0 | 1.0 | <1.0 | 1.0 | 7903614 |

No Fill

No Exceedance

Grey

Exceeds 1 criteria policy/level

Black

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical

Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - SURFACE WATER (WATER)

| Bureau Veritas ID | | | | | SDE615 | | | SDE616 | | |
|-------------------------------------|---------|-----|---------|----------|--------------|-------|----------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | SW4 | RDL | QC Batch | SW5 | RDL | QC Batch |
| Calculated Parameters | | | | | | | | | | |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | - | - | - | 38 | 1.0 | 7894693 | 220 | 1.0 | 7894693 |
| Calculated TDS | mg/L | - | 500 | - | 45 | 1.0 | 7894701 | 240 | 1.0 | 7894701 |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | - | - | - | <1.0 | 1.0 | 7894693 | <1.0 | 1.0 | 7894693 |
| Hardness (CaCO3) | mg/L | - | 80:100 | - | 44 | 1.0 | 7894046 | 220 | 1.0 | 7894046 |
| Langelier Index (@ 20C) | N/A | - | - | - | -1.19 | | 7894699 | 0.165 | | 7894699 |
| Langelier Index (@ 4C) | N/A | - | - | - | -1.44 | | 7894700 | -0.0850 | | 7894700 |
| Saturation pH (@ 20C) | N/A | - | - | - | 8.61 | | 7894699 | 7.28 | | 7894699 |
| Saturation pH (@ 4C) | N/A | - | - | - | 8.86 | | 7894700 | 7.53 | | 7894700 |
| Inorganics | • | | , | | | | | | | |
| Total Ammonia-N | mg/L | - | - | - | <0.050 | 0.050 | 7899195 | 1.2 | 0.050 | 7899195 |
| Conductivity | umho/cm | - | - | - | 89 | 1.0 | 7897446 | 440 | 1.0 | 7897446 |
| Total Organic Carbon (TOC) | mg/L | 1 | - | - | 3.9 | 0.40 | 7898671 | 23 | 2.0 | 7898671 |
| Orthophosphate (P) | mg/L | - | - | - | 0.017 | 0.010 | 7897503 | 0.10 | 0.010 | 7897503 |
| рН | рН | - | 6.5:8.5 | 6.5:8.5 | 7.42 | | 7897448 | 7.44 | | 7897448 |
| Total Phosphorus | mg/L | - | - | 0.01 | 0.09 | 0.02 | 7899137 | 1.5 | 0.02 | 7899137 |
| Dissolved Sulphate (SO4) | mg/L | - | 500 | 1 | <1.0 | 1.0 | 7897496 | <1.0 | 1.0 | 7897496 |
| Turbidity | NTU | - | 5 | 1 | 0.8 | 0.1 | 7896234 | 7.2 | 0.1 | 7896234 |
| Alkalinity (Total as CaCO3) | mg/L | - | 30:500 | 1 | 38 | 1.0 | 7897442 | 220 | 1.0 | 7897442 |
| Dissolved Chloride (Cl-) | mg/L | - | 250 | 1 | 2.9 | 1.0 | 7897487 | 12 | 1.0 | 7897487 |
| Nitrite (N) | mg/L | 1 | - | 1 | <0.010 | 0.010 | 7897511 | <0.010 | 0.010 | 7897511 |
| Nitrate (N) | mg/L | 10 | - | 1 | <0.10 | 0.10 | 7897511 | <0.10 | 0.10 | 7897511 |
| Metals | • | | | | • | | | • | | |
| Dissolved Calcium (Ca) | mg/L | - | - | 1 | 13 | 0.05 | 7904606 | 61 | 0.05 | 7900083 |
| Dissolved Magnesium (Mg) | mg/L | - | - | ı | 2.7 | 0.05 | 7904606 | 16 | 0.05 | 7900083 |
| Dissolved Potassium (K) | mg/L | - | - | ı | 2 | 1 | 7904606 | 5 | 1 | 7900083 |
| Dissolved Sodium (Na) | mg/L | - | 200 | 1 | 1.1 | 0.5 | 7904606 | 3.9 | 0.5 | 7900083 |
| Total Aluminum (Al) | ug/L | - | 100 | 1 | 100 | 49 | 7911141 | 1100 | 4.9 | 7903614 |

No Fill Grey

Black

No Exceedance

Exceeds 1 criteria policy/level Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] - Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives



exp Services Inc

Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - SURFACE WATER (WATER)

| Bureau Veritas ID | | | | | SDE615 | | | SDE616 | | |
|-----------------------|-------|------|--------|----------|--------------|------|----------|--------------|-------|----------|
| Sampling Date | | | | | 2022/03/17 | | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | SW4 | RDL | QC Batch | SW5 | RDL | QC Batch |
| Total Antimony (Sb) | ug/L | 6 | - | 20 | <5.0 | 5.0 | 7911141 | <0.50 | 0.50 | 7903614 |
| Total Arsenic (As) | ug/L | 10 | - | 100 | <10 | 10 | 7911141 | 1.2 | 1.0 | 7903614 |
| Total Barium (Ba) | ug/L | 1000 | - | - | <20 | 20 | 7911141 | 35 | 2.0 | 7903614 |
| Total Beryllium (Be) | ug/L | - | - | 11 | <4.0 | 4.0 | 7911141 | <0.40 | 0.40 | 7903614 |
| Total Boron (B) | ug/L | 5000 | - | 200 | <100 | 100 | 7911141 | 12 | 10 | 7903614 |
| Total Cadmium (Cd) | ug/L | 5 | - | 0.2 | <0.90 (1) | 0.90 | 7911141 | <0.090 | 0.090 | 7903614 |
| Total Calcium (Ca) | ug/L | - | - | - | 8900 | 2000 | 7911141 | 67000 | 200 | 7903614 |
| Total Chromium (Cr) | ug/L | 50 | - | - | <50 | 50 | 7911141 | <5.0 | 5.0 | 7903614 |
| Total Cobalt (Co) | ug/L | - | - | 0.9 | <5.0 (1) | 5.0 | 7911141 | 1.0 | 0.50 | 7903614 |
| Total Copper (Cu) | ug/L | - | 1000 | 5 | <9.0 (1) | 9.0 | 7911141 | 7.7 | 0.90 | 7903614 |
| Total Iron (Fe) | ug/L | - | 300 | 300 | <1000 (1) | 1000 | 7911141 | 6200 | 100 | 7903614 |
| Total Lead (Pb) | ug/L | 10 | - | 5 | <5.0 | 5.0 | 7911141 | 2.4 | 0.50 | 7903614 |
| Total Magnesium (Mg) | ug/L | - | - | - | 1600 | 500 | 7911141 | 18000 | 50 | 7903614 |
| Total Manganese (Mn) | ug/L | - | 50 | - | 410 | 20 | 7911141 | 450 | 2.0 | 7903614 |
| Total Molybdenum (Mo) | ug/L | - | - | 40 | <5.0 | 5.0 | 7911141 | 0.94 | 0.50 | 7903614 |
| Total Nickel (Ni) | ug/L | - | - | 25 | <10 | 10 | 7911141 | 1.8 | 1.0 | 7903614 |
| Total Potassium (K) | ug/L | - | - | - | <2000 | 2000 | 7911141 | 5500 | 200 | 7903614 |
| Total Selenium (Se) | ug/L | 50 | - | 100 | <20 | 20 | 7911141 | <2.0 | 2.0 | 7903614 |
| Total Silicon (Si) | ug/L | - | - | - | <500 | 500 | 7911141 | 3800 | 50 | 7903614 |
| Total Silver (Ag) | ug/L | - | - | 0.1 | <0.90 (1) | 0.90 | 7911141 | <0.090 | 0.090 | 7903614 |
| Total Sodium (Na) | ug/L | - | 200000 | - | 1200 | 1000 | 7911141 | 4300 | 100 | 7903614 |
| Total Strontium (Sr) | ug/L | - | - | - | <10 | 10 | 7911141 | 77 | 1.0 | 7903614 |
| Total Thallium (TI) | ug/L | - | - | 0.3 | <0.50 (1) | 0.50 | 7911141 | <0.050 | 0.050 | 7903614 |
| Total Titanium (Ti) | ug/L | - | - | - | <50 | 50 | 7911141 | 29 | 5.0 | 7903614 |
| Total Tungsten (W) | ug/L | - | - | 30 | <10 | 10 | 7911141 | <1.0 | 1.0 | 7903614 |
| Total Uranium (U) | ug/L | 20 | - | 5 | <1.0 | 1.0 | 7911141 | 0.81 | 0.10 | 7903614 |
| Total Vanadium (V) | ug/L | - | - | 6 | <5.0 | 5.0 | 7911141 | 2.8 | 0.50 | 7903614 |

No Fill Grey

Black

No Exceedance

Exceeds 1 criteria policy/level

Exceeds both criteria/levels

RDL = Reportable Detection Limit QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] -Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives

Ref. to MOEE Water Management document dated Feb.1999

(1) RDL exceeds criteria



exp Services Inc

Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

RCAP - SURFACE WATER (WATER)

| Bureau Veritas ID | | | | | SDE615 | | | SDE616 | | |
|-------------------|-------|-----|------|----------|--------------|-----|----------|--------------|-----|----------|
| Sampling Date | | | | | 2022/03/17 | | | 2022/03/17 | | |
| COC Number | | | | | 870268-01-01 | | | 870268-01-01 | | |
| | UNITS | MAC | A/O | Criteria | SW4 | RDL | QC Batch | SW5 | RDL | QC Batch |
| / | | | | | | | | | | i |
| Total Zinc (Zn) | ug/L | - | 5000 | 30 | <50 (1) | 50 | 7911141 | 80 | 5.0 | 7903614 |

No Fill Grey

No Exceedance

Exceeds 1 criteria policy/level

Black

Exceeds both criteria/levels

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

MAC,A/O: Ontario Drinking Water Standards - Maximum Acceptable Concentration [MAC] & Table 4-Chemical/Physical Objectives [A/O] -Not Health Related, respectively

(Made under the Ontario Safe Drinking Water Act, 2002)

Criteria: Ontario Provincial Water Quality Objectives

Ref. to MOEE Water Management document dated Feb. 1999

(1) RDL exceeds criteria



exp Services Inc

Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

TEST SUMMARY

Bureau Veritas ID: SDE609

Collected:

2022/03/17

Sample ID: MW3 Matrix: Water Shipped:

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7896580 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7900197 | N/A | 2022/03/24 | Anna-Kay Gooden |
| Hardness (calculated as CaCO3) | | 7896344 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7900101 | 2022/03/23 | 2022/03/24 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7896589 | N/A | 2022/03/24 | Automated Statchk |
| Anion and Cation Sum | CALC | 7896590 | N/A | 2022/03/24 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7896591 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7896592 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7896579 | N/A | 2022/03/24 | Automated Statchk |

Bureau Veritas ID: SDE609 Dup

Collected: 2022/03/17 Shipped:

Sample ID: MW3 Matrix: Water

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--------------------------------|-----------------|---------|-----------|---------------|-----------------|
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7900197 | N/A | 2022/03/24 | Anna-Kay Gooden |

Bureau Veritas ID: SDE610 Collected: Shipped:

2022/03/17

Sample ID: MW7A Matrix: Water

Received:

2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7897137 | N/A | 2022/03/24 | Anna-Kay Gooden |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7900101 | 2022/03/23 | 2022/03/24 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7894694 | N/A | 2022/03/24 | Automated Statchk |
| Anion and Cation Sum | CALC | 7894695 | N/A | 2022/03/24 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

TEST SUMMARY

Bureau Veritas ID: SDE610

Sample ID: MW7A

Collected:

2022/03/17

Matrix: Water

Shipped:

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|------------------------------------|-----------------|---------|-----------|---------------|-------------------|
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |

Bureau Veritas ID: SDE611

Sample ID: MW7B

Matrix: Water

Collected: 2022/03/17

Shipped:

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-------------------|
| Alkalinity | AT | 7897455 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |
| Conductivity | AT | 7897464 | N/A | 2022/03/23 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7897137 | N/A | 2022/03/24 | Anna-Kay Gooden |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7900101 | 2022/03/23 | 2022/03/24 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7894694 | N/A | 2022/03/24 | Automated Statchk |
| Anion and Cation Sum | CALC | 7894695 | N/A | 2022/03/24 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| pH | AT | 7897458 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |

Bureau Veritas ID: SDE611 Dup Sample ID: MW7B

Matrix: Water

Collected: 2022/03/17 Shipped: **Received:** 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|------------------|-----------------|---------|------------|---------------|--------------|
| Alkalinity | AT | 7897455 | N/A | 2022/03/23 | Surinder Rai |
| Conductivity | AT | 7897464 | N/A | 2022/03/23 | Surinder Rai |
| рН | AT | 7897458 | 2022/03/22 | 2022/03/23 | Surinder Rai |

Bureau Veritas ID: SDE612 Sample ID: MW9

Collected: Shipped:

2022/03/17

Matrix: Water

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--------------------------------------|-----------------|---------|-----------|---------------|-------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |



exp Services Inc

Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

TEST SUMMARY

Collected: Bureau Veritas ID: SDE612 2022/03/17

Shipped:

Sample ID: MW9 Matrix: Water **Received:** 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-------------------|
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7897137 | N/A | 2022/03/24 | Anna-Kay Gooden |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7900101 | 2022/03/23 | 2022/03/24 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7894694 | N/A | 2022/03/24 | Automated Statchk |
| Anion and Cation Sum | CALC | 7894695 | N/A | 2022/03/24 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |

Bureau Veritas ID: SDE613 Collected: 2022/03/17 Sample ID: SW1

Shipped:

2022/03/17

Received: Matrix: Water **Test Description** Instrumentation Batch **Extracted Date Analyzed** Analyst

| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
|--|-----------|---------|------------|------------|-----------------------|
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7900083 | 2022/03/23 | 2022/03/24 | Suban Kanapathippllai |
| Total Metals Analysis by ICPMS | ICP/MS | 7903614 | N/A | 2022/03/25 | Arefa Dabhad |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7898671 | N/A | 2022/03/23 | Anna-Kay Gooden |
| Total Phosphorus (Colourimetric) | LACH/P | 7899137 | 2022/03/23 | 2022/03/24 | Nimarta Singh |
| Turbidity | AT | 7896234 | N/A | 2022/03/22 | Roya Fathitil |



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

TEST SUMMARY

Bureau Veritas ID: SDE613 Dup

Sample ID: SW1 Matrix: Water **Collected:** 2022/03/17

Shipped:

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--------------------------------|-----------------|---------|-----------|---------------|--------------|
| Total Metals Analysis by ICPMS | ICP/MS | 7903614 | N/A | 2022/03/25 | Arefa Dabhad |

Bureau Veritas ID: SDE614

Sample ID: SW2 Matrix: Water **Collected:** 2022/03/17

Shipped:

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-----------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7900083 | 2022/03/23 | 2022/03/24 | Suban Kanapathippllai |
| Total Metals Analysis by ICPMS | ICP/MS | 7903614 | N/A | 2022/03/25 | Arefa Dabhad |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| pH | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7898671 | N/A | 2022/03/23 | Anna-Kay Gooden |
| Total Phosphorus (Colourimetric) | LACH/P | 7899137 | 2022/03/23 | 2022/03/24 | Nimarta Singh |
| Turbidity | AT | 7896234 | N/A | 2022/03/22 | Roya Fathitil |

Bureau Veritas ID: SDE614 Dup

Sample ID: SW2

Matrix: Water

Collected: 2022/03/17 Shipped:

2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|-------------------------------------|-----------------|---------|------------|---------------|-----------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Lab Filtered Metals Analysis by ICP | ICP | 7900083 | 2022/03/23 | 2022/03/24 | Suban Kanapathippllai |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |

Bureau Veritas ID: SDE615 Sample ID: SW4

Matrix: Water

Collected: 2022/03/17

Shipped:

Received:

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--------------------------------------|-----------------|---------|-----------|---------------|-------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |



exp Services Inc

Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

TEST SUMMARY

Bureau Veritas ID: SDE615

Collected: 2022/03/17 Shipped:

Sample ID: SW4 Matrix: Water

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-----------------------|
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7904606 | 2022/03/25 | 2022/03/28 | Suban Kanapathippllai |
| Total Metals Analysis by ICPMS | ICP/MS | 7911141 | N/A | 2022/03/30 | Prempal Bhatti |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7898671 | N/A | 2022/03/23 | Anna-Kay Gooden |
| Total Phosphorus (Colourimetric) | LACH/P | 7899137 | 2022/03/23 | 2022/03/24 | Nimarta Singh |
| Turbidity | AT | 7896234 | N/A | 2022/03/22 | Roya Fathitil |

Bureau Veritas ID: SDE616

Collected: 2022/03/17

Sample ID: SW5

Shipped:

Matrix: Water

Received: 2022/03/17

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-----------------------|
| Alkalinity | AT | 7897442 | N/A | 2022/03/23 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7894693 | N/A | 2022/03/24 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7897487 | N/A | 2022/03/23 | Alina Dobreanu |
| Conductivity | AT | 7897446 | N/A | 2022/03/23 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7894046 | N/A | 2022/03/24 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7900083 | 2022/03/23 | 2022/03/24 | Suban Kanapathippllai |
| Total Metals Analysis by ICPMS | ICP/MS | 7903614 | N/A | 2022/03/25 | Arefa Dabhad |
| Total Ammonia-N | LACH/NH4 | 7899195 | N/A | 2022/03/23 | Raiq Kashif |
| Nitrate & Nitrite as Nitrogen in Water | LACH | 7897511 | N/A | 2022/03/23 | Chandra Nandlal |
| рН | AT | 7897448 | 2022/03/22 | 2022/03/23 | Surinder Rai |
| Orthophosphate | KONE | 7897503 | N/A | 2022/03/23 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7894699 | N/A | 2022/03/24 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7894700 | N/A | 2022/03/24 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7897496 | N/A | 2022/03/24 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7894701 | N/A | 2022/03/24 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7898671 | N/A | 2022/03/23 | Anna-Kay Gooden |
| Total Phosphorus (Colourimetric) | LACH/P | 7899137 | 2022/03/23 | 2022/03/24 | Nimarta Singh |
| Turbidity | AT | 7896234 | N/A | 2022/03/22 | Roya Fathitil |



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

GENERAL COMMENTS

Each temperature is the average of up to three cooler temperatures taken at receipt

| Package 1 | 6.3°C |
|-----------|-------|
|-----------|-------|

Sample SDE615 [SW4]: Metals Analysis: Due to limited amount of sample available for analysis, a smaller than usual portion of the sample was used. Detection limits were adjusted accordingly.

Results relate only to the items tested.



QUALITY ASSURANCE REPORT

exp Services Inc

Client Project #: KCH-21008183
Site Location: HUNTER FARMS

| | | | Matrix | Spike | SPIKED | BLANK | Method | Blank | RP | D | QC Sta | ındard |
|----------|-----------------------------|------------|------------|-----------|------------|-----------|--------|-------------|-----------|-----------|------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7896234 | Turbidity | 2022/03/22 | | | 112 | 85 - 115 | <0.1 | NTU | 0.68 | 20 | | |
| 7897137 | Dissolved Organic Carbon | 2022/03/24 | 96 | 80 - 120 | 97 | 80 - 120 | <0.40 | mg/L | 0.39 | 20 | | |
| 7897442 | Alkalinity (Total as CaCO3) | 2022/03/23 | | | 93 | 85 - 115 | <1.0 | mg/L | 0.98 | 20 | | |
| 7897446 | Conductivity | 2022/03/23 | | | 100 | 85 - 115 | <1.0 | umho/c m | 0.85 | 25 | | |
| 7897448 | рН | 2022/03/23 | | | 102 | 98 - 103 | | | 0.96 | N/A | | |
| 7897455 | Alkalinity (Total as CaCO3) | 2022/03/23 | | | 94 | 85 - 115 | <1.0 | mg/L | 0.72 | 20 | | |
| 7897458 | рН | 2022/03/23 | | | 102 | 98 - 103 | | | 0.26 | N/A | | |
| 7897464 | Conductivity | 2022/03/23 | | | 100 | 85 - 115 | <1.0 | umho/c m | 0.36 | 25 | | |
| 7897487 | Dissolved Chloride (Cl-) | 2022/03/23 | 101 | 80 - 120 | 103 | 80 - 120 | <1.0 | mg/L | 4.7 | 20 | | |
| 7897496 | Dissolved Sulphate (SO4) | 2022/03/24 | 125 | 75 - 125 | 103 | 80 - 120 | <1.0 | mg/L | 1.9 | 20 | | |
| 7897503 | Orthophosphate (P) | 2022/03/23 | 107 | 75 - 125 | 102 | 80 - 120 | <0.010 | mg/L | NC | 25 | | |
| 7897511 | Nitrate (N) | 2022/03/23 | 105 | 80 - 120 | 102 | 80 - 120 | <0.10 | mg/L | NC | 20 | | |
| 7897511 | Nitrite (N) | 2022/03/23 | 88 | 80 - 120 | 102 | 80 - 120 | <0.010 | mg/L | NC | 20 | | |
| 7898671 | Total Organic Carbon (TOC) | 2022/03/23 | 94 | 80 - 120 | 98 | 80 - 120 | <0.40 | mg/L | 2.7 | 20 | | |
| 7899137 | Total Phosphorus | 2022/03/24 | NC | 80 - 120 | 107 | 80 - 120 | <0.004 | mg/L | 4.3 | 20 | 115 | 80 - 120 |
| 7899195 | Total Ammonia-N | 2022/03/23 | 98 | 75 - 125 | 100 | 80 - 120 | <0.050 | mg/L | 0.13 | 20 | | |
| 7900083 | Dissolved Calcium (Ca) | 2022/03/24 | 93 | 80 - 120 | 101 | 80 - 120 | <0.05 | mg/L | 0.012 | 25 | | |
| 7900083 | Dissolved Magnesium (Mg) | 2022/03/24 | 96 | 80 - 120 | 98 | 80 - 120 | <0.05 | mg/L | 0.43 | 25 | | |
| 7900083 | Dissolved Potassium (K) | 2022/03/24 | 99 | 80 - 120 | 100 | 80 - 120 | <1 | mg/L | 1.1 | 25 | | |
| 7900083 | Dissolved Sodium (Na) | 2022/03/24 | 92 | 80 - 120 | 99 | 80 - 120 | <0.5 | mg/L | 3.7 | 25 | | |
| 7900101 | Dissolved Aluminum (AI) | 2022/03/24 | 101 | 80 - 120 | 103 | 80 - 120 | <4.9 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Antimony (Sb) | 2022/03/24 | 104 | 80 - 120 | 103 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Arsenic (As) | 2022/03/24 | 102 | 80 - 120 | 102 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Barium (Ba) | 2022/03/24 | 104 | 80 - 120 | 104 | 80 - 120 | <2.0 | ug/L | 0.56 | 20 | | |
| 7900101 | Dissolved Beryllium (Be) | 2022/03/24 | 104 | 80 - 120 | 103 | 80 - 120 | <0.40 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Boron (B) | 2022/03/24 | 96 | 80 - 120 | 97 | 80 - 120 | <10 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Cadmium (Cd) | 2022/03/24 | 102 | 80 - 120 | 102 | 80 - 120 | <0.090 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Calcium (Ca) | 2022/03/24 | 91 | 80 - 120 | 105 | 80 - 120 | <200 | ug/L | 1.6 | 20 | | |
| 7900101 | Dissolved Chromium (Cr) | 2022/03/24 | 99 | 80 - 120 | 98 | 80 - 120 | <5.0 | ug/L | NC | 20 | | |



QUALITY ASSURANCE REPORT(CONT'D)

exp Services Inc

Client Project #: KCH-21008183
Site Location: HUNTER FARMS

| | | | Matrix | Spike | SPIKED | BLANK | Method I | Blank | RP | D | QC Sta | ndard |
|----------|---------------------------|------------|------------|-----------|------------|-----------|----------|-------|-----------|-----------|------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7900101 | Dissolved Cobalt (Co) | 2022/03/24 | 97 | 80 - 120 | 97 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Copper (Cu) | 2022/03/24 | 98 | 80 - 120 | 99 | 80 - 120 | <0.90 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Iron (Fe) | 2022/03/24 | 100 | 80 - 120 | 100 | 80 - 120 | <100 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Lead (Pb) | 2022/03/24 | 94 | 80 - 120 | 96 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Magnesium (Mg) | 2022/03/24 | 100 | 80 - 120 | 101 | 80 - 120 | <50 | ug/L | 0.17 | 20 | | |
| 7900101 | Dissolved Manganese (Mn) | 2022/03/24 | 103 | 80 - 120 | 102 | 80 - 120 | <2.0 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Molybdenum (Mo) | 2022/03/24 | 104 | 80 - 120 | 102 | 80 - 120 | <0.50 | ug/L | 5.2 | 20 | | |
| 7900101 | Dissolved Nickel (Ni) | 2022/03/24 | 97 | 80 - 120 | 98 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Phosphorus (P) | 2022/03/24 | 108 | 80 - 120 | 113 | 80 - 120 | <100 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Potassium (K) | 2022/03/24 | 101 | 80 - 120 | 99 | 80 - 120 | <200 | ug/L | 1.3 | 20 | | |
| 7900101 | Dissolved Selenium (Se) | 2022/03/24 | 100 | 80 - 120 | 100 | 80 - 120 | <2.0 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Silicon (Si) | 2022/03/24 | 101 | 80 - 120 | 103 | 80 - 120 | <50 | ug/L | 1.2 | 20 | | |
| 7900101 | Dissolved Silver (Ag) | 2022/03/24 | 96 | 80 - 120 | 97 | 80 - 120 | <0.090 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Sodium (Na) | 2022/03/24 | 97 | 80 - 120 | 99 | 80 - 120 | <100 | ug/L | 0.90 | 20 | | |
| 7900101 | Dissolved Strontium (Sr) | 2022/03/24 | 101 | 80 - 120 | 101 | 80 - 120 | <1.0 | ug/L | 1.6 | 20 | | |
| 7900101 | Dissolved Thallium (TI) | 2022/03/24 | 103 | 80 - 120 | 102 | 80 - 120 | <0.050 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Titanium (Ti) | 2022/03/24 | 102 | 80 - 120 | 102 | 80 - 120 | <5.0 | ug/L | NC | 20 | | |
| 7900101 | Dissolved Uranium (U) | 2022/03/24 | 104 | 80 - 120 | 103 | 80 - 120 | <0.10 | ug/L | 1.3 | 20 | | |
| 7900101 | Dissolved Vanadium (V) | 2022/03/24 | 102 | 80 - 120 | 100 | 80 - 120 | <0.50 | ug/L | 4.2 | 20 | | |
| 7900101 | Dissolved Zinc (Zn) | 2022/03/24 | 100 | 80 - 120 | 99 | 80 - 120 | <5.0 | ug/L | NC | 20 | | |
| 7900197 | Dissolved Organic Carbon | 2022/03/24 | 97 | 80 - 120 | 99 | 80 - 120 | <0.40 | mg/L | 0.15 | 20 | | |
| 7903614 | Total Aluminum (AI) | 2022/03/25 | 114 | 80 - 120 | 105 | 80 - 120 | <4.9 | ug/L | 3.9 | 20 | | |
| 7903614 | Total Antimony (Sb) | 2022/03/25 | 105 | 80 - 120 | 104 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7903614 | Total Arsenic (As) | 2022/03/25 | 103 | 80 - 120 | 107 | 80 - 120 | <1.0 | ug/L | 0.44 | 20 | | |
| 7903614 | Total Barium (Ba) | 2022/03/25 | 99 | 80 - 120 | 103 | 80 - 120 | <2.0 | ug/L | 1.6 | 20 | | |
| 7903614 | Total Beryllium (Be) | 2022/03/25 | 104 | 80 - 120 | 104 | 80 - 120 | <0.40 | ug/L | NC | 20 | | |
| 7903614 | Total Boron (B) | 2022/03/25 | 93 | 80 - 120 | 95 | 80 - 120 | <10 | ug/L | 1.1 | 20 | | |
| 7903614 | Total Cadmium (Cd) | 2022/03/25 | 100 | 80 - 120 | 102 | 80 - 120 | <0.090 | ug/L | NC | 20 | | |
| 7903614 | Total Calcium (Ca) | 2022/03/25 | -4.6 (1) | 80 - 120 | 105 | 80 - 120 | <200 | ug/L | 2.2 | 20 | | |
| 7903614 | Total Chromium (Cr) | 2022/03/25 | 98 | 80 - 120 | 101 | 80 - 120 | <5.0 | ug/L | NC | 20 | | |
| 7903614 | Total Cobalt (Co) | 2022/03/25 | 102 | 80 - 120 | 105 | 80 - 120 | <0.50 | ug/L | 0.49 | 20 | | |



QUALITY ASSURANCE REPORT(CONT'D)

exp Services Inc

Client Project #: KCH-21008183
Site Location: HUNTER FARMS

| | | | Matrix | Spike | SPIKED | BLANK | Method I | Blank | RP | D | QC Sta | ndard |
|----------|--------------------------|------------|------------|-----------|------------|-----------|----------|-------|-----------|-----------|------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7903614 | Total Copper (Cu) | 2022/03/25 | 104 | 80 - 120 | 105 | 80 - 120 | <0.90 | ug/L | 1.5 | 20 | | |
| 7903614 | Total Iron (Fe) | 2022/03/25 | 89 | 80 - 120 | 105 | 80 - 120 | <100 | ug/L | 0.72 | 20 | | |
| 7903614 | Total Lead (Pb) | 2022/03/25 | 98 | 80 - 120 | 98 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7903614 | Total Magnesium (Mg) | 2022/03/25 | 93 | 80 - 120 | 107 | 80 - 120 | <50 | ug/L | 1.2 | 20 | | |
| 7903614 | Total Manganese (Mn) | 2022/03/25 | 46 (1) | 80 - 120 | 102 | 80 - 120 | <2.0 | ug/L | 0.72 | 20 | | |
| 7903614 | Total Molybdenum (Mo) | 2022/03/25 | 102 | 80 - 120 | 102 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7903614 | Total Nickel (Ni) | 2022/03/25 | 99 | 80 - 120 | 103 | 80 - 120 | <1.0 | ug/L | 9.2 | 20 | | |
| 7903614 | Total Potassium (K) | 2022/03/25 | 107 | 80 - 120 | 107 | 80 - 120 | <200 | ug/L | 0.31 | 20 | | |
| 7903614 | Total Selenium (Se) | 2022/03/25 | 108 | 80 - 120 | 110 | 80 - 120 | <2.0 | ug/L | NC | 20 | | |
| 7903614 | Total Silicon (Si) | 2022/03/25 | 95 | 80 - 120 | 99 | 80 - 120 | <50 | ug/L | 1.6 | 20 | | |
| 7903614 | Total Silver (Ag) | 2022/03/25 | 97 | 80 - 120 | 100 | 80 - 120 | <0.090 | ug/L | NC | 20 | | |
| 7903614 | Total Sodium (Na) | 2022/03/25 | 58 (1) | 80 - 120 | 109 | 80 - 120 | <100 | ug/L | 2.1 | 20 | | |
| 7903614 | Total Strontium (Sr) | 2022/03/25 | 90 | 80 - 120 | 98 | 80 - 120 | <1.0 | ug/L | 0.38 | 20 | | |
| 7903614 | Total Thallium (TI) | 2022/03/25 | 103 | 80 - 120 | 101 | 80 - 120 | <0.050 | ug/L | NC | 20 | | |
| 7903614 | Total Titanium (Ti) | 2022/03/25 | 99 | 80 - 120 | 100 | 80 - 120 | <5.0 | ug/L | 3.8 | 20 | | |
| 7903614 | Total Tungsten (W) | 2022/03/25 | 105 | 80 - 120 | 108 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7903614 | Total Uranium (U) | 2022/03/25 | 102 | 80 - 120 | 103 | 80 - 120 | <0.10 | ug/L | NC | 20 | | |
| 7903614 | Total Vanadium (V) | 2022/03/25 | 101 | 80 - 120 | 102 | 80 - 120 | <0.50 | ug/L | 0.29 | 20 | | |
| 7903614 | Total Zinc (Zn) | 2022/03/25 | 99 | 80 - 120 | 106 | 80 - 120 | <5.0 | ug/L | 0.23 | 20 | | |
| 7903614 | Total Zirconium (Zr) | 2022/03/25 | 105 | 80 - 120 | 104 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7904606 | Dissolved Calcium (Ca) | 2022/03/28 | 98 | 80 - 120 | 97 | 80 - 120 | <0.05 | mg/L | 3.5 | 25 | | |
| 7904606 | Dissolved Magnesium (Mg) | 2022/03/28 | 100 | 80 - 120 | 96 | 80 - 120 | <0.05 | mg/L | 3.2 | 25 | | |
| 7904606 | Dissolved Potassium (K) | 2022/03/28 | 105 | 80 - 120 | 98 | 80 - 120 | <1 | mg/L | 3.8 | 25 | | |
| 7904606 | Dissolved Sodium (Na) | 2022/03/28 | 113 | 80 - 120 | 97 | 80 - 120 | <0.5 | mg/L | 2.3 | 25 | | |
| 7911141 | Total Aluminum (AI) | 2022/03/30 | 99 | 80 - 120 | 99 | 80 - 120 | <4.9 | ug/L | 3.4 | 20 | | |
| 7911141 | Total Antimony (Sb) | 2022/03/30 | 107 | 80 - 120 | 105 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7911141 | Total Arsenic (As) | 2022/03/30 | 103 | 80 - 120 | 99 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7911141 | Total Barium (Ba) | 2022/03/30 | 100 | 80 - 120 | 97 | 80 - 120 | <2.0 | ug/L | NC | 20 | | |
| 7911141 | Total Beryllium (Be) | 2022/03/30 | 103 | 80 - 120 | 98 | 80 - 120 | <0.40 | ug/L | NC | 20 | | |
| 7911141 | Total Boron (B) | 2022/03/30 | 99 | 80 - 120 | 95 | 80 - 120 | <10 | ug/L | NC | 20 | | |
| 7911141 | Total Cadmium (Cd) | 2022/03/30 | 103 | 80 - 120 | 100 | 80 - 120 | <0.090 | ug/L | NC | 20 | | |



QUALITY ASSURANCE REPORT(CONT'D)

exp Services Inc

Client Project #: KCH-21008183
Site Location: HUNTER FARMS

| | | | Matrix | Spike | SPIKED | BLANK | Method I | Blank | RP | D | QC Sta | ndard |
|----------|-----------------------|------------|------------|-----------|------------|-----------|----------|-------|-----------|-----------|------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7911141 | Total Calcium (Ca) | 2022/03/30 | 99 | 80 - 120 | 97 | 80 - 120 | <200 | ug/L | NC | 20 | | |
| 7911141 | Total Chromium (Cr) | 2022/03/30 | 95 | 80 - 120 | 92 | 80 - 120 | <5.0 | ug/L | NC | 20 | | |
| 7911141 | Total Cobalt (Co) | 2022/03/30 | 96 | 80 - 120 | 93 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7911141 | Total Copper (Cu) | 2022/03/30 | 98 | 80 - 120 | 94 | 80 - 120 | <0.90 | ug/L | 1.1 | 20 | | |
| 7911141 | Total Iron (Fe) | 2022/03/30 | 99 | 80 - 120 | 97 | 80 - 120 | <100 | ug/L | NC | 20 | | |
| 7911141 | Total Lead (Pb) | 2022/03/30 | 97 | 80 - 120 | 93 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7911141 | Total Magnesium (Mg) | 2022/03/30 | 97 | 80 - 120 | 95 | 80 - 120 | <50 | ug/L | NC | 20 | | |
| 7911141 | Total Manganese (Mn) | 2022/03/30 | 99 | 80 - 120 | 95 | 80 - 120 | <2.0 | ug/L | 3.7 | 20 | | |
| 7911141 | Total Molybdenum (Mo) | 2022/03/30 | 99 | 80 - 120 | 96 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7911141 | Total Nickel (Ni) | 2022/03/30 | 98 | 80 - 120 | 95 | 80 - 120 | <1.0 | ug/L | 0.11 | 20 | | |
| 7911141 | Total Potassium (K) | 2022/03/30 | 98 | 80 - 120 | 95 | 80 - 120 | <200 | ug/L | NC | 20 | | |
| 7911141 | Total Selenium (Se) | 2022/03/30 | 104 | 80 - 120 | 103 | 80 - 120 | <2.0 | ug/L | NC | 20 | | |
| 7911141 | Total Silicon (Si) | 2022/03/30 | 98 | 80 - 120 | 98 | 80 - 120 | <50 | ug/L | NC | 20 | | |
| 7911141 | Total Silver (Ag) | 2022/03/30 | 99 | 80 - 120 | 95 | 80 - 120 | <0.090 | ug/L | NC | 20 | | |
| 7911141 | Total Sodium (Na) | 2022/03/30 | 95 | 80 - 120 | 96 | 80 - 120 | <100 | ug/L | 4.9 | 20 | | |
| 7911141 | Total Strontium (Sr) | 2022/03/30 | 98 | 80 - 120 | 95 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7911141 | Total Thallium (TI) | 2022/03/30 | 99 | 80 - 120 | 99 | 80 - 120 | <0.050 | ug/L | NC | 20 | | |
| 7911141 | Total Titanium (Ti) | 2022/03/30 | 97 | 80 - 120 | 97 | 80 - 120 | <5.0 | ug/L | 0.036 | 20 | | |
| 7911141 | Total Tungsten (W) | 2022/03/30 | 95 | 80 - 120 | 92 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |
| 7911141 | Total Uranium (U) | 2022/03/30 | 100 | 80 - 120 | 100 | 80 - 120 | <0.10 | ug/L | NC | 20 | | |
| 7911141 | Total Vanadium (V) | 2022/03/30 | 98 | 80 - 120 | 95 | 80 - 120 | <0.50 | ug/L | NC | 20 | | |
| 7911141 | Total Zinc (Zn) | 2022/03/30 | 101 | 80 - 120 | 97 | 80 - 120 | <5.0 | ug/L | NC | 20 | | |



Bureau Veritas Job #: C272761 Report Date: 2022/03/30

QUALITY ASSURANCE REPORT(CONT'D)

exp Services Inc

Client Project #: KCH-21008183

Site Location: HUNTER FARMS

Sampler Initials: MB

| | | | Matrix | Spike | SPIKED | BLANK | Method E | Blank | RPI |) | QC Sta | ndard |
|----------|----------------------|------------|------------|-----------|------------|-----------|----------|-------|-----------|-----------|------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7911141 | Total Zirconium (Zr) | 2022/03/30 | 88 | 80 - 120 | 98 | 80 - 120 | <1.0 | ug/L | NC | 20 | | |

N/A = Not Applicable

Duplicate: Paired analysis of a separate portion of the same sample. Used to evaluate the variance in the measurement.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.

QC Standard: A sample of known concentration prepared by an external agency under stringent conditions. Used as an independent check of method accuracy.

Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.

Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.

NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)

NC (Duplicate RPD): The duplicate RPD was not calculated. The concentration in the sample and/or duplicate was too low to permit a reliable RPD calculation (absolute difference <= 2x RDL).

(1) Recovery or RPD for this parameter is outside control limits. The overall quality control for this analysis meets acceptability criteria.



Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by:

Anastassia Hamanov, Scientific Specialist

Bureau Veritas has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.

| BUREAU VERITAS | | Bureau Veritas 6740 Campobello Road, Mis | ssissauga, Ontario | Canada L5N 2l | L8 Tel:(905) 817- | | | (905) 817-5 | 777 www. | bvna.com | F | REC' | | LONDO | | 11111111 | stine (| Mar-22 15:15 Gripton | Page of |
|-------------------|---|--|----------------------------------|-----------------------|-------------------------------|--------------------------------------|--|-------------|---------------|-----------------|---------------------|--------|-----------|-------------------------------|-------------------------|--------------|----------------------|---|--------------------------------|
| | | VOICE TO: | | 10 | | REPO | RT TO: | | | | | | 5 1000 | INFORMATION: | | , | | 0 | |
| mpany Name | #28124 exp Ser Accounts Payabl | | | Company | Malli I | Oobbin | | | | | Quotation# | | B9171 | 8 | | MTA | M ENV-1605 | | Bottle Order #: |
| dress: | 15701 Robin's H | | | Attention Address: | 110,111 | | | | | | P.O. #: Project: | | KCH-2 | 1006317 ZIC | 06183 | | | | 870268 |
| | London ON N5V | | | | | | | | | | Project Nam | 0: | My | inter For | ns | | | COC #: | Project Manager: |
| d: | (519) 963-3000 | |) 963-1152 | Tel: | lealli e | lobbin@exp.com | Fax: | | | | Site #: | | 4.17 | 110 | | | | | Christine Gripton |
| naif: | | aren.Burke@exp.com | WIENDED FOR | Email: | NAME OF TAXABLE PARTY. | | | | | | Sampled By | _ | PI FASE B | E SPECIFIC) | | + | 11111 | C#870268-01-01 Turnaround Time (TAT) F | amufendi. |
| MOE REC | SUBMITTED ON T | G WATER OR WATER I HE BUREAU VERITAS | DRINKING WAT | TER CHAIN | OF CUSTOD | Y MUST BE | | - F | | | | | LENGE | L or Low loy | | | 3.58 | Please provide advance notice f | |
| Regulati | ion 153 (2011) | Ott | ner Regulations | | Special | Instructions | ircle) | illere | | | | | | | | 14.00 | | andard) TAT: if Rush TAT is not specified): | R |
| | Res/Park Mediur | | Sanitary Sewer Byl | | | | Field Filtered (please circle): Metals / Hg / Cr VI | Lab F | | PMS | | | | | | | | 5-7 Working days for most tests. | 1 |
| Table 2 | Ind/Comm Coarse | | Storm Sewer Bylaw inicipality | | | | gald) | sive | ater | Metals by ICPMS | | | | | | Plea days | se note: St | andard TAT for certain tests such as a your Project Manager for details. | BOD and Dioxins/Furans are > 5 |
| Table 3 | Jaginonas [] For K | The state of the s | Reg 406 Table | | | | ered Is / F | rehen | 8 | etals | | | | | | 4.5 | | Rush TAT (if applies to entire sub | nission) |
| | | Other OO | NAS | | | | J Filt | Comp | Surface Water | N peu | | | | | | 100 | Required: | | ne Required: |
| | | a on Certificate of Analy | | - | | | Field | RCAp - | CAP | ab File | | | | | | | Bottles | | call lab for #) |
| Sampl | le Barcode Label | Sample (Location) Iden | | late Sampled | Time Sample | d Matrix | | S. | RC | 3 | | - | - | | - | * 01 | Bottes | Comm | ents |
| | | WM3 | | Nor 17 | AM | GW | | X | | | | | | | | | | odinas | |
| | | ATWAY | | 1 | PM | 1 | | X | | | | | | | | | | 1 | |
| | | TUM | 3 | | PM | | | × | | | | | | | | | | | |
| | | PUMM | | | pur | V | | X | | | | | | | | | | V | |
| | | Swil | | | AM | Sw | | | X | | | | | | | | | Phad | |
| | | | | | A.A | | | | V | | | | | | | | | 1 Wills | |
| | | SW2 | | | AW | | | | X | | | | | | | | | | |
| | | SWY | | | PM | | | | X | | | | | | | | | | |
| | | SWS | | V | Par | | | | X | | | | | | | | | V | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | 00 | Zce |
| | RELINQUISHED BY: (S | Signature/Print) | Date: (YY/MM | | Time | RECEIVED | BY: (Signature | | | Date: (YY/N | MM/DD) | Tir | | # jars used and not submitted | | | Laborato | ory Use Only | |
| 114 | 116/1 | derello B | 92/03/17 | | | | 相似 | | 40.81 | 20226 | 4 | 15 | | | Time Sensit | ve T | | e (°C) on Recei Custody S | eal Yes No |
| NI ESS OTUES | DWISE ACREED TO IN | RITING, WORK SUBMITTED C | IN THIS CUAIN CT | CHETODY IS S | UP IECT TO BUD | Q4 R | | AND COND | | | 3 18 | FCUSTO | | ENTIS | | | 3, |) I much | |
| IS THE RESP | ENT AND ACCEPTANCE ONSIBILITY OF THE REI | OF OUR TERMS WHICH ARE LINQUISHER TO ENSURE THE | AVAILABLE FOR V | EWING AT W | W.BVNA.COM/TE USTODY RECOR | ERMS-AND-CONDITI D. AN INCOMPLETE | ONS. CHAIN OF CUS | TODY MAY | RESULT | | | | | | MUST BE KEP UNTIL DE | T COOL (| < 10°C)FF DBUREAU | ROM TIME OF SAMPLING VERITAS | Bureau Veritas Yellow: Cli |
| MPLE CONT | AINER, PRESERVATION | , HOLD TIME AND PACKAGE | INFORMATION CA | N BE VIEWED | AT WWW.BVNA.C | OM/RESOURCES/CI | AAIN-OF-CUST | DDY-FORMS | | | | | | | | -1.1 | A1.00 | | |

Page 25 of 26

Client Project #: KCH-21008183 Site Location: HUNTER FARMS

Sampler Initials: MB

Exceedance Summary Table – ODWS (2002)

Result Exceedances

| Sample ID | Bureau Veritas ID | Parameter | Criteria | Result | DL | UNITS |
|-----------|-------------------|-----------------------|----------|--------|------|-------|
| MW7A | SDE610-02 | Dissolved Uranium (U) | 20 | 35 | 0.10 | ug/L |

The exceedance summary table is for information purposes only and should not be considered a comprehensive listing or statement of conformance to applicable regulatory guidelines.

Exceedance Summary Table – Prov. Water Quality Obj. Result Exceedances

| Sample ID | Bureau Veritas ID | Parameter | Criteria | Result | DL | UNITS |
|-----------|-------------------|---------------------------|----------|--------|-------|-------|
| MW7A | SDE610-02 | Dissolved Molybdenum (Mo) | 40 | 45 | 0.50 | ug/L |
| MW7A | SDE610-02 | Dissolved Uranium (U) | 5 | 35 | 0.10 | ug/L |
| MW7A | SDE610-02 | Dissolved Zinc (Zn) | 30 | 38 | 5.0 | ug/L |
| MW7B | SDE611-02 | Dissolved Zinc (Zn) | 30 | 36 | 5.0 | ug/L |
| SW1 | SDE613-03-Lab Dup | Total Cobalt (Co) | 0.9 | 2.4 | 0.50 | ug/L |
| SW1 | SDE613-03 | Total Cobalt (Co) | 0.9 | 2.4 | 0.50 | ug/L |
| SW1 | SDE613-03 | Total Iron (Fe) | 300 | 39000 | 100 | ug/L |
| SW1 | SDE613-03-Lab Dup | Total Iron (Fe) | 300 | 39000 | 100 | ug/L |
| SW1 | SDE613-04 | Total Phosphorus | 0.01 | 0.41 | 0.02 | mg/L |
| SW1 | SDE613-03-Lab Dup | Total Zinc (Zn) | 30 | 43 | 5.0 | ug/L |
| SW1 | SDE613-03 | Total Zinc (Zn) | 30 | 43 | 5.0 | ug/L |
| SW2 | SDE614-04 | Total Phosphorus | 0.01 | 0.026 | 0.004 | mg/L |
| SW4 | SDE615-04 | Total Phosphorus | 0.01 | 0.09 | 0.02 | mg/L |
| SW5 | SDE616-03 | Total Cobalt (Co) | 0.9 | 1.0 | 0.50 | ug/L |
| SW5 | SDE616-03 | Total Copper (Cu) | 5 | 7.7 | 0.90 | ug/L |
| SW5 | SDE616-03 | Total Iron (Fe) | 300 | 6200 | 100 | ug/L |
| SW5 | SDE616-04 | Total Phosphorus | 0.01 | 1.5 | 0.02 | mg/L |
| SW5 | SDE616-03 | Total Zinc (Zn) | 30 | 80 | 5.0 | ug/L |

Detection Limit Exceedances

| Sample ID | Bureau Veritas ID | Parameter | Criteria | Result | DL | UNITS |
|-----------|-------------------|----------------------|----------|--------|------|-------|
| SW4 | SDE615-03 | Total Cadmium (Cd) | 0.2 | <0.90 | 0.90 | ug/L |
| SW4 | SDE615-03 | Total Cobalt (Co) | 0.9 | <5.0 | 5.0 | ug/L |
| SW4 | SDE615-03 | Total Copper (Cu) | 5 | <9.0 | 9.0 | ug/L |
| SW4 | SDE615-03 | Total Iron (Fe) | 300 | <1000 | 1000 | ug/L |
| SW4 | SDE615-03 | Total Silver (Ag) | 0.1 | <0.90 | 0.90 | ug/L |
| SW4 | SDE615-03 | Total Thallium (TI) | 0.3 | <0.50 | 0.50 | ug/L |
| SW4 | SDE615-03 | Total Zinc (Zn) | 30 | <50 | 50 | ug/L |
| SW4 | SDE615-03 | Total Zirconium (Zr) | 4 | <10 | 10 | ug/L |

The exceedance summary table is for information purposes only and should not be considered a comprehensive listing or statement of conformance to applicable regulatory guidelines.



Your Project #: LON-21008138 Site Location: HUNTER FARM Your C.O.C. #: 839959-01-01

Attention: Heather Jaggard

exp Services Inc London Branch 15701 Robin's Hill Rd Unit 2 London, ON CANADA N5V 0A5

> Report Date: 2021/10/08 Report #: R6845736

Version: 1 - Final

CERTIFICATE OF ANALYSIS

BV LABS JOB #: C1S2764 Received: 2021/09/29, 08:30

Sample Matrix: Water # Samples Received: 8

| | | Date | Date | | |
|--|----------|------------|------------|--------------------------|----------------------|
| Analyses | Quantity | Extracted | Analyzed | Laboratory Method | Analytical Method |
| Alkalinity | 3 | N/A | 2021/10/01 | CAM SOP-00448 | SM 23 2320 B m |
| Alkalinity | 5 | N/A | 2021/10/04 | CAM SOP-00448 | SM 23 2320 B m |
| Carbonate, Bicarbonate and Hydroxide | 1 | N/A | 2021/10/01 | CAM SOP-00102 | APHA 4500-CO2 D |
| Carbonate, Bicarbonate and Hydroxide | 2 | N/A | 2021/10/04 | CAM SOP-00102 | APHA 4500-CO2 D |
| Carbonate, Bicarbonate and Hydroxide | 5 | N/A | 2021/10/05 | CAM SOP-00102 | APHA 4500-CO2 D |
| Chloride by Automated Colourimetry | 4 | N/A | 2021/10/01 | CAM SOP-00463 | SM 23 4500-Cl E m |
| Chloride by Automated Colourimetry | 4 | N/A | 2021/10/04 | CAM SOP-00463 | SM 23 4500-Cl E m |
| Conductivity | 3 | N/A | 2021/10/01 | CAM SOP-00414 | SM 23 2510 m |
| Conductivity | 5 | N/A | 2021/10/04 | CAM SOP-00414 | SM 23 2510 m |
| Dissolved Organic Carbon (DOC) (1) | 1 | N/A | 2021/10/04 | CAM SOP-00446 | SM 23 5310 B m |
| Dissolved Organic Carbon (DOC) (1) | 3 | N/A | 2021/10/05 | CAM SOP-00446 | SM 23 5310 B m |
| Hardness (calculated as CaCO3) | 4 | N/A | 2021/10/04 | CAM SOP | SM 2340 B |
| | | | | 00102/00408/00447 | |
| Hardness (calculated as CaCO3) | 4 | N/A | 2021/10/05 | | SM 2340 B |
| | | | | 00102/00408/00447 | |
| Lab Filtered Metals Analysis by ICP | 4 | | | CAM SOP-00408 | EPA 6010D m |
| Lab Filtered Metals by ICPMS | 8 | | | CAM SOP-00447 | EPA 6020B m |
| Total Metals Analysis by ICPMS | 3 | N/A | 2021/10/05 | CAM SOP-00447 | EPA 6020B m |
| Total Metals Analysis by ICPMS | 1 | N/A | 2021/10/08 | CAM SOP-00447 | EPA 6020B m |
| Ion Balance (% Difference) | 4 | N/A | 2021/10/05 | | |
| Anion and Cation Sum | 4 | N/A | 2021/10/05 | | |
| Total Ammonia-N | 1 | N/A | 2021/10/01 | CAM SOP-00441 | USGS I-2522-90 m |
| Total Ammonia-N | 7 | N/A | 2021/10/04 | CAM SOP-00441 | USGS I-2522-90 m |
| Nitrate (NO3) and Nitrite (NO2) in Water (2) | 4 | N/A | 2021/10/01 | CAM SOP-00440 | SM 23 4500-NO3I/NO2B |
| Nitrate (NO3) and Nitrite (NO2) in Water (2) | 4 | N/A | 2021/10/04 | CAM SOP-00440 | SM 23 4500-NO3I/NO2B |
| рН | 5 | 2021/10/01 | 2021/10/04 | CAM SOP-00413 | SM 4500H+ B m |
| рН | 3 | 2021/09/30 | 2021/10/01 | CAM SOP-00413 | SM 4500H+ B m |
| Orthophosphate | 4 | N/A | 2021/10/01 | CAM SOP-00461 | EPA 365.1 m |
| Orthophosphate | 4 | N/A | 2021/10/04 | CAM SOP-00461 | EPA 365.1 m |
| | | | | | |



Your Project #: LON-21008138 Site Location: HUNTER FARM Your C.O.C. #: 839959-01-01

Attention: Heather Jaggard

exp Services Inc London Branch 15701 Robin's Hill Rd Unit 2 London, ON CANADA N5V 0A5

Report Date: 2021/10/08

Report #: R6845736 Version: 1 - Final

CERTIFICATE OF ANALYSIS

BV LABS JOB #: C1S2764 Received: 2021/09/29, 08:30

Sample Matrix: Water # Samples Received: 8

| | | Date | Date | | |
|-------------------------------------|----------|------------|------------|--------------------------|--------------------|
| Analyses | Quantity | Extracted | Analyzed | Laboratory Method | Analytical Method |
| Sat. pH and Langelier Index (@ 20C) | 8 | N/A | 2021/10/05 | | Auto Calc |
| Sat. pH and Langelier Index (@ 4C) | 8 | N/A | 2021/10/05 | | Auto Calc |
| Sulphate by Automated Colourimetry | 4 | N/A | 2021/10/01 | CAM SOP-00464 | EPA 375.4 m |
| Sulphate by Automated Colourimetry | 4 | N/A | 2021/10/04 | CAM SOP-00464 | EPA 375.4 m |
| Total Dissolved Solids (TDS calc) | 8 | N/A | 2021/10/05 | | Auto Calc |
| Total Organic Carbon (TOC) (3) | 4 | N/A | 2021/10/05 | CAM SOP-00446 | SM 23 5310B m |
| Total Phosphorus (Colourimetric) | 4 | 2021/10/04 | 2021/10/05 | CAM SOP-00407 | SM 23 4500 P B H m |
| Turbidity | 4 | N/A | 2021/10/01 | CAM SOP-00417 | SM 23 2130 B m |

Remarks:

Bureau Veritas is accredited to ISO/IEC 17025 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by Bureau Veritas are based upon recognized Provincial, Federal or US method compendia such as CCME, MELCC, EPA, APHA.

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in Bureau Veritas' profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and Bureau Veritas in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

Bureau Veritas liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. Bureau Veritas has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by Bureau Veritas, unless otherwise agreed in writing. Bureau Veritas is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Results relate to samples tested. When sampling is not conducted by Bureau Veritas, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

Reference Method suffix "m" indicates test methods incorporate validated modifications from specific reference methods to improve performance.

- * RPDs calculated using raw data. The rounding of final results may result in the apparent difference.
- (1) Dissolved Organic Carbon (DOC) present in the sample should be considered as non-purgeable DOC.



Your Project #: LON-21008138 Site Location: HUNTER FARM Your C.O.C. #: 839959-01-01

Attention: Heather Jaggard

exp Services Inc London Branch 15701 Robin's Hill Rd Unit 2 London, ON CANADA N5V 0A5

Report Date: 2021/10/08

Report #: R6845736 Version: 1 - Final

CERTIFICATE OF ANALYSIS

BV LABS JOB #: C1S2764

Received: 2021/09/29, 08:30

- (2) Values for calculated parameters may not appear to add up due to rounding of raw data and significant figures.
- (3) Total Organic Carbon (TOC) present in the sample should be considered as non-purgeable TOC.

Encryption Key



Please direct all questions regarding this Certificate of Analysis to your Project Manager.

Bureau Veritas

Christine Gripton, Senior Project Manager Email: Christine.Gripton@bureauveritas.com

Phone# (519)652-9444

This report has been generated and distributed using a secure automated process.

BV Labs has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.

> Total Cover Pages: 3 Page 3 of 24



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

RCAP - COMPREHENSIVE (LAB FILTERED)

| BV Labs ID | | QUK162 | | QUK163 | QUK164 | QUK165 | | | |
|-------------------------------------|---------|------------|----------|------------|------------|------------|-------|----------|--|
| Samulina Data | | 2021/09/28 | | 2021/09/28 | 2021/09/28 | 2021/09/28 | | | |
| Sampling Date | | 13:00 | | 16:00 | 16:05 | 16:30 | | | |
| | UNITS | BH3/MW | QC Batch | BH7A/MW | BH7B/MW | BH9/MW | RDL | QC Batch | |
| Calculated Parameters | | | | | | | | | |
| Anion Sum | me/L | 7.37 | 7610019 | 4.23 | 9.63 | 3.38 | N/A | 7610019 | |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | 280 | 7610010 | 140 | 400 | 130 | 1.0 | 7610010 | |
| Calculated TDS | mg/L | 390 | 7610017 | 230 | 510 | 180 | 1.0 | 7610017 | |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | 2.6 | 7610010 | 1.1 | 3.4 | 1.4 | 1.0 | 7610010 | |
| Cation Sum | me/L | 7.83 | 7610019 | 4.29 | 10.3 | 3.40 | N/A | 7610019 | |
| Hardness (CaCO3) | mg/L | 330 | 7610016 | 180 | 490 | 140 | 1.0 | 7610016 | |
| Ion Balance (% Difference) | % | 3.05 | 7610018 | 0.630 | 3.31 | 0.310 | N/A | 7610018 | |
| Langelier Index (@ 20C) | N/A | 0.974 | 7610013 | 0.386 | 1.25 | 0.408 | | 7610013 | |
| Langelier Index (@ 4C) | N/A | 0.726 | 7610014 | 0.137 | 1.00 | 0.158 | | 7610014 | |
| Saturation pH (@ 20C) | N/A | 7.02 | 7610013 | 7.52 | 6.70 | 7.63 | | 7610013 | |
| Saturation pH (@ 4C) | N/A | 7.27 | 7610014 | 7.77 | 6.95 | 7.88 | | 7610014 | |
| Inorganics | | | | | | | | | |
| Total Ammonia-N | mg/L | <0.050 | 7616218 | <0.050 | 0.097 | <0.050 | 0.050 | 7616218 | |
| Conductivity | umho/cm | 690 | 7613005 | 410 | 840 | 320 | 1.0 | 7613005 | |
| Dissolved Organic Carbon | mg/L | 3.7 | 7617408 | 4.8 | 10 | 4.1 | 0.40 | 7616559 | |
| Orthophosphate (P) | mg/L | <0.010 | 7613566 | <0.010 | <0.010 | <0.010 | 0.010 | 7613566 | |
| рН | рН | 8.00 | 7613008 | 7.91 | 7.95 | 8.04 | | 7613008 | |
| Dissolved Sulphate (SO4) | mg/L | 27 | 7613565 | 37 | 39 | 18 | 1.0 | 7613565 | |
| Alkalinity (Total as CaCO3) | mg/L | 290 | 7612994 | 140 | 410 | 130 | 1.0 | 7612994 | |
| Dissolved Chloride (Cl-) | mg/L | 38 | 7613553 | 18 | 24 | 9.0 | 1.0 | 7613553 | |
| Nitrite (N) | mg/L | <0.010 | 7613663 | 0.026 | 0.055 | 0.015 | 0.010 | 7613663 | |
| Nitrate (N) | mg/L | 0.11 | 7613663 | 1.08 | 0.26 | 0.54 | 0.10 | 7613663 | |
| Nitrate + Nitrite (N) | mg/L | 0.11 | 7613663 | 1.11 | 0.31 | 0.56 | 0.10 | 7613663 | |
| Metals | • | • | • | • | | • | • | • | |
| Dissolved Aluminum (AI) | ug/L | <4.9 | 7614958 | 7.3 | 5.9 | 9.4 | 4.9 | 7614958 | |
| Dissolved Antimony (Sb) | ug/L | <0.50 | 7614958 | 0.71 | <0.50 | 0.51 | 0.50 | 7614958 | |
| Dissolved Arsenic (As) | ug/L | 5.4 | 7614958 | 1.0 | <1.0 | <1.0 | 1.0 | 7614958 | |
| Dissolved Barium (Ba) | ug/L | 79 | 7614958 | 32 | 72 | 17 | 2.0 | 7614958 | |
| Dissolved Beryllium (Be) | ug/L | <0.40 | 7614958 | <0.40 | <0.40 | <0.40 | 0.40 | 7614958 | |
| Dissolved Boron (B) | ug/L | 28 | 7614958 | 17 | 16 | 16 | 10 | 7614958 | |
| Dissolved Cadmium (Cd) | ug/L | <0.090 | 7614958 | <0.090 | <0.090 | <0.090 | 0.090 | 7614958 | |
| RDL = Reportable Detection Limit | - | ı | | ı | | ı | | | |

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

N/A = Not Applicable



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

RCAP - COMPREHENSIVE (LAB FILTERED)

| BV Labs ID | | QUK162 | | QUK163 | QUK164 | QUK165 | | |
|---------------------------|-------|------------|----------|------------|------------|------------|-------|----------|
| Sampling Date | | 2021/09/28 | | 2021/09/28 | 2021/09/28 | 2021/09/28 | | |
| Sampling Date | | 13:00 | | 16:00 | 16:05 | 16:30 | | |
| | UNITS | BH3/MW | QC Batch | BH7A/MW | BH7B/MW | BH9/MW | RDL | QC Batch |
| Dissolved Calcium (Ca) | ug/L | 92000 | 7614958 | 53000 | 140000 | 42000 | 200 | 7614958 |
| Dissolved Chromium (Cr) | ug/L | <5.0 | 7614958 | <5.0 | <5.0 | <5.0 | 5.0 | 7614958 |
| Dissolved Cobalt (Co) | ug/L | <0.50 | 7614958 | <0.50 | <0.50 | <0.50 | 0.50 | 7614958 |
| Dissolved Copper (Cu) | ug/L | 17 | 7614958 | 23 | 21 | 11 | 0.90 | 7614958 |
| Dissolved Iron (Fe) | ug/L | <100 | 7614958 | <100 | <100 | <100 | 100 | 7614958 |
| Dissolved Lead (Pb) | ug/L | <0.50 | 7614958 | <0.50 | <0.50 | <0.50 | 0.50 | 7614958 |
| Dissolved Magnesium (Mg) | ug/L | 24000 | 7614958 | 12000 | 32000 | 8800 | 50 | 7614958 |
| Dissolved Manganese (Mn) | ug/L | 88 | 7614958 | 10 | 310 | <2.0 | 2.0 | 7614958 |
| Dissolved Molybdenum (Mo) | ug/L | 12 | 7614958 | 5.3 | 4.2 | 4.9 | 0.50 | 7614958 |
| Dissolved Nickel (Ni) | ug/L | 13 | 7614958 | 8.7 | 8.6 | 4.7 | 1.0 | 7614958 |
| Dissolved Phosphorus (P) | ug/L | <100 | 7614958 | <100 | <100 | <100 | 100 | 7614958 |
| Dissolved Potassium (K) | ug/L | 2800 | 7614958 | 3500 | 3600 | 3100 | 200 | 7614958 |
| Dissolved Selenium (Se) | ug/L | <2.0 | 7614958 | <2.0 | <2.0 | <2.0 | 2.0 | 7614958 |
| Dissolved Silicon (Si) | ug/L | 4700 | 7614958 | 2000 | 6900 | 2500 | 50 | 7614958 |
| Dissolved Silver (Ag) | ug/L | <0.090 | 7614958 | <0.090 | <0.090 | <0.090 | 0.090 | 7614958 |
| Dissolved Sodium (Na) | ug/L | 27000 | 7614958 | 14000 | 7300 | 12000 | 100 | 7614958 |
| Dissolved Strontium (Sr) | ug/L | 180 | 7614958 | 180 | 200 | 120 | 1.0 | 7614958 |
| Dissolved Thallium (TI) | ug/L | <0.050 | 7614958 | <0.050 | <0.050 | <0.050 | 0.050 | 7614958 |
| Dissolved Titanium (Ti) | ug/L | <5.0 | 7614958 | <5.0 | <5.0 | <5.0 | 5.0 | 7614958 |
| Dissolved Uranium (U) | ug/L | 0.59 | 7614958 | 1.2 | 0.74 | 0.59 | 0.10 | 7614958 |
| Dissolved Vanadium (V) | ug/L | <0.50 | 7614958 | <0.50 | 0.58 | <0.50 | 0.50 | 7614958 |
| Dissolved Zinc (Zn) | ug/L | 59 | 7614958 | 110 | 44 | 30 | 5.0 | 7614958 |

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

RCAP - SURFACE WATER (WATER)

| BV Labs ID | | QUK166 | | | QUK167 | | | QUK168 | | |
|-------------------------------------|---------|------------|-------|----------|------------|-------|----------|------------|-------|----------|
| Sampling Date | | 2021/09/28 | | | 2021/09/28 | | | 2021/09/28 | | |
| Jamping Bate | | 14:00 | | | 11:30 | | | 16:45 | | |
| | UNITS | SW1 | RDL | QC Batch | SW2 | RDL | QC Batch | SW4 | RDL | QC Batch |
| Calculated Parameters | | | | | | | | | | |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | 390 | 1.0 | 7610010 | 250 | 1.0 | 7610010 | 70 | 1.0 | 7610010 |
| Calculated TDS | mg/L | 650 | 1.0 | 7610017 | 380 | 1.0 | 7610017 | 170 | 1.0 | 7610017 |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | 3.5 | 1.0 | 7610010 | 3.6 | 1.0 | 7610010 | <1.0 | 1.0 | 7610010 |
| Hardness (CaCO3) | mg/L | 400 | 1.0 | 7610015 | 310 | 1.0 | 7610016 | 130 | 1.0 | 7610015 |
| Langelier Index (@ 20C) | N/A | 1.18 | | 7610013 | 1.13 | | 7610013 | -0.628 | | 7610013 |
| Langelier Index (@ 4C) | N/A | 0.930 | | 7610014 | 0.882 | | 7610014 | -0.878 | | 7610014 |
| Saturation pH (@ 20C) | N/A | 6.80 | | 7610013 | 7.06 | | 7610013 | 7.94 | | 7610013 |
| Saturation pH (@ 4C) | N/A | 7.05 | | 7610014 | 7.31 | | 7610014 | 8.19 | | 7610014 |
| Inorganics | | | | | | | | | | |
| Total Ammonia-N | mg/L | 0.082 | 0.050 | 7610470 | <0.050 | 0.050 | 7616218 | 0.14 | 0.050 | 7616218 |
| Conductivity | umho/cm | 1200 | 1.0 | 7613005 | 640 | 1.0 | 7611593 | 280 | 1.0 | 7611684 |
| Total Organic Carbon (TOC) | mg/L | 41 | 0.40 | 7613672 | 8.9 | 0.40 | 7613672 | 17 | 0.40 | 7613672 |
| Orthophosphate (P) | mg/L | 0.012 | 0.010 | 7611563 | 0.026 | 0.010 | 7611563 | 0.40 | 0.010 | 7611563 |
| рН | рН | 7.98 | | 7613008 | 8.19 | | 7611646 | 7.32 | | 7611688 |
| Total Phosphorus | mg/L | 1.9 | 0.1 | 7616206 | 0.043 | 0.004 | 7616206 | 0.46 | 0.02 | 7616206 |
| Dissolved Sulphate (SO4) | mg/L | <1.0 | 1.0 | 7611557 | 36 | 1.0 | 7611557 | 47 | 1.0 | 7611557 |
| Turbidity | NTU | 9.3 | 0.1 | 7610722 | 1.1 | 0.1 | 7610722 | 2.5 | 0.1 | 7610722 |
| Alkalinity (Total as CaCO3) | mg/L | 390 | 1.0 | 7612994 | 250 | 1.0 | 7611647 | 70 | 1.0 | 7611678 |
| Dissolved Chloride (Cl-) | mg/L | 150 | 2.0 | 7611552 | 30 | 1.0 | 7611552 | 14 | 1.0 | 7611552 |
| Nitrite (N) | mg/L | <0.010 | 0.010 | 7610949 | 0.031 | 0.010 | 7610949 | 0.039 | 0.010 | 7610949 |
| Nitrate (N) | mg/L | <0.10 | 0.10 | 7610949 | 5.26 | 0.10 | 7610949 | 0.45 | 0.10 | 7610949 |
| Metals | | | | | | | | | | |
| Dissolved Calcium (Ca) | mg/L | 130 | 0.05 | 7614963 | 95 | 0.05 | 7614963 | 38 | 0.05 | 7614094 |
| Dissolved Magnesium (Mg) | mg/L | 21 | 0.05 | 7614963 | 17 | 0.05 | 7614963 | 7.3 | 0.05 | 7614094 |
| Dissolved Potassium (K) | mg/L | 5 | 1 | 7614963 | 4 | 1 | 7614963 | 8 | 1 | 7614094 |
| Dissolved Sodium (Na) | mg/L | 89 | 0.5 | 7614963 | 12 | 0.5 | 7614963 | 2.5 | 0.5 | 7614094 |
| Total Aluminum (AI) | ug/L | 1300 | 4.9 | 7616141 | 67 | 4.9 | 7616141 | 140 | 4.9 | 7624000 |
| Total Antimony (Sb) | ug/L | <0.50 | 0.50 | 7616141 | <0.50 | 0.50 | 7616141 | <0.50 | 0.50 | 7624000 |
| Total Arsenic (As) | ug/L | 7.3 | 1.0 | 7616141 | <1.0 | 1.0 | 7616141 | <1.0 | 1.0 | 7624000 |
| Total Barium (Ba) | ug/L | 160 | 2.0 | 7616141 | 41 | 2.0 | 7616141 | 8.5 | 2.0 | 7624000 |
| Total Beryllium (Be) | ug/L | <0.40 | 0.40 | 7616141 | <0.40 | 0.40 | 7616141 | <0.40 | 0.40 | 7624000 |
| Total Boron (B) | ug/L | 43 | 10 | 7616141 | 22 | 10 | 7616141 | 44 | 10 | 7624000 |

QC Batch = Quality Control Batch



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

RCAP - SURFACE WATER (WATER)

| BV Labs ID | | QUK166 | | | QUK167 | | | QUK168 | | |
|-----------------------|-------|------------|-------|----------|------------|-------|----------|------------|-------|----------|
| Samuling Date | | 2021/09/28 | | | 2021/09/28 | | | 2021/09/28 | | |
| Sampling Date | | 14:00 | | | 11:30 | | | 16:45 | | |
| | UNITS | SW1 | RDL | QC Batch | SW2 | RDL | QC Batch | SW4 | RDL | QC Batch |
| Total Cadmium (Cd) | ug/L | <0.090 | 0.090 | 7616141 | <0.090 | 0.090 | 7616141 | 0.11 | 0.090 | 7624000 |
| Total Calcium (Ca) | ug/L | 160000 | 200 | 7616141 | 110000 | 200 | 7616141 | 41000 | 200 | 7624000 |
| Total Chromium (Cr) | ug/L | <5.0 | 5.0 | 7616141 | <5.0 | 5.0 | 7616141 | <5.0 | 5.0 | 7624000 |
| Total Cobalt (Co) | ug/L | 2.3 | 0.50 | 7616141 | <0.50 | 0.50 | 7616141 | 0.50 | 0.50 | 7624000 |
| Total Copper (Cu) | ug/L | 4.0 | 0.90 | 7616141 | 2.5 | 0.90 | 7616141 | 2.0 | 0.90 | 7624000 |
| Total Iron (Fe) | ug/L | 39000 | 100 | 7616141 | 130 | 100 | 7616141 | 230 | 100 | 7624000 |
| Total Lead (Pb) | ug/L | 2.0 | 0.50 | 7616141 | <0.50 | 0.50 | 7616141 | <0.50 | 0.50 | 7624000 |
| Total Magnesium (Mg) | ug/L | 24000 | 50 | 7616141 | 19000 | 50 | 7616141 | 7600 | 50 | 7624000 |
| Total Manganese (Mn) | ug/L | 1400 | 2.0 | 7616141 | 30 | 2.0 | 7616141 | 210 | 2.0 | 7624000 |
| Total Molybdenum (Mo) | ug/L | 0.82 | 0.50 | 7616141 | 1.3 | 0.50 | 7616141 | 1.3 | 0.50 | 7624000 |
| Total Nickel (Ni) | ug/L | 3.8 | 1.0 | 7616141 | <1.0 | 1.0 | 7616141 | <1.0 | 1.0 | 7624000 |
| Total Potassium (K) | ug/L | 5100 | 200 | 7616141 | 4000 | 200 | 7616141 | 7800 | 200 | 7624000 |
| Total Selenium (Se) | ug/L | <2.0 | 2.0 | 7616141 | <2.0 | 2.0 | 7616141 | <2.0 | 2.0 | 7624000 |
| Total Silicon (Si) | ug/L | 9900 | 50 | 7616141 | 4300 | 50 | 7616141 | 1800 | 50 | 7624000 |
| Total Silver (Ag) | ug/L | <0.090 | 0.090 | 7616141 | <0.090 | 0.090 | 7616141 | <0.090 | 0.090 | 7624000 |
| Total Sodium (Na) | ug/L | 93000 | 100 | 7616141 | 14000 | 100 | 7616141 | 1900 | 100 | 7624000 |
| Total Strontium (Sr) | ug/L | 280 | 1.0 | 7616141 | 190 | 1.0 | 7616141 | 44 | 1.0 | 7624000 |
| Total Thallium (TI) | ug/L | <0.050 | 0.050 | 7616141 | <0.050 | 0.050 | 7616141 | <0.050 | 0.050 | 7624000 |
| Total Titanium (Ti) | ug/L | 48 | 5.0 | 7616141 | 5.6 | 5.0 | 7616141 | 7.3 | 5.0 | 7624000 |
| Total Tungsten (W) | ug/L | <1.0 | 1.0 | 7616141 | <1.0 | 1.0 | 7616141 | <1.0 | 1.0 | 7624000 |
| Total Uranium (U) | ug/L | 1.4 | 0.10 | 7616141 | 2.4 | 0.10 | 7616141 | 0.10 | 0.10 | 7624000 |
| Total Vanadium (V) | ug/L | 3.4 | 0.50 | 7616141 | 0.87 | 0.50 | 7616141 | 0.79 | 0.50 | 7624000 |
| Total Zinc (Zn) | ug/L | 26 | 5.0 | 7616141 | <5.0 | 5.0 | 7616141 | 5.4 | 5.0 | 7624000 |
| Total Zirconium (Zr) | ug/L | <1.0 | 1.0 | 7616141 | <1.0 | 1.0 | 7616141 | <1.0 | 1.0 | 7624000 |

RDL = Reportable Detection Limit QC Batch = Quality Control Batch



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

RCAP - SURFACE WATER (WATER)

| | | QUK169 | | |
|-------------------------------------|---------|------------|-------|----------|
| Sampling Date | | 2021/09/28 | | |
| | | 17:00 | | |
| | UNITS | SW5 | RDL | QC Batch |
| Calculated Parameters | | | | |
| Bicarb. Alkalinity (calc. as CaCO3) | mg/L | 120 | 1.0 | 7610010 |
| Calculated TDS | mg/L | 140 | 1.0 | 7610017 |
| Carb. Alkalinity (calc. as CaCO3) | mg/L | <1.0 | 1.0 | 7610010 |
| Hardness (CaCO3) | mg/L | 130 | 1.0 | 7610016 |
| Langelier Index (@ 20C) | N/A | 0.150 | | 7610013 |
| Langelier Index (@ 4C) | N/A | -0.101 | | 7610014 |
| Saturation pH (@ 20C) | N/A | 7.71 | | 7610013 |
| Saturation pH (@ 4C) | N/A | 7.97 | | 7610014 |
| Inorganics | | | ı | |
| Total Ammonia-N | mg/L | 0.093 | 0.050 | 7616218 |
| Conductivity | umho/cm | 260 | 1.0 | 7611593 |
| Total Organic Carbon (TOC) | mg/L | 24 | 0.40 | 7613672 |
| Orthophosphate (P) | mg/L | 0.082 | 0.010 | 7611563 |
| рН | рН | 7.86 | | 761164 |
| Total Phosphorus | mg/L | 0.64 | 0.02 | 761620 |
| Dissolved Sulphate (SO4) | mg/L | <1.0 | 1.0 | 761155 |
| Turbidity | NTU | 5.0 | 0.1 | 7610722 |
| Alkalinity (Total as CaCO3) | mg/L | 120 | 1.0 | 761164 |
| Dissolved Chloride (Cl-) | mg/L | 9.7 | 1.0 | 761155 |
| Nitrite (N) | mg/L | <0.010 | 0.010 | 7610949 |
| Nitrate (N) | mg/L | <0.10 | 0.10 | 7610949 |
| Metals | | | ı | |
| Dissolved Calcium (Ca) | mg/L | 37 | 0.05 | 7614094 |
| Dissolved Magnesium (Mg) | mg/L | 7.9 | 0.05 | 7614094 |
| Dissolved Potassium (K) | mg/L | 3 | 1 | 7614094 |
| Dissolved Sodium (Na) | mg/L | 3.4 | 0.5 | 7614094 |
| Total Aluminum (Al) | ug/L | 940 | 4.9 | 7616143 |
| Total Antimony (Sb) | ug/L | <0.50 | 0.50 | 7616143 |
| Total Arsenic (As) | ug/L | 1.0 | 1.0 | 7616143 |
| Total Barium (Ba) | ug/L | 31 | 2.0 | 7616143 |
| | ug/L | <0.40 | 0.40 | 7616143 |
| Total Beryllium (Be) | | | | |



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

RCAP - SURFACE WATER (WATER)

| BV Labs ID | | QUK169 | | |
|--------------------------------|-------|------------|-------|----------|
| Samulina Data | | 2021/09/28 | | |
| Sampling Date | | 17:00 | | |
| | UNITS | SW5 | RDL | QC Batch |
| Total Cadmium (Cd) | ug/L | <0.090 | 0.090 | 7616141 |
| Total Calcium (Ca) | ug/L | 42000 | 200 | 7616141 |
| Total Chromium (Cr) | ug/L | <5.0 | 5.0 | 7616141 |
| Total Cobalt (Co) | ug/L | <0.50 | 0.50 | 7616141 |
| Total Copper (Cu) | ug/L | 2.2 | 0.90 | 7616141 |
| Total Iron (Fe) | ug/L | 1400 | 100 | 7616141 |
| Total Lead (Pb) | ug/L | 1.6 | 0.50 | 7616141 |
| Total Magnesium (Mg) | ug/L | 9000 | 50 | 7616141 |
| Total Manganese (Mn) | ug/L | 76 | 2.0 | 7616141 |
| Total Molybdenum (Mo) | ug/L | 1.2 | 0.50 | 7616141 |
| Total Nickel (Ni) | ug/L | 1.1 | 1.0 | 7616141 |
| Total Potassium (K) | ug/L | 3700 | 200 | 7616141 |
| Total Selenium (Se) | ug/L | <2.0 | 2.0 | 7616141 |
| Total Silicon (Si) | ug/L | 3500 | 50 | 7616141 |
| Total Silver (Ag) | ug/L | <0.090 | 0.090 | 7616141 |
| Total Sodium (Na) | ug/L | 3000 | 100 | 7616141 |
| Total Strontium (Sr) | ug/L | 57 | 1.0 | 7616141 |
| Total Thallium (TI) | ug/L | <0.050 | 0.050 | 7616141 |
| Total Titanium (Ti) | ug/L | 24 | 5.0 | 7616141 |
| Total Tungsten (W) | ug/L | <1.0 | 1.0 | 7616141 |
| Total Uranium (U) | ug/L | 0.44 | 0.10 | 7616141 |
| Total Vanadium (V) | ug/L | 2.3 | 0.50 | 7616141 |
| Total Zinc (Zn) | ug/L | 18 | 5.0 | 7616141 |
| Total Zirconium (Zr) | ug/L | <1.0 | 1.0 | 7616141 |
| RDL = Reportable Detection Lim | nit | | | |

RDL = Reportable Detection Limit QC Batch = Quality Control Batch



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

ELEMENTS BY ATOMIC SPECTROSCOPY (WATER)

| BV Labs ID | | QUK166 | QUK167 | QUK168 | QUK169 | | |
|-------------------------------|-------|------------|------------|------------|------------|-------|----------|
| Sampling Date | | 2021/09/28 | 2021/09/28 | 2021/09/28 | 2021/09/28 | | |
| Jamping Date | | 14:00 | 11:30 | 16:45 | 17:00 | | |
| | UNITS | SW1 | SW2 | SW4 | SW5 | RDL | QC Batch |
| Metals | | | | | | | |
| Dissolved Aluminum (AI) | ug/L | <4.9 | 9.4 | 24 | 11 | 4.9 | 7614958 |
| Dissolved Antimony (Sb) | ug/L | <0.50 | <0.50 | <0.50 | <0.50 | 0.50 | 7614958 |
| Dissolved Arsenic (As) | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |
| Dissolved Barium (Ba) | ug/L | 57 | 41 | 8.0 | 20 | 2.0 | 7614958 |
| Dissolved Beryllium (Be) | ug/L | <0.40 | <0.40 | <0.40 | <0.40 | 0.40 | 7614958 |
| Dissolved Bismuth (Bi) | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |
| Dissolved Boron (B) | ug/L | 34 | 21 | 44 | 22 | 10 | 7614958 |
| Dissolved Cadmium (Cd) | ug/L | <0.090 | <0.090 | 0.093 | <0.090 | 0.090 | 7614958 |
| Dissolved Calcium (Ca) | ug/L | 140000 | 100000 | 39000 | 41000 | 200 | 7614958 |
| Dissolved Chromium (Cr) | ug/L | <5.0 | <5.0 | <5.0 | <5.0 | 5.0 | 7614958 |
| Dissolved Cobalt (Co) | ug/L | <0.50 | <0.50 | <0.50 | <0.50 | 0.50 | 7614958 |
| Dissolved Copper (Cu) | ug/L | <0.90 | 1.9 | 1.7 | <0.90 | 0.90 | 7614958 |
| Dissolved Iron (Fe) | ug/L | <100 | <100 | 110 | 150 | 100 | 7614958 |
| Dissolved Lead (Pb) | ug/L | <0.50 | <0.50 | <0.50 | <0.50 | 0.50 | 7614958 |
| Dissolved Lithium (Li) | ug/L | <5.0 | <5.0 | <5.0 | <5.0 | 5.0 | 7614958 |
| Dissolved Magnesium (Mg) | ug/L | 25000 | 19000 | 7600 | 9000 | 50 | 7614958 |
| Dissolved Manganese (Mn) | ug/L | 18 | 20 | 200 | <2.0 | 2.0 | 7614958 |
| Dissolved Molybdenum (Mo) | ug/L | 0.63 | 1.4 | 1.6 | 1.2 | 0.50 | 7614958 |
| Dissolved Nickel (Ni) | ug/L | 2.4 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |
| Dissolved Phosphorus (P) | ug/L | <100 | 100 | 510 | 270 | 100 | 7614958 |
| Dissolved Potassium (K) | ug/L | 5100 | 4000 | 8200 | 3500 | 200 | 7614958 |
| Dissolved Selenium (Se) | ug/L | <2.0 | <2.0 | <2.0 | <2.0 | 2.0 | 7614958 |
| Dissolved Silicon (Si) | ug/L | 7200 | 4300 | 1500 | 2500 | 50 | 7614958 |
| Dissolved Silver (Ag) | ug/L | <0.090 | <0.090 | <0.090 | <0.090 | 0.090 | 7614958 |
| Dissolved Sodium (Na) | ug/L | 98000 | 13000 | 1900 | 3000 | 100 | 7614958 |
| Dissolved Strontium (Sr) | ug/L | 260 | 190 | 45 | 54 | 1.0 | 7614958 |
| Dissolved Tellurium (Te) | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |
| Dissolved Thallium (TI) | ug/L | <0.050 | <0.050 | <0.050 | <0.050 | 0.050 | 7614958 |
| Dissolved Tin (Sn) | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |
| Dissolved Titanium (Ti) | ug/L | <5.0 | <5.0 | <5.0 | <5.0 | 5.0 | 7614958 |
| Dissolved Tungsten (W) | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |
| Dissolved Uranium (U) | ug/L | 1.4 | 2.3 | 0.10 | 0.29 | 0.10 | 7614958 |
| RDL = Reportable Detection Li | mit | | | | | | |

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

ELEMENTS BY ATOMIC SPECTROSCOPY (WATER)

| BV Labs ID | | QUK166 | QUK167 | QUK168 | QUK169 | | |
|--------------------------|-------|------------|------------|------------|------------|------|----------|
| Sampling Date | | 2021/09/28 | 2021/09/28 | 2021/09/28 | 2021/09/28 | | |
| | | 14:00 | 11:30 | 16:45 | 17:00 | | |
| | UNITS | SW1 | SW2 | SW4 | SW5 | RDL | QC Batch |
| Dissolved Vanadium (V) | ug/L | <0.50 | 0.56 | <0.50 | 0.91 | 0.50 | 7614958 |
| Dissolved Zinc (Zn) | ug/L | <5.0 | <5.0 | <5.0 | <5.0 | 5.0 | 7614958 |
| Dissolved Zirconium (Zr) | ug/L | <1.0 | <1.0 | <1.0 | <1.0 | 1.0 | 7614958 |

RDL = Reportable Detection Limit QC Batch = Quality Control Batch



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

TEST SUMMARY

BV Labs ID: QUK162 Sample ID: BH3/MW Matrix: Water **Collected:** 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Alkalinity | AT | 7612994 | N/A | 2021/10/04 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/05 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7613553 | N/A | 2021/10/04 | Alina Dobreanu |
| Conductivity | AT | 7613005 | N/A | 2021/10/04 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7617408 | N/A | 2021/10/05 | Julianna Castiglione |
| Hardness (calculated as CaCO3) | | 7610016 | N/A | 2021/10/04 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7610018 | N/A | 2021/10/05 | Automated Statchk |
| Anion and Cation Sum | CALC | 7610019 | N/A | 2021/10/05 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7613663 | N/A | 2021/10/04 | Chandra Nandlal |
| рН | AT | 7613008 | 2021/10/01 | 2021/10/04 | Surinder Rai |
| Orthophosphate | KONE | 7613566 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7613565 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |

BV Labs ID: QUK163 Sample ID: BH7A/MW Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Alkalinity | AT | 7612994 | N/A | 2021/10/04 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/05 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7613553 | N/A | 2021/10/04 | Alina Dobreanu |
| Conductivity | AT | 7613005 | N/A | 2021/10/04 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7616559 | N/A | 2021/10/05 | Julianna Castiglione |
| Hardness (calculated as CaCO3) | | 7610016 | N/A | 2021/10/04 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7610018 | N/A | 2021/10/05 | Automated Statchk |
| Anion and Cation Sum | CALC | 7610019 | N/A | 2021/10/05 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7613663 | N/A | 2021/10/04 | Chandra Nandlal |
| РН | AT | 7613008 | 2021/10/01 | 2021/10/04 | Surinder Rai |
| Orthophosphate | KONE | 7613566 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7613565 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

TEST SUMMARY

BV Labs ID: QUK164 Sample ID: BH7B/MW Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Alkalinity | AT | 7612994 | N/A | 2021/10/04 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/05 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7613553 | N/A | 2021/10/04 | Alina Dobreanu |
| Conductivity | AT | 7613005 | N/A | 2021/10/04 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7616559 | N/A | 2021/10/04 | Julianna Castiglione |
| Hardness (calculated as CaCO3) | | 7610016 | N/A | 2021/10/04 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7610018 | N/A | 2021/10/05 | Automated Statchk |
| Anion and Cation Sum | CALC | 7610019 | N/A | 2021/10/05 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7613663 | N/A | 2021/10/04 | Chandra Nandlal |
| рН | AT | 7613008 | 2021/10/01 | 2021/10/04 | Surinder Rai |
| Orthophosphate | KONE | 7613566 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7613565 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |

BV Labs ID: QUK165 Sample ID: BH9/MW Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Alkalinity | AT | 7612994 | N/A | 2021/10/04 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/05 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7613553 | N/A | 2021/10/04 | Alina Dobreanu |
| Conductivity | AT | 7613005 | N/A | 2021/10/04 | Surinder Rai |
| Dissolved Organic Carbon (DOC) | TOCV/NDIR | 7616559 | N/A | 2021/10/05 | Julianna Castiglione |
| Hardness (calculated as CaCO3) | | 7610016 | N/A | 2021/10/04 | Automated Statchk |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Ion Balance (% Difference) | CALC | 7610018 | N/A | 2021/10/05 | Automated Statchk |
| Anion and Cation Sum | CALC | 7610019 | N/A | 2021/10/05 | Automated Statchk |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7613663 | N/A | 2021/10/04 | Chandra Nandlal |
| рН | AT | 7613008 | 2021/10/01 | 2021/10/04 | Surinder Rai |
| Orthophosphate | KONE | 7613566 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7613565 | N/A | 2021/10/04 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

TEST SUMMARY

BV Labs ID: QUK165 Dup Sample ID: BH9/MW

Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

Test Description Instrumentation Batch **Extracted Date Analyzed** Analyst Lab Filtered Metals by ICPMS ICP/MS 7614958 2021/10/02 2021/10/04 Prempal Bhatti

BV Labs ID: QUK166 Sample ID: SW1

Water

Matrix:

Collected: 2021/09/28

Shipped:

2021/09/29 Received:

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Alkalinity | AT | 7612994 | N/A | 2021/10/04 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/05 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7611552 | N/A | 2021/10/01 | Alina Dobreanu |
| Conductivity | AT | 7613005 | N/A | 2021/10/04 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7610015 | N/A | 2021/10/05 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7614963 | 2021/10/02 | 2021/10/04 | Meghaben Patel |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Total Metals Analysis by ICPMS | ICP/MS | 7616141 | N/A | 2021/10/05 | Nan Raykha |
| Total Ammonia-N | LACH/NH4 | 7610470 | N/A | 2021/10/01 | Viorica Rotaru |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7610949 | N/A | 2021/10/01 | Chandra Nandlal |
| рН | AT | 7613008 | 2021/10/01 | 2021/10/04 | Surinder Rai |
| Orthophosphate | KONE | 7611563 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7611557 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7613672 | N/A | 2021/10/05 | Julianna Castiglione |
| Total Phosphorus (Colourimetric) | LACH/P | 7616206 | 2021/10/04 | 2021/10/05 | Shivani Shivani |
| Turbidity | AT | 7610722 | N/A | 2021/10/01 | Neil Dassanayake |

BV Labs ID: QUK166 Dup Sample ID: SW1 Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-----------------|
| Alkalinity | AT | 7612994 | N/A | 2021/10/04 | Surinder Rai |
| Conductivity | AT | 7613005 | N/A | 2021/10/04 | Surinder Rai |
| Lab Filtered Metals Analysis by ICP | ICP | 7614963 | 2021/10/02 | 2021/10/04 | Meghaben Patel |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7610949 | N/A | 2021/10/01 | Chandra Nandlal |
| рН | AT | 7613008 | 2021/10/01 | 2021/10/04 | Surinder Rai |

BV Labs ID: QUK167 Sample ID: SW2 Matrix: Water

Collected: 2021/09/28 Shipped:

Received:

2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|------------------|-----------------|---------|-----------|---------------|--------------|
| Alkalinity | AT | 7611647 | N/A | 2021/10/01 | Surinder Rai |



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

TEST SUMMARY

BV Labs ID: QUK167 Sample ID: SW2

Collected: 2021/09/28 Shipped:

Matrix: Water

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/04 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7611552 | N/A | 2021/10/01 | Alina Dobreanu |
| Conductivity | AT | 7611593 | N/A | 2021/10/01 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7610016 | N/A | 2021/10/05 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7614963 | 2021/10/02 | 2021/10/04 | Meghaben Patel |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Total Metals Analysis by ICPMS | ICP/MS | 7616141 | N/A | 2021/10/05 | Nan Raykha |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7610949 | N/A | 2021/10/01 | Chandra Nandlal |
| рН | AT | 7611646 | 2021/09/30 | 2021/10/01 | Surinder Rai |
| Orthophosphate | KONE | 7611563 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7611557 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7613672 | N/A | 2021/10/05 | Julianna Castiglione |
| Total Phosphorus (Colourimetric) | LACH/P | 7616206 | 2021/10/04 | 2021/10/05 | Shivani Shivani |
| Turbidity | AT | 7610722 | N/A | 2021/10/01 | Neil Dassanayake |

BV Labs ID: QUK167 Dup Sample ID: SW2 Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|------------------|-----------------|---------|-----------|---------------|------------------|
| Turbidity | AT | 7610722 | N/A | 2021/10/01 | Neil Dassanayake |

BV Labs ID: QUK168

Test Description

Collected: Shipped:

2021/09/28

Sample ID: SW4 Matrix: Water

Received: 2021/09/29 Instrumentation Ratch Extracted Date Analyzed Analyst

| rest Description | instrumentation | Datch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|-------------------|
| Alkalinity | AT | 7611678 | N/A | 2021/10/01 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/01 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7611552 | N/A | 2021/10/01 | Alina Dobreanu |
| Conductivity | AT | 7611684 | N/A | 2021/10/01 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7610015 | N/A | 2021/10/05 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7614094 | 2021/10/02 | 2021/10/04 | Meghaben Patel |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Total Metals Analysis by ICPMS | ICP/MS | 7624000 | N/A | 2021/10/08 | Arefa Dabhad |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7610949 | N/A | 2021/10/01 | Chandra Nandlal |
| рН | AT | 7611688 | 2021/09/30 | 2021/10/01 | Surinder Rai |
| Orthophosphate | KONE | 7611563 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |



Client Project #: LON-21008138
Site Location: HUNTER FARM

Sampler Initials: JM

TEST SUMMARY

BV Labs ID: QUK168 Sample ID: SW4 Matrix: Water **Collected:** 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|------------------------------------|-----------------|---------|------------|---------------|----------------------|
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7611557 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7613672 | N/A | 2021/10/05 | Julianna Castiglione |
| Total Phosphorus (Colourimetric) | LACH/P | 7616206 | 2021/10/04 | 2021/10/05 | Shivani Shivani |
| Turbidity | AT | 7610722 | N/A | 2021/10/01 | Neil Dassanayake |

BV Labs ID: QUK168 Dup **Sample ID:** SW4

Matrix: Water

Collected: 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|------------------|-----------------|---------|------------|---------------|--------------|
| Alkalinity | AT | 7611678 | N/A | 2021/10/01 | Surinder Rai |
| Conductivity | AT | 7611684 | N/A | 2021/10/01 | Surinder Rai |
| pH | AT | 7611688 | 2021/09/30 | 2021/10/01 | Surinder Rai |

BV Labs ID: QUK169 Sample ID: SW5 Matrix: Water **Collected:** 2021/09/28

Shipped:

Received: 2021/09/29

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|--|-----------------|---------|------------|---------------|----------------------|
| Alkalinity | AT | 7611647 | N/A | 2021/10/01 | Surinder Rai |
| Carbonate, Bicarbonate and Hydroxide | CALC | 7610010 | N/A | 2021/10/04 | Automated Statchk |
| Chloride by Automated Colourimetry | KONE | 7611552 | N/A | 2021/10/01 | Alina Dobreanu |
| Conductivity | AT | 7611593 | N/A | 2021/10/01 | Surinder Rai |
| Hardness (calculated as CaCO3) | | 7610016 | N/A | 2021/10/05 | Automated Statchk |
| Lab Filtered Metals Analysis by ICP | ICP | 7614094 | 2021/10/02 | 2021/10/04 | Meghaben Patel |
| Lab Filtered Metals by ICPMS | ICP/MS | 7614958 | 2021/10/02 | 2021/10/04 | Prempal Bhatti |
| Total Metals Analysis by ICPMS | ICP/MS | 7616141 | N/A | 2021/10/05 | Nan Raykha |
| Total Ammonia-N | LACH/NH4 | 7616218 | N/A | 2021/10/04 | Amanpreet Sappal |
| Nitrate (NO3) and Nitrite (NO2) in Water | LACH | 7610949 | N/A | 2021/10/01 | Chandra Nandlal |
| рН | AT | 7611646 | 2021/09/30 | 2021/10/01 | Surinder Rai |
| Orthophosphate | KONE | 7611563 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Sat. pH and Langelier Index (@ 20C) | CALC | 7610013 | N/A | 2021/10/05 | Automated Statchk |
| Sat. pH and Langelier Index (@ 4C) | CALC | 7610014 | N/A | 2021/10/05 | Automated Statchk |
| Sulphate by Automated Colourimetry | KONE | 7611557 | N/A | 2021/10/01 | Avneet Kour Sudan |
| Total Dissolved Solids (TDS calc) | CALC | 7610017 | N/A | 2021/10/05 | Automated Statchk |
| Total Organic Carbon (TOC) | TOCV/NDIR | 7613672 | N/A | 2021/10/05 | Julianna Castiglione |
| Total Phosphorus (Colourimetric) | LACH/P | 7616206 | 2021/10/04 | 2021/10/05 | Shivani Shivani |
| Turbidity | AT | 7610722 | N/A | 2021/10/01 | Neil Dassanayake |



Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

GENERAL COMMENTS

Each temperature is the average of up to three cooler temperatures taken at receipt

| Package 1 | 1.0°C |
|-----------|-------|
| Package 2 | 2.7°C |

Results relate only to the items tested.



QUALITY ASSURANCE REPORT

exp Services Inc Client Project #: LON-21008138 Site Location: HUNTER FARM Sampler Initials: JM

| | | | Matrix Spike | Spike | SPIKED BLANK | BLANK | Method Blank | Blank | RPD | | QC Standard | ndard |
|----------|-----------------------------|------------|--------------|-----------|--------------|-----------|--------------|-------------|-----------|-----------|----------------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery QC Limits | QC Limits |
| 7610470 | Total Ammonia-N | 2021/10/01 | 99 | 75 - 125 | 66 | 80 - 120 | <0.050 | mg/L | NC | 20 | | |
| 7610722 | Turbidity | 2021/10/01 | | | 96 | 85 - 115 | <0.1 | NTU | 6.9 | 20 | | |
| 7610949 | Nitrate (N) | 2021/10/01 | 86 | 80 - 120 | 76 | 80 - 120 | <0.10 | mg/L | NC | 20 | | |
| 7610949 | Nitrite (N) | 2021/10/01 | 66 | 80 - 120 | 104 | 80 - 120 | <0.010 | mg/L | NC | 70 | | |
| 7611552 | Dissolved Chloride (CI-) | 2021/10/01 | NC | 80 - 120 | 105 | 80 - 120 | <1.0 | mg/L | 1.5 | 20 | | |
| 7611557 | Dissolved Sulphate (SO4) | 2021/10/01 | 101 | 75 - 125 | 104 | 80 - 120 | <1.0 | mg/L | 0.41 | 20 | | |
| 7611563 | Orthophosphate (P) | 2021/10/01 | 112 | 75 - 125 | 100 | 80 - 120 | <0.010 | mg/L | NC | 25 | | |
| 7611593 | Conductivity | 2021/10/01 | | | 66 | 85 - 115 | <1.0 | umho/c m | 0.62 | 25 | | |
| 7611646 | Н | 2021/10/01 | | | 102 | 98 - 103 | | | 0.95 | W/A | | |
| 7611647 | Alkalinity (Total as CaCO3) | 2021/10/01 | | | 96 | 85 - 115 | <1.0 | mg/L | 0.40 | 20 | | |
| 7611678 | Alkalinity (Total as CaCO3) | 2021/10/01 | | | 26 | 85 - 115 | <1.0 | mg/L | 1.0 | 20 | | |
| 7611684 | Conductivity | 2021/10/01 | | | 101 | 85 - 115 | <1.0 | umho/c m | 1.8 | 25 | | |
| 7611688 | рн | 2021/10/01 | | | 102 | 98 - 103 | | | 0.11 | N/A | | |
| 7612994 | Alkalinity (Total as CaCO3) | 2021/10/04 | | | 92 | 85 - 115 | <1.0 | mg/L | 1.3 | 20 | | |
| 7613005 | Conductivity | 2021/10/04 | | | 101 | 85 - 115 | <1.0 | umho/c m | 0.084 | 25 | | |
| 7613008 | рн | 2021/10/04 | | | 102 | 98 - 103 | | | 2.4 | N/A | | |
| 7613553 | Dissolved Chloride (CI-) | 2021/10/04 | NC | 80 - 120 | 102 | 80 - 120 | <1.0 | mg/L | 9.9 | 20 | | |
| 7613565 | Dissolved Sulphate (SO4) | 2021/10/04 | 95 | 75 - 125 | 101 | 80 - 120 | <1.0 | mg/L | 0.58 | 20 | | |
| 7613566 | Orthophosphate (P) | 2021/10/04 | 114 | 75 - 125 | 66 | 80 - 120 | <0.010 | mg/L | NC | 25 | | |
| 7613663 | Nitrate (N) | 2021/10/04 | 101 | 80 - 120 | 106 | 80 - 120 | <0.10 | mg/L | NC | 20 | | |
| 7613663 | Nitrite (N) | 2021/10/04 | 101 | 80 - 120 | 103 | 80 - 120 | <0.010 | mg/L | NC | 20 | | |
| 7613672 | Total Organic Carbon (TOC) | 2021/10/05 | 101 | 80 - 120 | 96 | 80 - 120 | <0.40 | mg/L | 0.17 | 20 | | |
| 7614094 | Dissolved Calcium (Ca) | 2021/10/05 | NC | 80 - 120 | 66 | 80 - 120 | <0.05 | mg/L | 1.5 | 25 | | |
| 7614094 | Dissolved Magnesium (Mg) | 2021/10/05 | 113 | 80 - 120 | 97 | 80 - 120 | <0.05 | mg/L | 1.3 | 25 | | |
| 7614094 | Dissolved Potassium (K) | 2021/10/05 | 106 | 80 - 120 | 66 | 80 - 120 | <1 | mg/L | 1.1 | 25 | | |
| 7614094 | Dissolved Sodium (Na) | 2021/10/05 | NC | 80 - 120 | 86 | 80 - 120 | <0.5 | mg/L | 0.16 | 25 | | |
| 7614958 | Dissolved Aluminum (AI) | 2021/10/04 | 101 | 80 - 120 | 107 | 80 - 120 | <4.9 | ng/L | 14 | 20 | | |
| 7614958 | Dissolved Antimony (Sb) | 2021/10/04 | 106 | 80 - 120 | 106 | 80 - 120 | <0.50 | ng/L | 1.2 | 20 | | |

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exp Services Inc Client Project #: LON-21008138

Site Location: HUNTER FARM Sampler Initials: JM

| | | | Matrix Snike | Snike | SPIKED BI ANK | BI ANK | Method Blank | Slank | RPD | | OC Standard | ndard |
|----------|---------------------------|------------|--------------|-----------|---------------|-----------|--------------|-------|-----------|-----------|----------------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery QC Limits | QC Limits |
| 7614958 | Dissolved Arsenic (As) | 2021/10/04 | 101 | 80 - 120 | 100 | 80 - 120 | <1.0 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Barium (Ba) | 2021/10/04 | 104 | 80 - 120 | 104 | 80 - 120 | <2.0 | 1/8n | 8.9 | 70 | | |
| 7614958 | Dissolved Beryllium (Be) | 2021/10/04 | 100 | 80 - 120 | 66 | 80 - 120 | <0.40 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Bismuth (Bi) | 2021/10/04 | 101 | 80 - 120 | 103 | 80 - 120 | <1.0 | ng/L | | | | |
| 7614958 | Dissolved Boron (B) | 2021/10/04 | 86 | 80 - 120 | 96 | 80 - 120 | <10 | ng/L | 0.47 | 20 | | |
| 7614958 | Dissolved Cadmium (Cd) | 2021/10/04 | 103 | 80 - 120 | 103 | 80 - 120 | <0.090 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Calcium (Ca) | 2021/10/04 | 96 | 80 - 120 | 104 | 80 - 120 | <200 | ng/L | 0.15 | 20 | | |
| 7614958 | Dissolved Chromium (Cr) | 2021/10/04 | 100 | 80 - 120 | 100 | 80 - 120 | <5.0 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Cobalt (Co) | 2021/10/04 | 103 | 80 - 120 | 66 | 80 - 120 | <0.50 | 1/8n | NC | 70 | | |
| 7614958 | Dissolved Copper (Cu) | 2021/10/04 | 86 | 80 - 120 | 86 | 80 - 120 | <0.90 | ng/L | 2.3 | 20 | | |
| 7614958 | Dissolved Iron (Fe) | 2021/10/04 | 102 | 80 - 120 | 102 | 80 - 120 | <100 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Lead (Pb) | 2021/10/04 | 96 | 80 - 120 | 100 | 80 - 120 | <0.50 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Lithium (Li) | 2021/10/04 | 106 | 80 - 120 | 108 | 80 - 120 | <5.0 | ng/L | | | | |
| 7614958 | Dissolved Magnesium (Mg) | 2021/10/04 | 101 | 80 - 120 | 102 | 80 - 120 | <50 | ng/L | 1.4 | 20 | | |
| 7614958 | Dissolved Manganese (Mn) | 2021/10/04 | 104 | 80 - 120 | 104 | 80 - 120 | <2.0 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Molybdenum (Mo) | 2021/10/04 | 104 | 80 - 120 | 103 | 80 - 120 | <0.50 | ng/L | 1.1 | 20 | | |
| 7614958 | Dissolved Nickel (Ni) | 2021/10/04 | 86 | 80 - 120 | 98 | 80 - 120 | <1.0 | ng/L | 11 | 20 | | |
| 7614958 | Dissolved Phosphorus (P) | 2021/10/04 | 105 | 80 - 120 | 116 | 80 - 120 | <100 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Potassium (K) | 2021/10/04 | 104 | 80 - 120 | 105 | 80 - 120 | <200 | ng/L | 0.67 | 20 | | |
| 7614958 | Dissolved Selenium (Se) | 2021/10/04 | 6 | 80 - 120 | 101 | 80 - 120 | <2.0 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Silicon (Si) | 2021/10/04 | 100 | 80 - 120 | 104 | 80 - 120 | <50 | ng/L | 0.55 | 20 | | |
| 7614958 | Dissolved Silver (Ag) | 2021/10/04 | 101 | 80 - 120 | 102 | 80 - 120 | <0.090 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Sodium (Na) | 2021/10/04 | 6 | 80 - 120 | 101 | 80 - 120 | <100 | ng/L | 2.2 | 20 | | |
| 7614958 | Dissolved Strontium (Sr) | 2021/10/04 | 103 | 80 - 120 | 101 | 80 - 120 | <1.0 | ng/L | 0.83 | 20 | | |
| 7614958 | Dissolved Tellurium (Te) | 2021/10/04 | 107 | 80 - 120 | 103 | 80 - 120 | <1.0 | ng/L | | | | |
| 7614958 | Dissolved Thallium (TI) | 2021/10/04 | 99 | 80 - 120 | 100 | 80 - 120 | <0.050 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Tin (Sn) | 2021/10/04 | 105 | 80 - 120 | 105 | 80 - 120 | <1.0 | ng/L | | | | |
| 7614958 | Dissolved Titanium (Ti) | 2021/10/04 | 66 | 80 - 120 | 102 | 80 - 120 | <5.0 | ng/L | NC | 20 | | |
| 7614958 | Dissolved Tungsten (W) | 2021/10/04 | 100 | 80 - 120 | 98 | 80 - 120 | <1.0 | ng/L | | | | |
| 7614958 | Dissolved Uranium (U) | 2021/10/04 | 66 | 80 - 120 | 100 | 80 - 120 | <0.10 | ng/L | 4.5 | 20 | | |
| 7614958 | Dissolved Vanadium (V) | 2021/10/04 | 102 | 80 - 120 | 101 | 80 - 120 | <0.50 | ng/L | NC | 20 | | |

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exp Services Inc Client Project #: LON-21008138 Site Location: HUNTER FARM Sampler Initials: JM

| | | | Matrix Spike | Spike | SPIKED BLANK | BLANK | Method Blank | Slank | RPD | 0 | QC Standard | ndard |
|----------|--------------------------|------------|--------------|-----------|--------------|-----------|-------------------|-------|-----------|-----------|-------------|-----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7614958 | Dissolved Zinc (Zn) | 2021/10/04 | 101 | 80 - 120 | 101 | 80 - 120 | <5.0 | 1/Bn | 1.9 | 20 | | |
| 7614958 | Dissolved Zirconium (Zr) | 2021/10/04 | 111 | 80 - 120 | 110 | 80 - 120 | <1.0 | 1/Bn | | | | |
| 7614963 | Dissolved Calcium (Ca) | 2021/10/04 | 26 | 80 - 120 | 100 | 80 - 120 | 0.05, RDL=0.05 | mg/L | 0.79 | 25 | | |
| 7614963 | Dissolved Magnesium (Mg) | 2021/10/04 | 86 | 80 - 120 | 66 | 80 - 120 | <0.05 | mg/L | 0.94 | 25 | | |
| 7614963 | Dissolved Potassium (K) | 2021/10/04 | 66 | 80 - 120 | 100 | 80 - 120 | <1 | mg/L | 1.1 | 25 | | |
| 7614963 | Dissolved Sodium (Na) | 2021/10/04 | 86 | 80 - 120 | 66 | 80 - 120 | <0.5 | mg/L | 0.79 | 25 | | |
| 7616141 | Total Aluminum (AI) | 2021/10/05 | 104 | 80 - 120 | 105 | 80 - 120 | <4.9 | ng/L | 3.7 | 20 | | |
| 7616141 | Total Antimony (Sb) | 2021/10/05 | 108 | 80 - 120 | 103 | 80 - 120 | <0.50 | ng/L | 6.3 | 20 | | |
| 7616141 | Total Arsenic (As) | 2021/10/05 | 105 | 80 - 120 | 102 | 80 - 120 | <1.0 | 1/Bn | 0.52 | 20 | | |
| 7616141 | Total Barium (Ba) | 2021/10/05 | 103 | 80 - 120 | 103 | 80 - 120 | <2.0 | T/Bn | 0.42 | 20 | | |
| 7616141 | Total Beryllium (Be) | 2021/10/05 | 105 | 80 - 120 | 100 | 80 - 120 | <0.40 | 7/Bn | NC | 20 | | |
| 7616141 | Total Boron (B) | 2021/10/05 | 100 | 80 - 120 | 6 | 80 - 120 | <10 | ng/L | 1.4 | 20 | | |
| 7616141 | Total Cadmium (Cd) | 2021/10/05 | 103 | 80 - 120 | 100 | 80 - 120 | <0.090 | ng/L | NC | 20 | | |
| 7616141 | Total Calcium (Ca) | 2021/10/05 | 96 | 80 - 120 | 101 | 80 - 120 | <200 | ng/L | 0.18 | 20 | | |
| 7616141 | Total Chromium (Cr) | 2021/10/05 | 103 | 80 - 120 | 101 | 80 - 120 | <5.0 | ng/L | NC | 20 | | |
| 7616141 | Total Cobalt (Co) | 2021/10/05 | 105 | 80 - 120 | 102 | 80 - 120 | <0.50 | ng/L | NC | 20 | | |
| 7616141 | Total Copper (Cu) | 2021/10/05 | 108 | 80 - 120 | 108 | 80 - 120 | <0.90 | ng/L | NC | 20 | | |
| 7616141 | Total Iron (Fe) | 2021/10/05 | 102 | 80 - 120 | 100 | 80 - 120 | <100 | ng/L | 12 | 20 | | |
| 7616141 | Total Lead (Pb) | 2021/10/05 | 97 | 80 - 120 | 94 | 80 - 120 | <0.50 | ng/L | NC | 20 | | |
| 7616141 | Total Magnesium (Mg) | 2021/10/05 | 101 | 80 - 120 | 104 | 80 - 120 | <50 | ng/L | 4.3 | 20 | | |
| 7616141 | Total Manganese (Mn) | 2021/10/05 | 103 | 80 - 120 | 102 | 80 - 120 | <2.0 | ng/L | 0.16 | 20 | | |
| 7616141 | Total Molybdenum (Mo) | 2021/10/05 | 106 | 80 - 120 | 103 | 80 - 120 | <0.50 | ng/L | 8.5 | 20 | | |
| 7616141 | Total Nickel (Ni) | 2021/10/05 | 100 | 80 - 120 | 100 | 80 - 120 | <1.0 | ng/L | NC | 20 | | |
| 7616141 | Total Potassium (K) | 2021/10/05 | 104 | 80 - 120 | 105 | 80 - 120 | <200 | ng/L | 1.1 | 20 | | |
| 7616141 | Total Selenium (Se) | 2021/10/05 | 105 | 80 - 120 | 107 | 80 - 120 | <2.0 | ng/L | NC | 20 | | |
| 7616141 | Total Silicon (Si) | 2021/10/05 | 100 | 80 - 120 | 101 | 80 - 120 | <50 | ng/L | 3.4 | 20 | | |
| 7616141 | Total Silver (Ag) | 2021/10/05 | 103 | 80 - 120 | 102 | 80 - 120 | <0.090 | ng/L | NC | 20 | | |
| 7616141 | Total Sodium (Na) | 2021/10/05 | 105 | 80 - 120 | 102 | 80 - 120 | <100 | ng/L | 5.2 | 20 | | |
| 7616141 | Total Strontium (Sr) | 2021/10/05 | 97 | 80 - 120 | 96 | 80 - 120 | <1.0 | ng/L | 1.8 | 20 | | |
| 7616141 | Total Thallium (TI) | 2021/10/05 | 97 | 80 - 120 | 92 | 80 - 120 | <0.050 | ng/L | NC | 20 | | |

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exp Services Inc Client Project #: LON-21008138

Site Location: HUNTER FARM Sampler Initials: JM

| | | | Matrix Spike | Spike | SPIKED BLANK | BLANK | Method Blank | Blank | RPD | ٥ | QC Sta | QC Standard |
|----------|--------------------------|------------|--------------|-----------|--------------|-----------|--------------|-------|-----------|-----------|------------|-------------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | % Recovery | QC Limits |
| 7616141 | Total Titanium (Ti) | 2021/10/05 | 86 | 80 - 120 | 100 | 80 - 120 | <5.0 | 1/8n | NC | 20 | | |
| 7616141 | Total Tungsten (W) | 2021/10/05 | 109 | 80 - 120 | 103 | 80 - 120 | <1.0 | ng/L | NC | 20 | | |
| 7616141 | Total Uranium (U) | 2021/10/05 | 92 | 80 - 120 | 90 | 80 - 120 | <0.10 | ng/L | 0.88 | 20 | | |
| 7616141 | Total Vanadium (V) | 2021/10/05 | 106 | 80 - 120 | 102 | 80 - 120 | <0.50 | ng/L | 12 | 20 | | |
| 7616141 | Total Zinc (Zn) | 2021/10/05 | 104 | 80 - 120 | 105 | 80 - 120 | <5.0 | 1/8n | 3.1 | 20 | | |
| 7616141 | Total Zirconium (Zr) | 2021/10/05 | 111 | 80 - 120 | 104 | 80 - 120 | <1.0 | 1/8n | NC | 20 | | |
| 7616206 | Total Phosphorus | 2021/10/05 | 101 | 80 - 120 | 105 | 80 - 120 | <0.004 | T/Bm | NC | 20 | 06 | 80 - 120 |
| 7616218 | Total Ammonia-N | 2021/10/04 | 100 | 75 - 125 | 100 | 80 - 120 | <0.050 | mg/L | NC | 20 | | |
| 7616559 | Dissolved Organic Carbon | 2021/10/04 | 92 | 80 - 120 | 26 | 80 - 120 | <0.40 | mg/L | 0.040 | 20 | | |
| 7617408 | Dissolved Organic Carbon | 2021/10/05 | 101 | 80 - 120 | 86 | 80 - 120 | <0.40 | mg/L | 2.8 | 20 | | |
| 7624000 | Total Aluminum (AI) | 2021/10/08 | 68 | 80 - 120 | 103 | 80 - 120 | <4.9 | ng/L | | | | |
| 7624000 | Total Antimony (Sb) | 2021/10/08 | 94 | 80 - 120 | 105 | 80 - 120 | <0.50 | ng/L | | | | |
| 7624000 | Total Arsenic (As) | 2021/10/08 | 68 | 80 - 120 | 101 | 80 - 120 | <1.0 | 1/8n | | | | |
| 7624000 | Total Barium (Ba) | 2021/10/08 | 87 | 80 - 120 | 66 | 80 - 120 | <2.0 | 1/8n | | | | |
| 7624000 | Total Beryllium (Be) | 2021/10/08 | 88 | 80 - 120 | 66 | 80 - 120 | <0.40 | T/Bn | | | | |
| 7624000 | Total Boron (B) | 2021/10/08 | 66 (1) | 80 - 120 | 06 | 80 - 120 | <10 | 1/8n | | | | |
| 7624000 | Total Cadmium (Cd) | 2021/10/08 | 90 | 80 - 120 | 102 | 80 - 120 | <0.090 | ng/L | NC | 20 | | |
| 7624000 | Total Calcium (Ca) | 2021/10/08 | 67 (1) | 80 - 120 | 105 | 80 - 120 | <200 | 1/8n | | | | |
| 7624000 | Total Chromium (Cr) | 2021/10/08 | 85 | 80 - 120 | 97 | 80 - 120 | <5.0 | ng/L | NC | 20 | | |
| 7624000 | Total Cobalt (Co) | 2021/10/08 | 88 | 80 - 120 | 100 | 80 - 120 | <0.50 | ng/L | | | | |
| 7624000 | Total Copper (Cu) | 2021/10/08 | 87 | 80 - 120 | 98 | 80 - 120 | <0.90 | ng/L | NC | 20 | | |
| 7624000 | Total Iron (Fe) | 2021/10/08 | 88 | 80 - 120 | 66 | 80 - 120 | <100 | ng/L | | | | |
| 7624000 | Total Lead (Pb) | 2021/10/08 | 88 | 80 - 120 | 102 | 80 - 120 | <0.50 | ng/L | NC | 20 | | |
| 7624000 | Total Magnesium (Mg) | 2021/10/08 | 82 | 80 - 120 | 101 | 80 - 120 | <50 | ng/L | | | | |
| 7624000 | Total Manganese (Mn) | 2021/10/08 | 82 | 80 - 120 | 98 | 80 - 120 | <2.0 | ng/L | | | | |
| 7624000 | Total Molybdenum (Mo) | 2021/10/08 | 86 | 80 - 120 | 96 | 80 - 120 | <0.50 | ng/L | | | | |
| 7624000 | Total Nickel (Ni) | 2021/10/08 | 87 | 80 - 120 | 96 | 80 - 120 | <1.0 | ng/L | 15 | 20 | | |
| 7624000 | Total Potassium (K) | 2021/10/08 | 86 | 80 - 120 | 66 | 80 - 120 | <200 | ng/L | | | | |
| 7624000 | Total Selenium (Se) | 2021/10/08 | 91 | 80 - 120 | 107 | 80 - 120 | <2.0 | ng/L | | | | |
| 7624000 | Total Silicon (Si) | 2021/10/08 | 89 | 80 - 120 | 102 | 80 - 120 | <50 | ng/L | | | | |
| 7624000 | Total Silver (Ag) | 2021/10/08 | 68 | 80 - 120 | 66 | 80 - 120 | <0.090 | T/Bn | | | | |
| | | | | | | | | | | | | |

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exp Services Inc

Sampler Initials: JM

Client Project #: LON-21008138 Site Location: HUNTER FARM

| | | | Matrix Spike | Spike | SPIKED BLANK | BLANK | Method Blank | 3lank | RPD | D | QC Standard | dard |
|----------|------------------------------|------------|--------------|-----------|--------------|-----------|---------------------|-------|-----------|-----------|--------------------------------|----------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | UNITS | Value (%) | QC Limits | QC Limits % Recovery QC Limits | C Limits |
| 7624000 | Total Sodium (Na) | 2021/10/08 | 59 (1) | 80 - 120 | 101 | 80 - 120 | <100 | 1/8n | | | | |
| 7624000 | Total Strontium (Sr) | 2021/10/08 | 64 (1) | 80 - 120 | 86 | 80 - 120 | <1.0 | 1/8n | | | | |
| 7624000 | 7624000 Total Thallium (TI) | 2021/10/08 | 06 | 80 - 120 | 101 | 80 - 120 | <0.050 | 1/8n | | | | |
| 7624000 | Total Titanium (Ti) | 2021/10/08 | 85 | 80 - 120 | 100 | 80 - 120 | <5.0 | 1/8n | | | | |
| 7624000 | Total Tungsten (W) | 2021/10/08 | 88 | 80 - 120 | 901 | 80 - 120 | <1.0 | 1/8n | | | | |
| 7624000 | Total Uranium (U) | 2021/10/08 | 68 | 80 - 120 | 101 | 80 - 120 | <0.10 | 1/8n | | | | |
| 7624000 | Total Vanadium (V) | 2021/10/08 | 88 | 80 - 120 | 66 | 80 - 120 | <0.50 | 1/8n | | | | |
| 7624000 | Total Zinc (Zn) | 2021/10/08 | 06 | 80 - 120 | 103 | 80 - 120 | <5.0 | 1/8n | NC | 20 | | |
| 7624000 | 7624000 Total Zirconium (Zr) | 2021/10/08 | 93 | 80 - 120 | 102 | 80 - 120 | <1.0 | ng/L | | | | |
| | | | | | | | | | | | | |

N/A = Not Applicable

Duplicate: Paired analysis of a separate portion of the same sample. Used to evaluate the variance in the measurement.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.

QC Standard: A sample of known concentration prepared by an external agency under stringent conditions. Used as an independent check of method accuracy.

Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.

Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.

NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)

NC (Duplicate RPD): The duplicate RPD was not calculated. The concentration in the sample and/or duplicate was too low to permit a reliable RPD calculation (absolute difference <= 2x RDL).

(1) Recovery or RPD for this parameter is outside control limits. The overall quality control for this analysis meets acceptability criteria.



Report Date: 2021/10/08

exp Services Inc

Client Project #: LON-21008138 Site Location: HUNTER FARM

Sampler Initials: JM

VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by:

Anastassia Hamanov, Scientific Specialist

Ewa Pranjic, M.Sc., C.Chem, Scientific Specialist

BV Labs has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.

Appendix K – Water Balance Assessment



TABLE K1 - PRE-DEVELOPMENT WATER BALANCE CALCULATIONS

| AREA A - Drains to the Sandusky Drain | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | | ding Capacity mm) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|-------------|-------|----------------------|------------------------|------------------------|------------------------|--------------------|------|--------|
| Agricultural Land | 0 | 111,551 | 190,407 | Sandy Loam | В | | 150 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Pasture and Shrubs | 0 | 68,966 | | Sand | Α | | 100 | 0.8 | | | | | |
| Mature Forest | 0 | 2,090 | | Sandy Loam | В | : | 300 | 0.8 | | | | | |
| Richmond Street | 5,460 | 2,340 | | Sandy Loam | В | | 75 | 0.6 | | | | | |
| | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | ост | NOV | DEC | Totals |
| Average Temperature (°C) | -5.6 | -4.5 | -0.1 | 6.8 | 13.1 | 18.3 | 20.8 | 19.7 | 15.5 | 9.2 | 3.4 | -2.6 | |
| Total Precipitation (mm/month) | 74.2 | 65.5 | 71.5 | 83.4 | 89.8 | 91.7 | 82.7 | 82.9 | 103.0 | 81.3 | 98.0 | 87.5 | 1011.5 |
| Precipitation as rain (mm/month) | 24.5 | 27.1 | 53.2 | 83.4 | 89.8 | 91.7 | 82.7 | 82.9 | 103.0 | 81.3 | 98.0 | 48.7 | |
| Precipitation as snow (mm/month) | 49.7 | 38.4 | 18.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 38.8 | |
| Potential Snow Melt (mm/month) | 20.9 | 32.8 | 49.1 | 26.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 19.9 | |
| Actual Snow Melt (mm/month) | 20.9 | 32.8 | 49.1 | 22.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 19.9 | |
| Snow Storage (mm/month) | 47.7 | 53.4 | 22.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 18.9 | |
| Agricultural Land | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 115.6 | 90.5 | 56.3 | 30.5 | 16.0 | 10.0 | 570.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -32.9 | -7.6 | 46.7 | 50.8 | 82.0 | 58.6 | 441.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m³/month) | 993 | 1205 | 2264 | 4284 | 7842 | 11445 | 12895 | 10095 | 6280 | 3402 | 1785 | 1116 | |
| Estimated Runoff (m³/month) | 993 4075 | | | | | | | | | | | | 63606 |
| Estimated Infiltration (m³/month) | | 5472 | 6402 | 3015 | 870 | 0 | 0 | 0 | 2084 | 2267 | 3659 | 6532 | 34375 |
| Estimated inflitration (m /month) | 0 | 0 | 2744 | 4523 | 1305 | 0 | 0 | 0 | 3126 | 3400 | 5488 | 0 | 20586 |
| Pasture and Shrubs | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 114.0 | 88.6 | 56.3 | 30.5 | 16.0 | 10.0 | 566.7 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -31.3 | -5.7 | 46.7 | 50.8 | 82.0 | 58.6 | 444.8 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 49.2 | 13.5 | 3.9 | 0.0 | 0.0 | 0.0 | 9.3 | 10.2 | 16.4 | 58.6 | 246.6 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 32.8 | 54.1 | 15.6 | 0.0 | 0.0 | 0.0 | 37.4 | 40.6 | 65.6 | 0.0 | 246.1 |
| Estimated Actual Evapotranspiration (m ³ /month) | 614 | 745 | 1400 | 2648 | 4848 | 7076 | 7862 | 6110 | 3883 | 2103 | 1103 | 690 | 39083 |
| Estimated Runoff (m³/month) | 2519 | 3383 | 3392 | 932 | 269 | 0 | 0 | 0 | 644 | 701 | 1131 | 4038 | 17010 |
| Estimated Infiltration (m³/month) | 0 | 0 | 2262 | 3729 | 1076 | 0 | 0 | 0 | 2577 | 2803 | 4524 | 0 | 16970 |
| Mature Forest | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 117.2 | 92.6 | 56.3 | 30.5 | 16.0 | 10.0 | 573.9 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -34.5 | -9.7 | 46.7 | 50.8 | 82.0 | 58.6 | 437.6 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 49.2 | 13.5 | 3.9 | 0.0 | 0.0 | 0.0 | 9.3 | 10.2 | 16.4 | 58.6 | 246.6 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 32.8 | 54.1 | 15.6 | 0.0 | 0.0 | 0.0 | 37.4 | 40.6 | 65.6 | 0.0 | 246.1 |
| Estimated Actual Evapotranspiration (m ³ /month) | 19 | 23 | 42 | 80 | 147 | 214 | 245 | 194 | 118 | 64 | 33 | 21 | 1199 |
| Estimated Runoff (m ³ /month) | 76 | 103 | 103 | 28 | 8 | 0 | 0 | 0 | 20 | 21 | 34 | 122 | 515 |
| Estimated Infiltration (m³/month) | 0 | 0 | 69 | 113 | 33 | 0 | 0 | 0 | 78 | 85 | 137 | 0 | 514 |
| Richmond Street (pervious) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 7.8 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Intitration (mm/month) Estimated Actual Evapotranspiration (m³/month) | | | | | | | | | | | | | |
| | 21 | 25 | 48 | 90 | 165 | 240 | 263 | 203 | 132 | 71 | 37 | 23 | 1318 |
| Estimated Runoff (m³/month) | 85 | 115 | 134 | 63 | 18 | 0 | 0 | 0 | 44 | 48 | 77 | 137 | 721 |
| Estimated Infiltration (m ³ /month) | 0 | 0 | 58 | 95 | 27 | 0 | 0 | 0 | 66 | 71 | 115 | 0 | 432 |



| IMPERVIOUS AREAS | | | | | | | | | | | | | |
|---|------|------|-------|------|-------|-------|-------|-------|-------|------|-------|-------|--------|
| Estimated Actual Evapotranspiration (mm/month) | 8.2 | 10.8 | 18.4 | 19.1 | 16.2 | 16.5 | 14.9 | 14.9 | 18.5 | 14.6 | 17.6 | 12.3 | 182.1 |
| Surplus (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Runoff (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Estimated Actual Evapotranspiration (m ³ /month) | 45 | 59 | 101 | 104 | 88 | 90 | 81 | 81 | 101 | 80 | 96 | 67 | 994 |
| Estimated Runoff (m³/month) | 203 | 268 | 458 | 474 | 402 | 411 | 370 | 371 | 461 | 364 | 439 | 307 | 4529 |
| Estimated Infiltration (m³/month) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AREA A TOTALS | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 1691 | 2056 | 3855 | 7206 | 13090 | 19066 | 21346 | 16684 | 10514 | 5721 | 3055 | 1917 | 106201 |
| Estimated Runoff (m³/month) | 6959 | 9341 | 10489 | 4514 | 1568 | 411 | 370 | 371 | 3252 | 3400 | 5340 | 11136 | 57150 |
| Estimated Infiltration (m³/month) | 0 | 0 | 5131 | 8460 | 2441 | 0 | 0 | 0 | 5846 | 6359 | 10265 | 0 | 38502 |



| AREA B - Drains to Wetland C | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | | ling Capacity nm) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|------------|-------|----------------------|------------------------|------------------------|------------------------|--------------------|------|--------|
| Agricultural Land | 0 | 10,005 | 71,714 | Sandy Loam | В | 1 | 50 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Pasture and Shrubs | 0 | 14,552 | | Sandy Loam | В | 1 | 50 | 0.8 | | | | | |
| Mature Forest | | 13,804 | | Sandy Loam | В | 3 | 00 | 0.7 | | | | | |
| Urban Lawn/Grassed Area | | 33,352 | | Sandy Loam | В | 7 | 75 | 0.6 | | | | | |
| Agricultural Land | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | ост | NOV | DEC | Totals |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 115.6 | 90.5 | 56.3 | 30.5 | 16.0 | 10.0 | 570.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -32.9 | -7.6 | 46.7 | 50.8 | 82.0 | 58.6 | 441.3 |
| Initial Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m³/month) | 89 | 108 | 203 | 384 | 703 | 1027 | 1157 | 905 | 563 | 305 | 160 | 100 | 5705 |
| Estimated Runoff (m³/month) | 365 | 491 | 574 | 270 | 78 | 0 | 0 | 0 | 187 | 203 | 328 | 586 | 3083 |
| Estimated Infiltration (m³/month) | 0 | 0 | 246 | 406 | 117 | 0 | 0 | 0 | 280 | 305 | 492 | 0 | 1846 |
| Mature Forest | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 117.2 | 92.6 | 56.3 | 30.5 | 16.0 | 10.0 | 573.9 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -34.5 | -9.7 | 46.7 | 50.8 | 82.0 | 58.6 | 437.6 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 53.3 | 20.3 | 5.9 | 0.0 | 0.0 | 0.0 | 14.0 | 15.2 | 24.6 | 58.6 | 277.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 28.7 | 47.3 | 13.7 | 0.0 | 0.0 | 0.0 | 32.7 | 35.6 | 57.4 | 0.0 | 215.3 |
| Estimated Actual Evapotranspiration (m³/month) | 123 | 149 | 280 | 530 | 970 | 1416 | 1618 | 1278 | 777 | 421 | 221 | 138 | 7922 |
| Estimated Runoff (m³/month) | 504 | 677 | 736 | 280 | 81 | 0 | 0 | 0 | 193 | 210 | 340 | 808 | 3829 |
| Estimated Infiltration (m³/month) | 0 | 0 | 396 | 653 | 188 | 0 | 0 | 0 | 451 | 491 | 792 | 0 | 2972 |
| Urban Lawn/Grassed Area | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 297 | 360 | 677 | 1281 | 2345 | 3422 | 3745 | 2895 | 1878 | 1017 | 534 | 334 | 18784 |
| Estimated Runoff (m³/month) | 1218 | 1636 | 1914 | 902 | 260 | 0 | 0 | 0 | 623 | 678 | 1094 | 1953 | 10278 |
| Estimated Infiltration (m³/month) | 0 | 0 | 820 | 1352 | 390 | 0 | 0 | 0 | 935 | 1017 | 1641 | 0 | 6155 |
| Pasture and Shrubs | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 115.6 | 90.5 | 56.3 | 30.5 | 16.0 | 10.0 | 570.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -32.9 | -7.6 | 46.7 | 50.8 | 82.0 | 58.6 | 441.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 49.2 | 13.5 | 3.9 | 0.0 | 0.0 | 0.0 | 9.3 | 10.2 | 16.4 | 58.6 | 246.6 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 32.8 | 54.1 | 15.6 | 0.0 | 0.0 | 0.0 | 37.4 | 40.6 | 65.6 | 0.0 | 246.1 |
| Estimated Actual Evapotranspiration (m³/month) | 130 | 157 | 295 | 559 | 1023 | 1493 | 1682 | 1317 | 819 | 444 | 233 | 146 | 8298 |
| Estimated Runoff (m³/month) | 532 | 714 | 716 | 197 | 57 | 0 | 0 | 0 | 136 | 148 | 239 | 852 | 3589 |
| Estimated Infiltration (m³/month) | 0 | 0 | 477 | 787 | 227 | 0 | 0 | 0 | 544 | 591 | 955 | 0 | 3581 |
| AREA B TOTALS | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 638 | 775 | 1456 | 2754 | 5041 | 7358 | 8202 | 6396 | 4037 | 2187 | 1147 | 717 | 40709 |
| Estimated Runoff (m³/month) | 2619 | 3518 | 3940 | 1649 | 476 | 0 | 0 | 0 | 1139 | 1239 | 2000 | 4199 | 20779 |
| Estimated Infiltration (m³/month) | 0 | 0 | 1940 | 3198 | 923 | 0 | 0 | 0 | 2210 | 2404 | 3880 | 0 | 14554 |
| · · · · | | | | | | | | | | | | | |



| AREA C - Drains to the Southeast (Ida Street) | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | | ling Capacity nm) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|------------|-------|----------------------|------------------------|------------------------|------------------------|--------------------|------|-------|
| Urban Lawn/Grassed Area | a 0 | 18,802 | 21,368 | Sandy Loam | В | 7 | 75 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Mature Fores | t 0 | 2,566 | | Sandy Loam | В | 3 | 00 | 0.7 | | | | | |
| | | | | | | | | | | | | | |
| Urban Lawn/Grassed Area | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 167 | 203 | 382 | 722 | 1322 | 1929 | 2111 | 1632 | 1059 | 573 | 301 | 188 | 10589 |
| Estimated Runoff (m³/month) | 687 | 922 | 1079 | 508 | 147 | 0 | 0 | 0 | 351 | 382 | 617 | 1101 | 5794 |
| Estimated Infiltration (m³/month) | 0 | 0 | 462 | 762 | 220 | 0 | 0 | 0 | 527 | 573 | 925 | 0 | 3470 |
| Mature Forest | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 117.2 | 92.6 | 56.3 | 30.5 | 16.0 | 10.0 | 573.9 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -34.5 | -9.7 | 46.7 | 50.8 | 82.0 | 58.6 | 437.6 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 53.3 | 20.3 | 5.9 | 0.0 | 0.0 | 0.0 | 14.0 | 15.2 | 24.6 | 58.6 | 277.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 28.7 | 47.3 | 13.7 | 0.0 | 0.0 | 0.0 | 32.7 | 35.6 | 57.4 | 0.0 | 215.3 |
| Estimated Actual Evapotranspiration (m ³ /month) | 23 | 28 | 52 | 99 | 180 | 263 | 301 | 238 | 144 | 78 | 41 | 26 | 1472 |
| Estimated Runoff (m³/month) | 94 | 126 | 137 | 52 | 15 | 0 | 0 | 0 | 36 | 39 | 63 | 150 | 712 |
| Estimated Infiltration (m³/month) | 0 | 0 | 74 | 121 | 35 | 0 | 0 | 0 | 84 | 91 | 147 | 0 | 552 |
| | | | | | | | | | | | | | |
| AREA C TOTALS | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m ³ /month) | 190 | 231 | 434 | 821 | 1502 | 2192 | 2412 | 1870 | 1203 | 652 | 342 | 214 | 12062 |
| Estimated Runoff (m³/month) | 780 | 1048 | 1216 | 560 | 162 | 0 | 0 | 0 | 387 | 421 | 680 | 1251 | 6506 |
| Estimated Infiltration (m³/month) | 0 | 0 | 536 | 884 | 255 | 0 | 0 | 0 | 611 | 664 | 1072 | 0 | 4022 |
| ,, | | | | - 55. | | | - | | | | | | |



| AREA D - Drains to the Southwest (into the Sandusky Drain) | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | | ding Capacity nm) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|------------|-------|----------------------|------------------------|------------------------|------------------------|--------------------|------|-------|
| Agricultural Land | 3473.9 | 143,421 | 169,611 | Sandy Loam | В | 1 | 150 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Urban Lawn/Grassed Area | 0 | 22,716 | | Sandy Loam | В | | 75 | 0.6 | | | | | |
| Agricultural Land | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 115.6 | 90.5 | 56.3 | 30.5 | 16.0 | 10.0 | 570.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -32.9 | -7.6 | 46.7 | 50.8 | 82.0 | 58.6 | 441.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 1276 | 1549 | 2911 | 5507 | 10083 | 14715 | 16580 | 12980 | 8075 | 4374 | 2295 | 1434 | 81779 |
| Estimated Runoff (m³/month) | 5239 | 7036 | 8231 | 3877 | 1119 | 0 | 0 | 0 | 2679 | 2914 | 4704 | 8398 | 44196 |
| Estimated Infiltration (m³/month) | 0 | 0 | 3527 | 5816 | 1678 | 0 | 0 | 0 | 4019 | 4371 | 7056 | 0 | 26467 |
| Urban Lawn/Grassed Area | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 202 | 245 | 461 | 872 | 1597 | 2331 | 2551 | 1972 | 1279 | 693 | 363 | 227 | 12793 |
| Estimated Runoff (m³/month) | 830 | 1114 | 1304 | 614 | 177 | 0 | 0 | 0 | 424 | 462 | 745 | 1330 | 7000 |
| Estimated Infiltration (m³/month) | 0 | 0 | 559 | 921 | 266 | 0 | 0 | 0 | 636 | 692 | 1118 | 0 | 4192 |
| Impervious | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.2 | 10.8 | 18.4 | 19.1 | 16.2 | 16.5 | 14.9 | 14.9 | 18.5 | 14.6 | 17.6 | 12.3 | 182.1 |
| Surplus (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Runoff (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Estimated Actual Evapotranspiration (m ³ /month) | 28 | 37 | 64 | 66 | 56 | 57 | 52 | 52 | 64 | 51 | 61 | 43 | 632 |
| Estimated Runoff (m³/month) | 129 | 171 | 291 | 302 | 256 | 261 | 236 | 236 | 293 | 232 | 279 | 195 | 2881 |
| Estimated Infiltration (m³/month) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AREA D TOTALS | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 1507 | 1832 | 3437 | CAAC | 11736 | 17103 | 19182 | 15003 | 9418 | F110 | 2719 | 1704 | 05305 |
| Estimated Actual Evapotranspiration (m /month) Estimated Runoff (m³/month) | | | | 6446 | | | | | | 5118 | | | 95205 |
| Estimated Runoff (m /month) Estimated Infiltration (m ³ /month) | 6198 | 8321 | 9826 | 4793 | 1552 | 261 | 236 | 236 | 3397 | 3607 | 5728 | 9923 | 54078 |
| Estimated minitration (in /month) | 0 | 0 | 4086 | 6737 | 1944 | 0 | 0 | 0 | 4655 | 5064 | 8174 | 0 | 30660 |
| | | | | | | | | | | | | | |



TABLE K2 - POST-DEVELOPMENT WATER BALANCE CALCULATIONS

| Drainage to the Sandusky Drain Blocks 201-208a | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | Water Hold (m | ing Capacity m) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|------------|------------------|--------------------|------------------------|------------------------|------------------------|--------------------|------|--------|
| Low-Medium Density | | | | | | | | | | | | | |
| (Urban Lawn) Open Space/Wetland A and Sandusky Drair | | 34,178 | 124,600 | Sandy Loam | В | 7 | '5 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| (Pasture and Shrubs) | 9128 | 36,512 | | Sand | Α | 10 | 00 | 0.8 | | | | | |
| | | | | | | | | | | | | | |
| | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | ОСТ | NOV | DEC | Totals |
| Average Temperature (°C) | -5.6 | -4.5 | -0.1 | 6.8 | 13.1 | 18.3 | 20.8 | 19.7 | 15.5 | 9.2 | 3.4 | -2.6 | |
| Total Precipitation (mm/month) | 74.2 | 65.5 | 71.5 | 83.4 | 89.8 | 91.7 | 82.7 | 82.9 | 103.0 | 81.3 | 98.0 | 87.5 | 1011.5 |
| Precipitation as rain (mm/month) | 24.5 | 27.1 | 53.2 | 83.4 | 89.8 | 91.7 | 82.7 | 82.9 | 103.0 | 81.3 | 98.0 | 48.7 | |
| Precipitation as snow (mm/month) | 49.7 | 38.4 | 18.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 38.8 | |
| Potential Snow Melt (mm/month) | 20.9 | 32.8 | 49.1 | 26.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 19.9 | |
| Actual Snow Melt (mm/month) | 20.9 | 32.8 | 49.1 | 22.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 19.9 | |
| Snow Storage (mm/month) | 47.7 | 53.4 | 22.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 18.9 | |
| Louis Adadissas Danaitas (Unbara Laures) | | | | | | | | | | | | | |
| Low-Medium Density (Urban Lawn) | 0.0 | 10.0 | 20.2 | 20.4 | 70.2 | 102.6 | 442.2 | 06.0 | F.C. 2 | 20.5 | 46.0 | 10.0 | F.C. 2 |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m³/month) | 304 | 369 | 694 | 1312 | 2403 | 3507 | 3838 | 2967 | 1924 | 1042 | 547 | 342 | 19249 |
| Estimated Runoff (m³/month) | 1248 | 1677 | 1961 | 924 | 267 | 0 | 0 | 0 | 638 | 694 | 1121 | 2001 | 10532 |
| Estimated Infiltration (m³/month) | 0 | 0 | 841 | 1386 | 400 | 0 | 0 | 0 | 958 | 1042 | 1682 | 0 | 6307 |
| Open Space/Wetland A and Sandusky Drain (Pasture and Shrubs) | | | | | | | | | | | | | |
| • | 8.0 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 114.0 | 00.6 | FC 2 | 20 F | 16.0 | 10.0 | 566.7 |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | | | | | | 114.0 | 88.6 | 56.3 | 30.5 | 16.0 | 10.0 | |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -31.3 | -5.7 | 46.7 | 50.8 | 82.0 | 58.6 | 444.8 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 49.2 | 13.5 | 3.9 | 0.0 | 0.0 | 0.0 | 9.3 | 10.2 | 16.4 | 58.6 | 246.6 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 32.8 | 54.1 | 15.6 | 0.0 | 0.0 | 0.0 | 37.4 | 40.6 | 65.6 | 0.0 | 246.1 |
| Estimated Actual Evapotranspiration (m³/month) | 325 | 394 | 741 | 1402 | 2567 | 3746 | 4162 | 3235 | 2056 | 1114 | 584 | 365 | 20691 |
| Estimated Runoff (m³/month) | 1334 | 1791 | 1796 | 494 | 142 | 0 | 0 | 0 | 341 | 371 | 599 | 2138 | 9005 |
| Estimated Infiltration (m³/month) | 0 | 0 | 1197 | 1974 | 570 | 0 | 0 | 0 | 1364 | 1484 | 2395 | 0 | 8984 |
| Impervious Areas | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.2 | 10.8 | 18.4 | 19.1 | 16.2 | 16.5 | 14.9 | 14.9 | 18.5 | 14.6 | 17.6 | 12.3 | 182.1 |
| Surplus (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Runoff (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Estimated Actual Evapotranspiration (m³/month) | 441 | 581 | 993 | 1028 | 871 | 890 | 803 | 804 | 999 | 789 | 951 | 665 | 9815 |
| Estimated Runoff (m³/month) | 2008 | 2646 | 4522 | 4685 | 3970 | 4054 | 3656 | 3665 | 4553 | 3594 | 4332 | 3030 | 44715 |
| Estimated Infiltration (m³/month) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL (Blocks 201-208a) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 1070 | 1344 | 2428 | 3743 | 5841 | 8143 | 8803 | 7006 | 4979 | 2945 | 2082 | 1372 | 49756 |
| | | | | | | | | | | | | | |
| Estimated Runoff (m³/month) | 4590 | 6114 | 8279 | 6102 | 4379 | 4054 | 3656 | 3665 | 5533 | 4659 | 6052 | 7170 | 64252 |



| Drainage to Wetland C Blocks A210 and A212 | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | | ing Capacity m) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|------------|-------|--------------------|------------------------|------------------------|------------------------|--------------------|------|-------|
| Low Densit (Urban Lawn | • | 17,318 | 55,700 | Sandy Loam | В | 7 | '5 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Open Space (Pasture and Shrubs | | 20,432 | | Sandy Loam | В | 1 | 50 | 0.8 | | | | | |
| Low Density (Urban Lawn) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 154 | 187 | 352 | 665 | 1217 | 1777 | 1945 | 1503 | 975 | 528 | 277 | 173 | 9753 |
| Estimated Runoff (m³/month) | 633 | 850 | 994 | 468 | 135 | 0 | 0 | 0 | 324 | 352 | 568 | 1014 | 5337 |
| Estimated Infiltration (m ³ /month) | 0 | 0 | 426 | 702 | 203 | 0 | 0 | 0 | 485 | 528 | 852 | 0 | 3196 |
| Open Space/Wetland C (Pasture and Shrubs) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 115.6 | 90.5 | 56.3 | 30.5 | 16.0 | 10.0 | 570.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -32.9 | -7.6 | 46.7 | 50.8 | 82.0 | 58.6 | 441.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 49.2 | 13.5 | 3.9 | 0.0 | 0.0 | 0.0 | 9.3 | 10.2 | 16.4 | 58.6 | 246.6 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 32.8 | 54.1 | 15.6 | 0.0 | 0.0 | 0.0 | 37.4 | 40.6 | 65.6 | 0.0 | 246.1 |
| Estimated Actual Evapotranspiration (m ³ /month) | 182 | 221 | 415 | 785 | 1436 | 2096 | 2362 | 1849 | 1150 | 623 | 327 | 204 | 11650 |
| Estimated Runoff (m ³ /month) | 746 | 1002 | 1005 | 276 | 80 | 0 | 0 | 0 | 191 | 208 | 335 | 1196 | 5039 |
| Estimated Infiltration (m ³ /month) | 0 | 0 | 670 | 1105 | 319 | 0 | 0 | 0 | 763 | 830 | 1340 | 0 | 5027 |
| Impervious Areas | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.2 | 10.8 | 18.4 | 19.1 | 16.2 | 16.5 | 14.9 | 14.9 | 18.5 | 14.6 | 17.6 | 12.3 | 182.1 |
| Surplus (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Runoff (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Estimated Actual Evapotranspiration (m³/month) | 147 | 193 | 330 | 342 | 290 | 296 | 267 | 268 | 333 | 263 | 317 | 221 | 3268 |
| Estimated Runoff (m³/month) | 669 | 881 | 1506 | 1560 | 1322 | 1350 | 1217 | 1220 | 1516 | 1197 | 1442 | 1009 | 14888 |
| Estimated Infiltration (m ³ /month) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL (Blocks A210 and A212) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 483 | 601 | 1097 | 1792 | 2944 | 4169 | 4574 | 3620 | 2458 | 1414 | 921 | 599 | 24672 |
| Estimated Runoff (m ³ /month) | 2047 | 2733 | 3504 | 2304 | 1537 | 1350 | 1217 | 1220 | 2030 | 1756 | 2346 | 3219 | 25264 |
| Estimated Infiltration (m³/month) | 0 | 0 | 1096 | 1807 | 521 | 0 | 0 | 0 | 1249 | 1358 | 2192 | 0 | 8223 |
| | | | | | | | | | | | | | |



| Drainage to the southeast (Ida Street) Block A211 Low Density | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | Water Hold (m | ing Capacity m) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|--|---|--|---|--|---|---|---|---|---|---|---|--|
| (Urban Lawn) | | 2,430 | 5,400 | Sandy Loam | В | 7 | '5 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Low Density (Urban Lawn) Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) Estimated Runoff (mm/month) Estimated Infiltration (mm/month) | 36.5 36.5 0.0 | 49.1 49.1 0.0 | 82.0 57.4 24.6 | 67.6 27.0 40.5 | 19.5 7.8 11.7 | -10.9 0.0 0.0 | -29.6 0.0 0.0 | -3.9 0.0 0.0 | 46.7 18.7 28.0 | 50.8 20.3 30.5 | 82.0 32.8 49.2 | 58.6 58.6 0.0 | 448.3 308.2 184.5 |
| Estimated Inflitration (Infl/Information (m³/month) Estimated Runoff (m³/month) Estimated Infiltration (m³/month) | 22 89 0 | 26 119 0 | 49 139 60 | 93 66 99 | 171 19 28 | 249 0 0 | 273 0 0 | 211 0 0 | 137 45 68 | 74 49 74 | 39 80 120 | 24 142 0 | 1369 749 448 |
| Impervious Areas Estimated Actual Evapotranspiration (mm/month) Surplus (mm/month) Estimated Runoff (mm/month) Estimated Infiltration (mm/month) Estimated Actual Evapotranspiration (m³/month) Estimated Runoff (m³/month) Estimated Infiltration (m³/month) | 8.2 37.2 37.2 0.0 24 111 0 | 10.8 49.1 49.1 0.0 32 146 0 | 18.4 83.9 83.9 0.0 55 249 | 19.1 86.9 86.9 0.0 57 258 0 | 16.2 73.6 73.6 0.0 48 219 | 16.5 75.2 75.2 0.0 49 223 0 | 14.9 67.8 67.8 0.0 44 201 0 | 14.9 68.0 68.0 0.0 44 202 0 | 18.5 84.5 84.5 0.0 55 251 0 | 14.6 66.7 66.7 0.0 43 198 0 | 17.6 80.4 80.4 0.0 52 239 0 | 12.3 56.2 56.2 0.0 37 167 0 | 182.1 829.4 829.4 0.0 541 2463 0 |
| TOTAL (Block A211) Estimated Actual Evapotranspiration (m³/month) Estimated Runoff (m³/month) Estimated Infiltration (m²/month) | 46 199 0 | 58 265 0 | 104 389 60 | 150 324 99 | 219 238 28 | 298 223 0 | 317 201 0 | 255 202 0 | 192 296 68 | 118 247 74 | 91 318 120 | 61 309 0 | 1909 3212 448 |



| Drainage to North SWMF | Impervious | Pervious | Total Area | | | Mateu Held | ing Capacity | Infiltration | | | Meltmax | | |
|---|------------|------------|-------------------|------------|------------|------------|--------------|--------------|------------------------|------------------------|---------|------|-------|
| Block A209 | Area (m²) | Area (m²) | (m ²) | Soil Type | Soil Group | | m) | Factor | T _{rain} (°C) | T _{snow} (°C) | (%/100) | | |
| Medium-Low Densit | | / u cu (/ | ··· / | | | • | • | | | | (, , | | |
| (Urban Lawı | 12,526 | 6,745 | 25,900 | Sandy Loam | В | 7 | '5 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| SWM Facility (North | n) 3,713 | 2,917 | | Sandy Loam | В | 7 | '5 | 0.6 | | | | | |
| Medium-Low Density (Urban Lawn) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 60 | 73 | 137 | 259 | 474 | 692 | 757 | 585 | 380 | 206 | 108 | 67 | 3799 |
| Estimated Runoff (m³/month) | 246 | 331 | 387 | 182 | 53 | 0 | 0 | 0 | 126 | 137 | 221 | 395 | 2078 |
| Estimated Infiltration (m³/month) | 0 | 0 | 166 | 273 | 79 | 0 | 0 | 0 | 189 | 206 | 332 | 0 | 1245 |
| SWM Facility (North) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 26 | 32 | 59 | 112 | 205 | 299 | 328 | 253 | 164 | 89 | 47 | 29 | 1643 |
| Estimated Runoff (m³/month) | 107 | 143 | 167 | 79 | 23 | 0 | 0 | 0 | 54 | 59 | 96 | 171 | 899 |
| Estimated Infiltration (m³/month) | 0 | 0 | 72 | 118 | 34 | 0 | 0 | 0 | 82 | 89 | 144 | 0 | 538 |
| Impervious Areas | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.2 | 10.8 | 18.4 | 19.1 | 16.2 | 16.5 | 14.9 | 14.9 | 18.5 | 14.6 | 17.6 | 12.3 | 182.1 |
| Surplus (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Runoff (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Estimated Actual Evapotranspiration (m ³ /month) | 133 | 175 | 299 | 310 | 262 | 268 | 242 | 242 | 301 | 238 | 286 | 200 | 2957 |
| Estimated Runoff (m³/month) | 605 | 797 | 1362 | 1411 | 1196 | 1221 | 1101 | 1104 | 1371 | 1083 | 1305 | 913 | 13469 |
| Estimated Infiltration (m³/month) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL (Block A209) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 219 | 279 | 495 | 681 | 942 | 1259 | 1327 | 1081 | 845 | 532 | 441 | 297 | 8398 |
| Estimated Runoff (m³/month) | 958 | 1271 | 1916 | 1672 | 1271 | 1221 | 1101 | 1104 | 1552 | 1279 | 1622 | 1479 | 16446 |
| Estimated Infiltration (m³/month) | 0 | 0 | 238 | 392 | 113 | 0 | 0 | 0 | 271 | 294 | 475 | 0 | 1783 |
| | | | | | | | | | | | | | |



| Drainage to South SWMF Block A208b | Impervious Area (m²) | Pervious Area (m²) | Total Area (m²) | Soil Type | Soil Group | | ling Capacity nm) | Infiltration Factor | T _{rain} (°C) | T _{snow} (°C) | Meltmax (%/100) | | |
|---|-------------------------|-----------------------|--------------------|------------|------------|--------------|----------------------|------------------------|------------------------|------------------------|--------------------|-------|--------|
| Low-Medium De | • | 70.076 | | | | _ | | 0.5 | | 40.0 | 0.00 | | |
| (Urban Li | . , | 78,076 | 241,500 | Sandy Loam | В | | 75 | 0.6 | 3.3 | -10.0 | 0.92 | | |
| Park/Open S | , , , | 16,088 | | Sandy Loam | B B | | 75 75 | 0.6 0.6 | | | | | |
| SWM Facility (Sc | outh) 13,121 | 10,309 | | Sandy Loam | В | • | /5 | 0.6 | | | | | |
| Low-Medium Density (Urban Lawn) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m ³ /month) | 695 | 843 | 1585 | 2998 | 5489 | 8011 | 8768 | 6777 | 4396 | 2381 | 1249 | 781 | 43972 |
| Estimated Runoff (m³/month) | 2852 | 3830 | 4481 | 2111 | 609 | 0 | 0 | 0 | 1458 | 1587 | 2561 | 4572 | 24060 |
| Estimated Infiltration (m ³ /month) | 0 | 0 | 1920 | 3166 | 913 | 0 | 0 | 0 | 2188 | 2380 | 3841 | 0 | 14408 |
| Park/Open Space | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m³/month) | 143 | 174 | 327 | 618 | 1131 | 1651 | 1807 | 1396 | 906 | 491 | 257 | 161 | 9061 |
| Estimated Runoff (m³/month) | 588 | 789 | 923 | 435 | 125 | 0 | 0 | 0 | 301 | 327 | 528 | 942 | 4958 |
| Estimated Infiltration (m³/month) | 0 | 0 | 396 | 652 | 188 | 0 | 0 | 0 | 451 | 490 | 792 | 0 | 2969 |
| SWM Facility (South) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.9 | 10.8 | 20.3 | 38.4 | 70.3 | 102.6 | 112.3 | 86.8 | 56.3 | 30.5 | 16.0 | 10.0 | 563.2 |
| Surplus (mm/month) | 36.5 | 49.1 | 82.0 | 67.6 | 19.5 | -10.9 | -29.6 | -3.9 | 46.7 | 50.8 | 82.0 | 58.6 | 448.3 |
| Estimated Runoff (mm/month) | 36.5 | 49.1 | 57.4 | 27.0 | 7.8 | 0.0 | 0.0 | 0.0 | 18.7 | 20.3 | 32.8 | 58.6 | 308.2 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 24.6 | 40.5 | 11.7 | 0.0 | 0.0 | 0.0 | 28.0 | 30.5 | 49.2 | 0.0 | 184.5 |
| Estimated Actual Evapotranspiration (m³/month) | 92 | 111 | 209 | 396 | 725 | 1058 | 1158 | 895 | 580 | 314 | 165 | 103 | 5806 |
| Estimated Runoff (m³/month) | 377 | 506 | 592 | 279 | 80 | 0 | 0 | 0 | 193 | 209 | 338 | 604 | 3177 |
| Estimated Infiltration (m³/month) | 0 | 0 | 254 | 418 | 121 | 0 | 0 | 0 | 289 | 314 | 507 | 0 | 1902 |
| Impervious Areas | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (mm/month) | 8.2 | 10.8 | 18.4 | 19.1 | 16.2 | 16.5 | 14.9 | 14.9 | 18.5 | 14.6 | 17.6 | 12.3 | 182.1 |
| Surplus (mm/month) | 8.2 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Runoff (mm/month) | 37.2 | 49.1 | 83.9 | 86.9 | 73.6 | 75.2 75.2 | 67.8 | 68.0 | 84.5 | 66.7 | 80.4 | 56.2 | 829.4 |
| Estimated Infiltration (mm/month) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Estimated Actual Evapotranspiration (m³/month) | 1120 | 1476 | 2523 | 2614 | 2215 | 2262 | 2040 | 2045 | 2540 | 2005 | 2417 | 1691 | 24948 |
| Estimated Runoff (m³/month) | 5104 | 6726 | 11493 | 11908 | 10090 | 10304 | 9292 | 9315 | 11573 | 9135 | 11011 | 7703 | 113654 |
| Estimated Infiltration (m³/month) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | |
| TOTAL (Block A208b) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 2050 | 2605 | 4644 | 6626 | 9559 | 12981 | 13772 | 11113 | 8422 | 5192 | 4089 | 2736 | 83788 |
| Estimated Runoff (m³/month) | 8920 | 11851 | 17488 | 14732 | 10905 | 10304 | 9292 | 9315 | 13525 | 11258 | 14438 | 13820 | 145848 |
| Estimated Infiltration (m³/month) | 0 | 0 | 2570 | 4236 | 1222 | 0 | 0 | 0 | 2927 | 3184 | 5140 | 0 | 19280 |
| | | | | | | | | | | | | | |

Project Name: Hunter Farm
Project Number: LON-21008138-A0
Client: Auburn Developments



TABLE K3 - WATER BALANCE SUMMARY

DRAINAGE TO THE SANDUSKY DRAIN:

| AREA A TOTALS (Pre-Development) | | | | | | | | | | | | | |
|--|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|
| Estimated Actual Evapotranspiration (m³/month) | 1691 | 2056 | 3855 | 7206 | 13090 | 19066 | 21346 | 16684 | 10514 | 5721 | 3055 | 1917 | 106201 |
| Estimated Runoff (m³/month) | 6959 | 9341 | 10489 | 4514 | 1568 | 411 | 370 | 371 | 3252 | 3400 | 5340 | 11136 | 57150 |
| Estimated Infiltration (m³/month) | 0 | 0 | 5131 | 8460 | 2441 | 0 | 0 | 0 | 5846 | 6359 | 10265 | 0 | 38502 |
| | | | | | | | | | | | | | |
| AREA D TOTALS (Pre-Development) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m3/month) | 1507 | 1832 | 3437 | 6446 | 11736 | 17103 | 19182 | 15003 | 9418 | 5118 | 2719 | 1704 | 95205 |
| Estimated Runoff (m3/month) | 6198 | 8321 | 9826 | 4793 | 1552 | 261 | 236 | 236 | 3397 | 3607 | 5728 | 9923 | 54078 |
| Estimated Infiltration (m3/month) | 0 | 0 | 4086 | 6737 | 1944 | 0 | 0 | 0 | 4655 | 5064 | 8174 | 0 | 30660 |
| | | | | | | | | | | | | | |
| TOTAL Blocks 201-208a (Post-Development) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m3/month) | 1070 | 1344 | 2428 | 3743 | 5841 | 8143 | 8803 | 7006 | 4979 | 2945 | 2082 | 1372 | 49756 |
| Estimated Runoff (m3/month) | 4590 | 6114 | 8279 | 6102 | 4379 | 4054 | 3656 | 3665 | 5533 | 4659 | 6052 | 7170 | 64252 |
| Estimated Infiltration (m3/month) | 0 | 0 | 2038 | 3360 | 969 | 0 | 0 | 0 | 2322 | 2526 | 4077 | 0 | 15291 |
| | | | | | | | | | | | | | |
| TOTAL Block A208b (Post-Development) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 2050 | 2605 | 4644 | 6626 | 9559 | 12981 | 13772 | 11113 | 8422 | 5192 | 4089 | 2736 | 83788 |
| Estimated Runoff (m³/month) | 8920 | 11851 | 17488 | 14732 | 10905 | 10304 | 9292 | 9315 | 13525 | 11258 | 14438 | 13820 | 145848 |
| Estimated Infiltration (m³/month) | 0 | 0 | 2570 | 4236 | 1222 | 0 | 0 | 0 | 2927 | 3184 | 5140 | 0 | 19280 |
| | | | | | | | | | | | | | |
| TOTAL Block A209 (Post-Development) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 219 | 279 | 495 | 681 | 942 | 1259 | 1327 | 1081 | 845 | 532 | 441 | 297 | 8398 |
| Estimated Runoff (m³/month) | 958 | 1271 | 1916 | 1672 | 1271 | 1221 | 1101 | 1104 | 1552 | 1279 | 1622 | 1479 | 16446 |
| Estimated Infiltration (m³/month) | 0 | 0 | 238 | 392 | 113 | 0 | 0 | 0 | 271 | 294 | 475 | 0 | 1783 |

| Drainage to the Sandusky Drain (PRE VS. POST) | PRE | POST | VOL CHANGE | % Difference | Post with Mitigation | % Difference with Mitigation |
|--|---------|---------|---------------|-----------------|-------------------------|------------------------------|
| Estimated Runoff (m3/year) | 111,228 | 226,546 | 115,318 | 204% | 135,928 | 122% |
| Estimated Infiltration (m3/year) | 69,161 | 36,354 | (32,807) | 53% | 55,384 | 80% |
| With Mitigation: | | | | | | |
| Estimated Runoff | m³/year | 135928 | | | | |
| Estimated Infiltration | m³/year | 55384 | | | | |
| Runoff reduction | | 0.4 | | | | |
| Effectiveness | | 0.21 | | | | |

Monthly Water Balance - Summary Tables

Project Name: Hunter Farm
Project Number: LON-21008138-A0
Client: Auburn Developments



DRAINAGE TO WETLAND C:

| AREA B TOTALS (Pre- Development) | | | | | | | | | | | | | |
|--|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| Estimated Actual Evapotranspiration (m3/month) | 638 | 775 | 1456 | 2754 | 5041 | 7358 | 8202 | 6396 | 4037 | 2187 | 1147 | 717 | 40709 |
| Estimated Runoff (m3/month) | 2619 | 3518 | 3940 | 1649 | 476 | 0 | 0 | 0 | 1139 | 1239 | 2000 | 4199 | 20779 |
| Estimated Infiltration (m3/month) | 0 | 0 | 1940 | 3198 | 923 | 0 | 0 | 0 | 2210 | 2404 | 3880 | 0 | 14554 |
| | | | | | | | | | | | | | |
| TOTAL Blocks A210 and A212 (Post Development) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m3/month) | 483 | 601 | 1097 | 1792 | 2944 | 4169 | 4574 | 3620 | 2458 | 1414 | 921 | 599 | 24672 |
| Estimated Runoff (m3/month) | 2047 | 2733 | 3504 | 2304 | 1537 | 1350 | 1217 | 1220 | 2030 | 1756 | 2346 | 3219 | 25264 |
| Estimated Infiltration (m3/month) | 0 | 0 | 1096 | 1807 | 521 | 0 | 0 | 0 | 1249 | 1358 | 2192 | 0 | 8223 |

| Drainage to Wetland C (PRE VS. POST) | PRE | POST | VOL CHANGE | % Difference | Post with Mitigation | % Difference with Mitigation |
|---|---------|--------|---------------|-----------------|-------------------------|------------------------------|
| Estimated Runoff (m3/year) | 20,779 | 25,264 | 4,485 | 122% | 10,106 | 49% |
| Estimated Infiltration (m3/year) | 14,554 | 8,223 | (6,331) | 57% | 11,710 | 80% |
| With Mitigation: | | | | | | |
| Estimated Runoff | m³/year | 10106 | | | | |
| Estimated Infiltration | m³/year | 11710 | | | | |
| Runoff reduction | | 0.6 | | | | |
| Effectiveness | | 0.23 | | | | |

Monthly Water Balance - Summary Tables

Project Name: Hunter Farm
Project Number: LON-21008138-A0
Client: Auburn Developments



DRAINAGE TO THE SOUTHEAST:

| AREA C TOTALS (Pre-Development) | | | | | | | | | | | | | |
|--|-----|------|------|-----|------|------|------|------|------|-----|------|------|-------|
| Estimated Actual Evapotranspiration (m3/month) | 190 | 231 | 434 | 821 | 1502 | 2192 | 2412 | 1870 | 1203 | 652 | 342 | 214 | 12062 |
| Estimated Runoff (m3/month) | 780 | 1048 | 1216 | 560 | 162 | 0 | 0 | 0 | 387 | 421 | 680 | 1251 | 6506 |
| Estimated Infiltration (m3/month) | 0 | 0 | 536 | 884 | 255 | 0 | 0 | 0 | 611 | 664 | 1072 | 0 | 4022 |
| | | | | | | | | | | | | | |
| TOTAL Block A211 (Post-Development) | | | | | | | | | | | | | |
| Estimated Actual Evapotranspiration (m³/month) | 46 | 58 | 104 | 150 | 219 | 298 | 317 | 255 | 192 | 118 | 91 | 61 | 1909 |
| Estimated Runoff (m³/month) | 199 | 265 | 389 | 324 | 238 | 223 | 201 | 202 | 296 | 247 | 318 | 309 | 3212 |
| Estimated Infiltration (m³/month) | 0 | 0 | 60 | 99 | 28 | 0 | 0 | 0 | 68 | 74 | 120 | 0 | 448 |

| Area C (PRE VS. POST) | PRE | POST | VOL CHANGE | % CHANGE | % of Pre- Dev Conditions |
|----------------------------------|------|------|---------------|----------|--------------------------------|
| Estimated Runoff (m3/year) | 6506 | 3212 | -3294 | -51% | 49% |
| Estimated Infiltration (m3/year) | 4022 | 448 | -3574 | -89% | 11% |

| Drainage to the Southeast (Ida Street) (PRE VS. POST) ¹ | PRE | POST | VOL CHANGE | % Difference | Post with Mitigation | % Difference with Mitigation |
|---|---------|-------|---------------|-----------------|-------------------------|---------------------------------------|
| Estimated Runoff (m3/year) | 6,506 | 3,212 | (3,294) | 49% | 128 | 2% |
| Estimated Infiltration (m3/year) | 4,022 | 448 | (3,574) | 11% | 3,224 | 80% |
| With Mitigation: | | | | | | |
| Estimated Runoff | m³/year | 128 | | | | |
| Estimated Infiltration | m³/year | 3224 | | | | |
| Runoff reduction | | 0.96 | | | | |
| Effectiveness | | 0.9 | | | | |

Notes:

^{1.} Runoff and infiltration in the drainage area to the southeast (Ida Street) are significantly different due to a smaller drainage area in the post development.

Monthly Water Balance

Project Name: Hunter Farm
Project Number: LON-21008138-A0
Client: Auburn Developments



TABLE K4 - WATER BALANCE ASSUMPTIONS

- 1. AET occurs year round. Although the average temperature is below 0°C in the winter months, fluctuation above and below the freezing temperature of water occurs. The Thornthwaite model used assumes Train = 3.3°C and Tsnow = -10.0°C. When the average monthly temperature falls between these values, the monthly precipitation as rain and snow is derived by assuming a linear interpolation between these values, consistent with the methodology used in the accepted USGS reference material (McCabe, G.J., and Markstrom, S.L., 2007, A monthly water-balance model driven by a graphical use interface: U.S. Geological Survey Open-File report 2007-1088, 6 p.). Values of AET were taken from the Thornthwaite model and are considered to be representative of actual site conditions.
- 2. Monthly surplus is calculated by summing the precipitation as rain and actual snow melt, less estimated evapotranspiration.
- 3. Negative surplus values can be achieved during the summer months as water storage is the vadose zone of the soil is subject to evapotranspiration and depleted.
- 4. Infiltration is assumed not to occur between December and February as frost is typically present throughout those months.
- 5. Infiltration in March (Average temperature of -0.1°C), is assumed to occur during half of the month.
- No net infiltration or runoff occur in the summer as the rainfall accumulation is stored on site and infiltration was not assigned a negative value. See
 Assumption 3.
- 7. Evapotranspiration in impervious areas is the sum of precipitation as rain and snow melt multiplied by a factor of 0.18.
- 8. Under post development conditions, it is assumed that infiltration follows the new drainage pathways.
- 9. Forested areas west of Richmond Street and adjacent to Wetland C are assumed to be removed post-development.
- 10. Impervious areas are based on the Conceptual SWM Strategy the Site (Stantec, 2022)
- 11. Water holding capacity for SWM facilities is assumed to be 75mm.

| | | | | Direct | nt Duning a | ta Candu | du Dunin | | | | | SWM (wet) | SWM (dry) | Wetla | and C | Ida Chuanh |
|------------------|------|------|------|--------|-------------|-----------|-----------|-------|-------|------|-------|-----------|-----------|-------|--------|------------|
| | | | | Direc | ct Drainage | to Sandus | sky Drain | | | | | south | north | NE we | etland | Ida Street |
| Block | A201 | A202 | A203 | A204a | A204b | A205a | A205b | A206a | A206b | A207 | A208a | A208b | A209 | A210 | A212 | A211 |
| Total Area | 1.61 | 2.96 | 1.75 | 0.99 | 0.68 | 0.89 | 0.78 | 0.57 | 0.18 | 0.45 | 1.6 | 24.15 | 2.59 | 4.31 | 1.26 | 0.54 |
| Low Density | | | 1.75 | | | | | | | 0.45 | 0.37 | 10.79 | 0.155 | | 1.26 | 0.54 |
| Medium Density | 1.61 | | | | | 0.89 | | | | | 0.91 | 5.006 | 1.462 | | | |
| High Density | | | | | | | | | | | | | | | | |
| Park | | 2.96 | | | | | | 0.57 | 0.18 | | | 0.404 | | 1.276 | | |
| Open Space | | | | 0.99 | 0.68 | | | | | | 0.17 | 1.607 | | 2.554 | | |
| Street | | | | | | | 0.78 | | | | 0.15 | 4 | 0.31 | 0.48 | | |
| SWM Facility | | | | | | | | | | | • | 2.343 | 0.663 | | · | |
| Impervious Areas | 1.05 | 0.59 | 0.96 | 0.20 | 0.14 | 0.58 | 0.55 | 0.11 | 0.04 | 0.25 | 0.93 | 13.70 | 1.62 | 1.10 | 0.69 | 0.30 |
| Pervious Areas | 0.56 | 2.37 | 0.79 | 0.79 | 0.54 | 0.31 | 0.23 | 0.46 | 0.14 | 0.20 | 0.67 | 10.45 | 0.97 | 3.21 | 0.57 | 0.24 |

Post-Development Conditions:

| Sub-Catchment | Area (ha) | TIMP | AxC | XIMP | AxC | CN | AxCN | IA | AxIA | Description |
|-----------------|-----------|------|--------|------|-----------|----|----------|-------------|--------------|---|
| 201 | 1.61 | 0.65 | 1.047 | 0.55 | 0.886 | 61 | 98.210 | 5 | 8.050 | MD on the north of the west of Richmond part from the site. |
| 202 | 2.96 | 0.20 | 0.591 | 0.05 | 0.148 | 75 | 221.700 | 5 | 14.780 | Park block on west of Richmond |
| 203 | 1.76 | 0.55 | 0.968 | 0.45 | 0.792 | 61 | 107.360 | 5 | 8.800 | SF blocks on the south of the west of Richmond part from the site |
| 204a | 0.99 | 0.20 | 0.198 | 0.20 | 0.198 | 75 | 74.250 | 5 | 4.950 | Sandusky drain on west of Richmond |
| 204b | 0.68 | 0.20 | 0.136 | 0.20 | 0.136 | 75 | 51.000 | 5 | 3.400 | Sandusky drain on east of Richmond |
| 205a | 0.89 | 0.65 | 0.579 | 0.55 | 0.490 | 61 | 54.290 | 5 | 4.450 | MD between Sandusky drain and Richmond |
| 205b | 0.78 | 0.70 | 0.546 | 0.60 | 0.468 | 61 | 47.580 | 5 | 3.900 | Richmond street |
| 206a | 0.59 | 0.20 | 0.118 | 0.05 | 0.030 | 75 | 44.250 | 5 | 2.950 | West park block on south boundary of west of Richmond |
| 206b | 0.18 | 0.20 | 0.036 | 0.05 | 0.009 | 75 | 13.500 | 5 | 0.900 | East park block on the south boundary of west of Richmond |
| 207 | 0.45 | 0.65 | 0.293 | 0.55 | 0.248 | 61 | 27.450 | 5 | 2.250 | MD between Sandusky drain and Marion Street. |
| | | | | | | | | | | |
| 208a (MD) | 0.91 | 0.65 | 0.592 | 0.55 | 0.501 | 61 | 55.567 | 5 | 4.555 | - |
| 208a (SF) | 0.37 | 0.55 | 0.204 | 0.45 | 0.167 | 61 | 22.626 | 5 | 1.855 | - |
| 208a (Roads) | 0.15 | 0.70 | 0.105 | 0.60 | 0.090 | 61 | 9.150 | 5 | 0.750 | - |
| 208a (OS) | 0.17 | 0.20 | 0.034 | 0.05 | 0.009 | 61 | 10.412 | 5 | 0.853 | - |
| 208a (Weighted) | 1.60 | 0.58 | 0.935 | 0.48 | 0.766 | 61 | 97.754 | 5 | 8.013 | Proposed uncontrolled toward the Drain |
| | | | | | | | | | | |
| 208b (MD) | 4.21 | 0.65 | 2.737 | 0.55 | 2.316 | 61 | 256.810 | 5 | 21.050 | |
| 208b (SF) | 12.00 | 0.55 | 6.599 | 0.45 | 5.399 | 61 | 731.840 | 5 | 59.987 | - |
| 208b (Roads) | 4.00 | 0.70 | 2.798 | 0.60 | 2.399 | 61 | 243.849 | 5 | 19.988 | - |
| 208b (OS) | 3.95 | 0.20 | 0.790 | 0.05 | 0.198 | 61 | 240.950 | 5 | 19.750 | - |
| 208b (Weighted) | 24.15 | 0.54 | 12.92 | 0.43 | 10.31 | 61 | 1473.45 | 5 | 120.77 | Proposed site toward south SWMF toward Sandusky drain |
| | | | | | | | | | | |
| 209 (MD) | 1.56 | 0.65 | 1.017 | 0.55 | 0.860 | 61 | 95.404 | 5 | 7.820 | - |
| 209 (SF) | 0.25 | 0.55 | 0.138 | 0.45 | 0.113 | 61 | 15.250 | 5 | 1.250 | - |
| 209 (Roads) | 0.31 | 0.70 | 0.217 | 0.60 | 0.186 | 61 | 18.910 | 5 | 1.550 | - |
| 209 (OS) | 0.49 | 0.20 | 0.098 | 0.05 | 0.025 | 61 | 29.890 | 5 | 2.450 | - |
| 209 (Weighted) | 2.61 | 0.56 | 1.47 | 0.45 | 1.18 | 61 | 159.45 | 5 | 13.07 | Proposed site toward north SWMF toward Sandusky drain |
| | | | | | | | | | | |
| 210 (OS) | 2.20 | 0.20 | 0.440 | 0.05 | 0.110 | 75 | 164.850 | 10 | 21.980 | Undeveloped open space area |
| 210 (Roads) | 0.48 | 0.70 | 0.336 | 0.60 | 0.288 | 75 | 36.000 | 5 | 2.400 | - |
| 210 (Parks) | 1.58 | 0.20 | 0.315 | 0.05 | 0.079 | 75 | 118.200 | 5 | 7.880 | - |
| 210 (Weighted) | 4.25 | 0.26 | 1.09 | 0.11 | 0.48 | 75 | 319.05 | 8 | 32.26 | Proposed parks on northeast toward the north |
| | | | | | | | | | | |
| 211 | 0.54 | 0.55 | 0.297 | 0.45 | 0.243 | 61 | 32.940 | 5 | 2.700 | SF blocks on the southeast toward IDA Street |
| 212 | 1.26 | 0.55 | 0.693 | 0.45 | 0.567 | 75 | 94.500 | 5 | 6.300 | SF blocks on the northeast |
| | | | | | | | | | | |
| Total | 45.31 | 0.48 | 21.92 | 0.37 | 16.95 | 64 | 2916.74 | 5 | 237.55 | - |
| | | | | | | | | | | |
| Sub-Catchment | Area (ha) | С | AxC | CN | AxC | IA | AxIA | | | Description |
| EXT-1 | 19.09 | 0.20 | 3.818 | 75 | 1431.750 | 5 | 95.450 | | | th runoff toward Sandusky Drain |
| EXT-2 | 479.35 | 0.20 | 95.870 | 75 | 35951.250 | 5 | 2396.750 | | | noff toward Sandusky Drain Via Hunter Branch |
| EXT-3 | 186.58 | 0.20 | 37.316 | 75 | 13993.500 | 5 | 932.900 | | | h runoff toward Sandusky Drain through site |
| EXT-4 | 0.91 | 0.20 | 0.182 | 75 | 68.250 | 5 | 4.550 | External on | southeast co | rner of site through IDA toward Sandusky Drain |
| Total | 685.93 | | 137.19 | | 51444.75 | | 3429.65 | | | |
| | • | | | | | | | - | | |

Airport Method

3.26(1.1-C)L^{0.5} S^{0.33} Tc=

Tc = Time of Concentration (min)

C = Runoff Coefficient

L = Catchment Length (m) S = Catchment Slope (%)

730.70

730.70

Appendix L – Well Survey Questionnaire Responses

(please select the appropriate box)

Agree to Provide Well Information

I hereby disclose the following information to **EXP Services Inc**. regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| Name | Ril Ruto | 10 0 | | | | |
|--|---|--|---------|--|--|--|
| Address | DE CLAR | 1 Rosemary Rash | Mussen. | | | |
| Phone | 519 268 11 | 1 31. DOKCHESTER | | | | |
| Existing well | ☐ No wells present at the address noted above | | | | | |
| | Yes – please re | fer to requested details below | | | | |
| Location of Well | Shallow we | ell located in from | 0.1 | | | |
| (Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | bedroom win Well used to water to how area . House I 1975 a I believe was existing | provide HENGE ses withe | | | | |
| | - / 22 | Date Drilled | | | | |
| Depth of Well | 8 !! | | 77 | | | |
| Depth of Well Type of Well: Dug/Bored or Drilled) | 8 !! | (estimate, if not known) Static Water Level | (17 | | | |

| following a | not to address | provide s: | information | regarding | onsite | well | (s) | to | EXP | Services | Inc. | at | the |
|-------------|-------------------|---------------|-------------|-----------|--------|------|-----|----|-----|----------|------|----|-----|
| | | | | | | - | _ | _0 | | | | | |

Owner's Signature

Date

Please return to:

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5

Fax: 519-963-1152

(please select the appropriate box)

Agree to Provide Well Information

I hereby disclose the following information to **EXP Services Inc.** regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| Name | Penelope (| Cloutier | |
|---|--|--|----------------------|
| Address | 272 Clar | a St Dorches | ster ONT |
| Phone | (519) 860-8 | 131 | JONE |
| Existing well | No wells present at th | | |
| | ☐ Yes – please refer to | requested details below | |
| Location of Well | | | = |
| (Describe location, in | | | |
| reference to existing | | | |
| buildings or structures. If preferred, you can | | | |
| provide a sketch on the back of this page) | | | |
| back of this page) | | | - |
| Depth of Well | | Date Drilled (estimate, if not known) | |
| Type of Well: | | | |
| (Dug/Bored or Drilled) | | Static Water Level | |
| Do you have | □No | 1 | |
| Municipal water? | Yes – if yes, is the we | ell still being used? | |
| | de Well Information vide information regarding | onsite well (s) to EXP | Services Inc. at the |
| | • | | • |
| (1) | _ | // |) - 0 = |
| Kerry Clo | ula | May 15, | 6022 |
| Owner's Signature | | Date () | |
| Please return to: | | | |

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5 Fax: 519-963-1152

(please select the appropriate box)

Agree to Provide Well Information

I hereby disclose the following information to EXP Services Inc. regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| Name | Carlos & Sarah Almeida |
|--|---|
| Address | 289 Clara St., Dorchester, ON |
| Phone | |
| Existing well | ☑ No wells present at the address noted above |
| | ☐ Yes – please refer to requested details below |
| Location of Well | |
| (Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | |
| Depth of Well | Date Drilled (estimate, if not known) |
| Type of Well: (Dug/Bored or Drilled) | Static Water Level |
| Do you have Municipal water? | □ No □Yes – if yes, is the well still being used? ⋈/⁄ |

| Declin | a to Pro | avide | Well | Inform | nation |
|---------|----------|-------|---------|--------|--------|
| Decilli | e lu ri | JVIUE | A A CII | ,,,, | Iauvii |

| I choose | not to | provide | information | regarding | onsite | well (| s) to | EXP | Services | Inc. | at | the |
|-------------|--------|---------|-------------|-----------|--------|--------|-------|-----|----------|------|----|-----|
| following a | addres | s: | | | | | | | | | | |

Sarah almada Owner's Signature

Date

Please return to:

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5 Fax: 519-963-1152

(please select the appropriate box)

| | Agree | to | Provide | Well | Information |
|--|--------------|----|----------------|------|-------------|
|--|--------------|----|----------------|------|-------------|

I hereby disclose the following information to **EXP Services Inc**. regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| | | | 201 |
|--|------------------------------------|--|----------------------|
| Name | S. DAYLE GL | our D | |
| Address | | HERINE ST- | DORCHESTER |
| Phone | 519-268-3 | | TO THE GREET |
| Existing well | No wells present at the | | |
| | ☐ Yes – please refer to r | equested details below | D = V * E |
| (Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | | | |
| Depth of Well | | Date Drilled (estimate, if not known) | |
| Type of Well: (Dug/Bored or Drilled) | | Static Water Level | |
| Do you have Municipal water? | ☐ No ☐ Yes – if yes, is the wel | I still being used? | |
| following address: | | | Services Inc. at the |
| 5 . | | | |

Please return to:

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5 **Fax:** 519-963-1152

(please select the appropriate box)

Agree to Provide Well Information

I hereby disclose the following information to **EXP Services Inc.** regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| Address Phone Existing well | 1519 268 | verine 8t. Dorch 3 2668 | uster |
|--|---|--|-----------------|
| | 1519 268 | 3 2668 | 2010 |
| Existing well | | | |
| | | t at the address noted above | |
| | | er to requested details below | |
| (Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | | | |
| Depth of Well | | Date Drilled (estimate, if not known) | |
| Type of Well: Dug/Bored or Drilled) | | Static Water Level | |
| A | □ No Ves – if yes, is th | ne well still being used? | • |
| Dug/Bored or Drilled) Do you have flunicipal water? Decline to Provide | © Yes – if yes, is the Well Information | Static Water Level ne well still being used? rding onsite well (s) to EXP | Services Inc. a |

Please return to:

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5 Fax: 519-963-1152

WELL SURVEY QUESTIONNAIRE (please select the appropriate box)

☐ Agree to Provide Well Information

I hereby disclose the following information to EXP Services Inc. regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| Name | Chesher | - John + N | ancy |
|--|-----------------------------|---|-----------------|
| Address | 4611 (| nation Str | eeb |
| Phone | 519-2 | 68-1036 | |
| Existing well | ☐ No wells present at | the address noted above o requested details below | |
| (Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | 3 feet t | from bach ducking | door |
| Depth of Well | 6 feet? | Date Drilled (estimate, if not known) | 7 60+ years |
| Type of Well: (Dug/Bored or Drilled) | 7 | Static Water Level | 36 fet - con be |
| Do you have Municipal water? | ☑ No ☐ Yes – if yes, is the | well still being upod? | Jenopo |

☐ Decline to Provide Well Information

I choose not to provide information regarding onsite well (s) to EXP Services Inc. at the following address:

Owner's Signature

Please return to:

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5 Fax: 519-963-1152

E-mail: Heather.Jaggard@exp.com (please include WELL SURVEY in subject line).

May 7 2022

WELL SURVEY QUESTIONNAIRE (please select the appropriate box)

Agree to Provide Well Information

I hereby disclose the following information to EXP Services Inc. regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may

| Vame | | | | | 1 |
|---|----------------|----------------------------|-----------------------------|---------------------------------------|----|
| vaine | 911 | JART | QUIC | | |
| ddress | 11/11/11 | MINI | MIKS | | |
| hone | | MARION 202 0345 | 31 | DORCHESTE | R |
| xisting well | ☑ No wells | present at the add | Iress noted above | ve | H |
| ocation of Well | i res - pie | ease refer to reque | sted details belo | w | |
| Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | | | | | |
| Depth of Well | | | Drilled nate, if not known) | | |
| Type of Well: Dug/Bored or Drilled) | | Stat | ic Water Level | , | |
| o you have | □No | | | | |
| lunicipal water? | 0 W/2591 | ves is the well still I | peing used? | ERE 15 NO WELL | |
| Decline to Provide thoose not to provide lowing address: | le Well Inform | nation on regarding onsite | 17 WAS | FILLED IN IN (P Services Inc. at the | 19 |
| 1 | 1 | | | | |

Please return to:

Owner's Signature

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5

Fax: 519-963-1152

E-mail: Heather.Jaggard@exp.com (please include WELL SURVEY in subject line).

27 Apr 2022

(please select the appropriate box)

Agree to Provide Well Information

I hereby disclose the following information to **EXP Services Inc**. regarding the well on the subject property (noted below) and in doing so, acknowledge that the monitoring results may be available to the public on request.

| Name | JAMES Va | nder Brandt. | |
|--|-------------------------------|--|---------------|
| Address | 4673 Ma | rion Street Do | rchester ONT. |
| Phone | 519-281-23 | | 101000 |
| Existing well | ☐ No wells present at t | the address noted above prequested details below | |
| (Describe location, in reference to existing buildings or structures. If preferred, you can provide a sketch on the back of this page) | Inside house | 3 | |
| Depth of Well | 85 FEET | Date Drilled (estimate, if not known) | 1964? |
| Type of Well: (Dug/Bored or Drilled) | ORICED | Static Water Level | 62 FEET |
| Do you have Municipal water? | □ No ☑ Yes – if yes, is the w | ell still being used? | 10 |

| П | Decline | to Dro | wida W | Vall I | forma | 4inm |
|-----|---------|--------|--------|---------|--------|------|
| 1 1 | Decime | IO Pro | VIOR V | veli ir | ntorma | ซเกท |

I choose not to provide information regarding onsite well (s) to EXP Services Inc. at the following address:

Owner's Signature

Please return to:

Heather Jaggard Exp Services Inc. 15701 Robin's Hill Rd. London ON N5V 0A5

Fax: 519-963-1152

Hagit Blumenthal

Subject: FW: Hunter Farm - LON-21008138

Private Well Survey

Completed on April 26, 2022. A total of 87 survey forms were delivered. The neighbourhoods / properties they were delivered to are shown here: \\exp\\data\LON\LON-21008138-A0\\50 Input\\Hydrogeological Work\\door-to-door survey\LON-21008138 Hunter Farm Well Survey Neighbourhoods.jpg

Other Notes:

- A water shutoff valve was observed in the front lawn of the property located at 4673 Marion Street.
- At least one well was observed in the front lawn of a property located on the east side of Ron Allen Drive.
- Spoke to the homeowner of 4984 Marion Street. They use a private well that is approx. 65 ft deep, located in the front of the property. The well was observed during the visit. Water was dripping/flowing out the top of the well (was capped but water was seeping out of the top).
- Spoke to the owner of My Pet's Spot, located at 3826 Catherine Street. Property is on a private well took picture (see \\exp\data\LON\LON-21008138-A0\50 Input\Hydrogeological Work\door-to-door survey\3826 Catherine Street Well (My Pets Spot).jpg). Depth of well is unknown, installed approx. 1954. The owner stated roughly 26 properties in Dorchester are on their own private well, the rest are on Town water. She knows this because the owners of the 26 properties fought with the Town to keep their private wells and not be transferred to Town water. Not sure if there is a way to confirm with the Town what these 26 properties are?
- A survey could not be delivered to 4216 Catherine Street (salon). The person I spoke with said they would not
 be able to deliver the form to the property owner. They stated they do not believe they use a private well. The
 neighbouring property to the east (4218 Catherine Street Flowershop) also stated they didn't think they were
 on a well but they did take a copy of the form to provide to the property owner. These are commercial
 properties and the businesses rent from the owners.

Kassandra Wallace

EXP | Intermediate Hydrogeologist

t: +1.226.616.0742 | m: +1.519.573.9210 | e: <u>kassandra.wallace@exp.com</u>

<u>exp.com</u> | <u>legal disclaimer</u> keep it green, read from the screen **Appendix M – Dewatering Calculations**



APPENDIX M: Short-Term Flow Rate

Table M-1: Basement

| Parameters | Symbols | Unit | Value | | |
|---|----------------|--------|-----------------|--|--|
| Geological Formation | - | - | Glacial Deposit | | |
| Ground Elevation | - | mASL | 256.00 | | |
| Highest Groundwater Elevation | - | mASL | 255.45 | | |
| Lowest Basement Bottom Elevation | - | mASL | 253.50 | | |
| Base of the Water-Bearing Zone | - | mASL | 250.00 | | |
| Height of Static Water Table Above the Base of the Water-Bearing Zone | Н | m | 5.45 | | |
| Dewatering Target Elevation | - | mASL | 253.00 | | |
| Height of Target Water Level Above the Base of Water-Bearing Zone | h _w | m | 3.00 | | |
| Hydraulic Conductivity | К | m/s | 8.2E-04 | | |
| Length of Excavation | - | m | 20.00 | | |
| Width of Excavation | - | m | 20.00 | | |
| Equivalent Radius (equivalent perimeter) | r _e | m | 12.73 | | |
| Method to Calculate Radius of Influence | - | - | Cooper-Jacob | | |
| Time (30 days) | t | S | 2592000 | | |
| Specific Yield | Sy | | 0.30 | | |
| Cooper-Jacob's Radius of Influence from Sides of Excavation | Rcj | m | 294.75 | | |
| Radius of Influence | Ro | m | 307.48 | | |
| Dewatering Flow Rate (unconfined radial flow component) | Q | m³/day | 1447.07 | | |
| Factor of Safety | fs | - | 2.00 | | |
| Dewatering Flow Rate (multiplied by factor of safety) | Q.fs | m³/day | 2894 | | |
| Precipitation Event | - | mm/day | 0 | | |
| Volume from Precipitation | - | m³/day | 0 | | |
| Dewatering Flow Rate Without Safety Factor (including stormwater collection) | - | m³/day | 1447 | | |
| Dewatering Flow Rate With Safety Factor (including stormwater collection) | - | m³/day | 2894 | | |

Notes:

mASL - meters above sea level

Analytical Solution for Estimating Radial Flow from an Unconfined Aquifer to a Fully-Penetrating Excavation

$$Q_{w} = \frac{\pi K(H^{2} - h^{2})}{Ln\left[\frac{R_{o}}{r_{e}}\right]} \qquad r_{e} = \frac{a+b}{\pi} \qquad R_{o} = R_{cj} + r_{e} \qquad R_{cj} = \sqrt{2.25KDt/S}$$

(Based on the Dupuit-Forcheimer Equation)

Where:

 Q_w = Flow rate per unit length of excavation (m³/s)

K = Hydraulic conductivity (m/s)

H = Height of static water table above base of water-bearing zone (m)

h_w = Height of target water level above the base of water-bearing zone (m)

Rcj=Cooper Jacob Radius of Influence (m)

R_o=Radius of influence (m)

re=Equivalent perimeter (m)

Project No. LON-21008138-A0



Modified DUPUIT Equation: unconfined flow into a long excavation. No flow from the bottom!

Table M-2: Servicing Dewatering Calculations

| Ĭ | Section | GW level | GW Target | Aquifer Bottom | X | W | Α | K | s | r _e | R_o | L=R0/2 | H_{sat} | \mathbf{Q}_{ends} | Q _{ends} | Q _{trench} | Q _{trench} | Q _{total} | \mathbf{Q}_{total} |
|---|---------|----------|-----------|----------------|----|---|----------------|---------|------|----------------|--------|--------|-----------|---------------------|-------------------|---------------------|---------------------|--------------------|----------------------|
| ı | | m AMSL | m AMSL | m AMSL | m | m | m ² | m/s | m | m | m | m | m | m³/s | L/d | m³/s | L/d | m³/s | L/d |
| | X-X' | 255.45 | 252.50 | 250.00 | 50 | 5 | 250 | 8.2E-04 | 2.95 | 17.51 | 270.93 | 135.47 | 5.45 | 0.022056 | 1,905,603 | 0.007098 | 613,276 | 0.029154 | 2,518,878 |

$$Q = \frac{\pi K(H^2 - h^2)}{Ln\left[\frac{R_o}{r_e}\right]} + 2\left[\frac{xK(H^2 - h^2)}{2L}\right]$$

A = dewatered area (m²)

Q = construction dewatering rate (m³/sec)

K = saturated and horizontal hydraulic conductivity (m/s)

 $H = hydraulic head beyond R_0 (m)$

h = hydraulic head within A (m)

s = drawdown (=H-h)

r_e = equivalent well radius of A (m)

 R_0 = radius of influence of construction dewatering/pumping from equivalent well center (m)

x = length of the trench (m)

w = width (m)

L = distance of influence of construction dewatering/pumping from equivalent well center (m)

 $\pi = Pi(1)$

Appendix N – Limitations and Use of Report

LIMITATIONS AND USE OF REPORT

BASIS OF REPORT

This report ("Report") is based on site conditions known or inferred by the geotechnical investigation undertaken as of the date of the Report. Should changes occur which potentially impact the geotechnical condition of the site, or if construction is implemented more than one year following the date of the Report, the recommendations of EXP may require re-evaluation.

The Report is provided solely for the guidance of design engineers and on the assumption that the design will be in accordance with applicable codes and standards. Any changes in the design features which potentially impact the geotechnical analyses or issues concerning the geotechnical aspects of applicable codes and standards will necessitate a review of the design by EXP. Additional field work and reporting may also be required.

Where applicable, recommended field services are the minimum necessary to ascertain that construction is being carried out in general conformity with building code guidelines, generally accepted practices and EXP's recommendations. Any reduction in the level of services recommended will result in EXP providing qualified opinions regarding the adequacy of the work. EXP can assist design professionals or contractors retained by the Client to review applicable plans, drawings, and specifications as they relate to the Report or to conduct field reviews during construction.

Contractors contemplating work on the site are responsible for conducting an independent investigation and interpretation of the test pit results contained in the Report. The number of test pits necessary to determine the localized underground conditions as they impact construction costs, techniques, sequencing, equipment and scheduling may be greater than those carried out for the purpose of the Report.

Classification and identification of soils, rocks, geological units, contaminant materials, building envelopment assessments, and engineering estimates are based on investigations performed in accordance with the standard of care set out below and require the exercise of judgment. As a result, even comprehensive sampling and testing programs implemented with the appropriate equipment by experienced personnel may fail to locate some conditions. All investigations or building envelope descriptions involve an inherent risk that some conditions will not be detected. All documents or records summarizing investigations are based on assumptions of what exists between the actual points sampled. Actual conditions may vary significantly between the points investigated. Some conditions are subject to change over time. The Report presents the conditions at the sampled points at the time of sampling. Where special concerns exist, or the Client has special considerations or requirements, these should be disclosed to EXP to allow for additional or special investigations to be undertaken not otherwise within the scope of investigation conducted for the purpose of the Report.



RELIANCE ON INFORMATION PROVIDED

The evaluation and conclusions contained in the Report are based on conditions in evidence at the time of site inspections and information provided to EXP by the Client and others. The Report has been prepared for the specific site, development, building, design or building assessment objectives and purpose as communicated by the Client. EXP has relied in good faith upon such representations, information and instructions and accepts no responsibility for any deficiency, misstatement or inaccuracy contained in the Report as a result of any misstatements, omissions, misrepresentation or fraudulent acts of persons providing information. Unless specifically stated otherwise, the applicability and reliability of the findings, recommendations, suggestions or opinions expressed in the Report are only valid to the extent that there has been no material alteration to or variation from any of the information provided to EXP.

STANDARD OF CARE

The Report has been prepared in a manner consistent with the degree of care and skill exercised by engineering consultants currently practicing under similar circumstances and locale. No other warranty, expressed or implied, is made. Unless specifically stated otherwise, the Report does not contain environmental consulting advice.

COMPLETE REPORT

All documents, records, data and files, whether electronic or otherwise, generated as part of this assignment form part of the Report. This material includes, but is not limited to, the terms of reference given to EXP by its client ("Client"), communications between EXP and the Client, other reports, proposals or documents prepared by EXP for the Client in connection with the site described in the Report. In order to properly understand the suggestions, recommendations and opinions expressed in the Report, reference must be made to the Report in its entirety. EXP is not responsible for use by any party of portions of the Report.

USE OF REPORT

The information and opinions expressed in the Report, or any document forming part of the Report, are for the sole benefit of the Client. No other party may use or rely upon the Report in whole or in part without the written consent of EXP. Any use of the Report, or any portion of the Report, by a third party are the sole responsibility of such third party. EXP is not responsible for damages suffered by any third party resulting from unauthorized use of the Report.

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