



Proposed Industrial Subdivision 1045 Donnybrook Drive

Preliminary Stormwater Management Report

Project Location:

1045 Donnybrook Drive, Dorchester, ON

Prepared for:

Lantern Capital
2425 Matheson Boulevard East, 8th Floor,
Mississauga, ON L4W 5K4

Prepared by:

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February 18, 2022

MTE File No.: 49549-100





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1.0 Introduction

MTE Consultants Inc. (MTE) was retained by Lantern Capital, to complete the preliminary stormwater management report for the property at 1045 Donnybrook Drive in the Town of Dorchester (Municipality of Thames Centre, County of Middlesex), Ontario. As presented on the Draft Plan of Subdivision (Zelinka Priamo, January 2022) provided in **Appendix A**, it is intended to develop the property with 11 industrial blocks, public roads and a Stormwater Management (SWM) block.

The property is located to the east of the intersection of Donnybrook Drive and Starlight Lane. The property is approximately 22.17 ha in size. The property is bounded to the north by Donnybrook Drive and existing residential properties, to the west by existing residential properties, to the east by existing commercial and agricultural properties, and to the south by Highway 401. The site location is illustrated on **Figure 1**.

This report addresses the stormwater management requirements for the proposed industrial subdivision and provides a preliminary design which meets these requirements. This report is a preliminary report for support of the draft plan application. A more detailed, final SWM report will be prepared during the future subdivision detailed engineering design process.

2.0 Criteria

The proposed stormwater management (SWM) criteria in consultation with Municipality of Thames Centre for the subject site, are as follows:

- Attenuation of the post-development peak flows for the 2-year through 100-year storm events to the pre-development (existing) peak flow rates;
- Implementation of water quality controls to provide Level 1 (enhanced) treatment levels as per the MECP SWM Practices Planning and Design Manual, 2003 (SWMPDM);

The subject development is located within the Upper Thames River Subwatershed but is not located in within area regulated by the Upper Thames River Conservation Authority (UTRCA).

3.0 Methodology

In order to successfully complete the SWM design for the development, the following specific tasks were undertaken:

- Determined the allowable/pre-development flow rates;
- Determined the percent impervious of the site and catchment area parameters for inclusion in Visual OTHYMO modelling;
- Calculated post-development runoff hydrographs using Visual OTHYMO;
- Determined preliminary SWM Pond footprint to provide required storage for SWM control (both quantity and quality); and
- Preliminary investigation of re-routing the existing municipal drains on the property to allow for the proposed development.

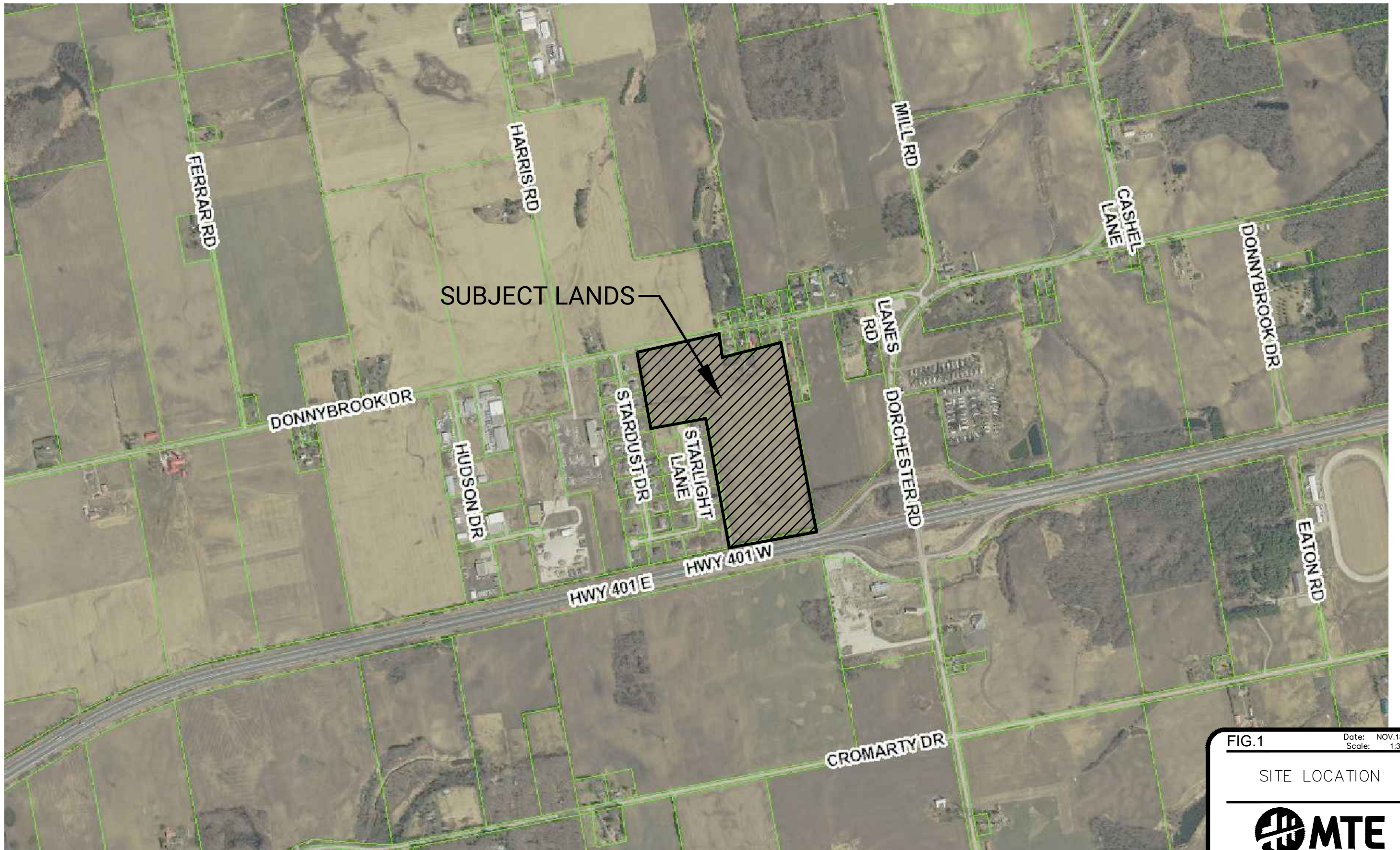


FIG.1

Date: NOV.18/21
Scale: 1:3000

SITE LOCATION



Engineers, Scientists, Surveyors

Project No.: 49549-100

4.0 Existing Conditions

A brief description of the existing drainage conditions is outlined below.

4.1 General Site information

The proposed development is located at 1045 Donnybrook Drive. The land drains to the Rath Harris Municipal Drain and to the Newton-Capstick Municipal Drain. Relevant Information for both municipal drains is provided in **Appendix B**. A preliminary geotechnical investigation was completed by Sola Engineering on June 15, 2021 (Report# 2021-15454) and is provided in **Appendix C**. A topographical survey of the site was completed by MTE on August 8, 2021.

4.1.1 Soil Information

Based on the information obtained from AG Maps (Ministry of Agriculture, Food and Rural Affairs) the local soils are determined to have hydrologic soil group (HSG) C. The preliminary geotechnical information compiled by Sola Engineering (provided in **Appendix C**) is consistent with Ag Maps.

4.2 Pre-Development Drainage

Refer to **Figure 2** for the pre-development drainage area plan. The site is currently agricultural.

Under the existing conditions, approximately 12.57 ha of the site (Catchment A01) slopes from south to the north toward the Rath Harris Municipal Drain. The drain is an open channel and conveys runoff to the north to an existing 1000 mm diameter culvert crossing under Donnybrook Drive. The drain ultimately discharges to the Dorchester Pond Drain. In addition, the external controlled flow from the adjacent Silvermoon Subdivision to the west is conveyed to Rath Harris Municipal Drain through the subject lands. The review of Silvermoon Subdivision SWM Report indicates that controlled flows to the subject land were designed to be 138 L/s for 2-year and 923 L/s for 100-year events. For more details, refer to Rath Harris Municipal Drain and Silvermoon Subdivision SWM Report, provided in **Appendix B**.

The remaining 9.60 ha lands (Catchment A02) slopes from south to east toward the Newton-Capstick Municipal Drain. The Newton-Capstick Drain consists of both a 300mm diameter tile drain and surface drainage. This drain conveys runoff to the east through the neighboring property. The drain (both 300mm diameter tile drain and surface flow) conveys runoff to the north-east through the neighbouring property, under Donnybrook Drive, under Mill Road and then joins the Lawton Municipal Drain. For more details, refer to Rath Harris Municipal Drain information, provided in **Appendix B**.

The dividing line between Rath Harris Municipal Drain and Newton-Capstick Municipal Drain was determined based on the topographic information compiled by MTE and is presented on **Figure 2**. Pre-development catchment area parameters are summarized in Table 4.1.

Table 4-1: Pre-Development Catchment Area Parameters

Catchment ID	Description	Area (ha)	Imperviousness (%)	CN Curve Number ¹
A01	Catchment Drains to Rath Harris Municipal Drain	12.57	0	83
A02	Catchment Drains to Newton-Capstick Municipal Drain	9.60	0	83
TOTAL		22.17		

¹CN values were selected in accordance with NRCS guidelines. CN values were estimated for catchment having HSG'C' and Agricultural Land (small grains, good hydrologic condition)

4.3 Existing Hydrology

Existing hydrologic conditions were evaluated using Visual OTTHYMO 6.2 (VO2) hydrologic simulation software. The existing catchment area parameters provided in **Table 4.1** above and shown on **Figure 2** were modelled to estimate the pre-development peak flows to both the Rath Harris Municipal Drain and Newton-Capstick Municipal Drain. The 2, 5, 10, 25, 50, and 100-year storm events were all modelled using the City of London's design storm parameters with a 4-hour duration.

The pre-development conditions VO2 input parameters and corresponding model output are presented in **Appendix D**. The model results are summarized in the following table.

Table 4-2: Existing Conditions Peak Flows

Storm Event	Catchment A01 Existing Peak Flow Rates to Rath Harris Municipal Drain (m ³ /s)	Catchment A02 Existing Peak Flow Rates to Newton-Capstick Municipal Drain (m ³ /s)
2-year	0.321	0.247
5-year	0.336	0.259
10-year	0.454	0.351
25-year	0.607	0.468
50-year	0.686	0.561
100-year	0.852	0.658

Due to uncertainties regarding to downstream conveyance capacity of Newton-Capstick Municipal Drain, we have proposed more stringent release rates to this drain by decreasing the existing site peak flows by 20-35%. The proposed post-development target flows outlined on **Table 4-3**.

Table 4-3: Proposed Target Release Rates to Newton-Capstick Municipal Drain

Storm Event	Catchment A02 Existing Peak Flow Rates to Newton-Capstick Municipal Drain (m ³ /s)	Percentage Decrease (%)	Proposed Target Release Rates to Newton-Capstick Municipal Drain (m ³ /s)
2-year	0.247	20	0.198
5-year	0.259	20	0.207
10-year	0.351	20	0.281
25-year	0.468	30	0.328
50-year	0.561	30	0.393
100-year	0.658	35	0.428

Although, the Rath Harris Municipal Drain has defined surface channel downstream, the existing flow rates were decreased by 10% for each storm event to generate more stringent release rates. The proposed post-development target flows are outlined below.

Table 4-4: Proposed Target Release Rates to Rath Harris Municipal Drain

Storm Event	Catchment A01 Existing Peak Flow Rates to Rath-Harris Municipal Drain (m ³ /s)	Percentage Decrease (%)	Proposed Target Release Rates to Rath-Harris Municipal Drain (m ³ /s)
2-year	0.321	10	0.289
5-year	0.336	10	0.302
10-year	0.454	10	0.409
25-year	0.607	10	0.546
50-year	0.686	10	0.617
100-year	0.852	10	0.767

5.0 Proposed Conditions

The proposed development is comprised of 11 Industrial Blocks with a public road (Street 'A'). The proposed development increases the imperviousness of the site with the addition of building and hard surface coverage. Refer to the proposed Draft Plan of Subdivision provided in **Appendix A** for the proposed development layout. A stormwater management strategy was developed to accommodate the stormwater for both the proposed development and the external drainage area.

5.1 Proposed Municipal Drain Strategy

It will be necessary to reroute the Rath Harris Municipal Drain and Newton-Capstick Municipal Drain within the subject land to accommodate proposed development. These Municipal Drain alterations will be subject to the regulations of Section 78 of the Drainage Act.

The Rath Harris Municipal Drain is to be re-routed and sized to accommodate the controlled post-development flow from the neighbouring Silvermoon Subdivision (138 L/s for 2-year and 923 L/s for 100-year events). As shown on **Figure 3**, the estimated width of re-routed Rath Harris Municipal Drain is 30 m which includes allowance for grading and buffer. More information including sizing calculations for the drain channel and culvert under the Street 'A' will be provided during the future detailed design stage of the development. The existing drain outlet (1000 mm diameter culvert under the Donnybrook Drive) is to remain under the post-development conditions.

As shown on Newton-Capstick Municipal Drain plan and profiles provided in **Appendix B** there is presently a 300mm tile drain along with the junction drop structure on the development land and a catchbasin by the east property line. It is proposed to reroute the 300 mm tile drain to run along the east property line. The conveyance capacity of the rerouted drain is to be the same (or higher) as the existing drain. The need for the junction drop structure will be reviewed accordingly. Refer to **Figure 3** which shows in concept the re-routing of the drain.

5.2 Proposed SWM Strategy

The proposed SWM strategy was developed to meet Municipal, UTRCA and provincial requirements. The proposed drainage plan and SWM strategy are shown on **Figure 3**.

Based on our SWM assessment it was determined the most efficient option to provide quantity and quality control for the proposed subdivision was through the implementation of a single wet pond. Due to the existing grading constraints it is not feasible to provide outlets from the proposed SWM Pond to both the Newton-Capstick Municipal Drain and Rath Harris Municipal Drain. Therefore, it is proposed that the pond will outlet to the Rath Harris Drain only. Runoff from the site will be controlled to the target rates for the Rath Harris Drain noted in **Table 4-3**. The allowable outlet rate to the Newton-Capstick Drain will not be utilized.

Additionally, the MECP Source Protection Information Atlas shows that the Newton-Capstick Municipal Drain has been identified as a 'WHPA Groundwater Under the Influence' (WHPA-E) area. Considering the subject site is a proposed industrial development, diverting runoff away from the Newton-Capstick Municipal Drain will be beneficial for source water protection.

Runoff from minor storm events will be collected and conveyed by proposed local storm sewers. Similarly, major flows will be conveyed to the pond block via shallow surface flow on the proposed public road. The collected stormwater will be conveyed to the proposed stormwater management facility (wet SWM pond) to control flows (both quality and quantity) before releasing to the existing Rath Harris Municipal Drain.

As shown on **Figure 3**, the post development drainage is divided to Catchment A1 (industrial development) and SWM Block Catchment A2. The total imperviousness for industrial portion was assumed to be 85%. The proposed drainage parameters are presented in **Table 5.1**, below.

Table 5-1: Post-Development Catchment Area Parameters

Catchment ID	Description	Area (ha)	Imperviousness (%)	CN Curve Number ¹
A1	Proposed Industrial Development	20.34	85	74
A2	SWM Block	1.83	0	88 ²
TOTAL		22.17		

¹CN values were selected in accordance with NRCS guidelines. CN values were estimated for catchment having HSG'C' and lawns in good conditions

²CN values were increased to account for permanent pool and impervious area (access road).

Proposed hydrologic conditions were evaluated using Visual OTTHYMO 6.2 (VO2) hydrologic simulation software. The proposed catchment area parameters provided in **Table 5.1** and shown on **Figure 3** were modelled to estimate the peak flows directed to the SWM Pond (for quality and quantity control) and Pond outflows to the Rath Harris Municipal Drain. As mentioned above, due to the existing grading constraints and to protect downstream drinking water sources, there will be no outflow from the SWM Pond to Newton-Capstick Municipal Drain. The City of London design storm parameters were used to model the storm events (25mm to 100-year). Design storms were modelled as Chicago distributions with a 4-hour storm duration. In addition, the proposed pond storage was checked by using a conservative storm duration of 24-hours for the 100-year storm. The post-development conditions VO2 input parameters and corresponding model output are presented in **Appendix E**.

5.3 Proposed SWM Pond

The proposed SWM facility will be designed to meet the subdivision stormwater quality and quantity control requirements. The proposed facility will be designed as a wet pond in accordance with the guidance presented in the Stormwater Management Planning and Design Manual, MECP, 2003 (SMPDM).

Wet ponds consist of both permanent pool and active storage. The permanent pool (1.0 m deep) is used to provide quality control while active storage provides both water quality and quantity treatment. The SWM facility was conceptually designed with side slopes of 5:1 H:V, and an active storage depth 1.7 m. The conceptual SWM Facility footprint is shown on **Figure 3**.

5.3.1 Stormwater Management - Quality Control

Water quality control of runoff from the proposed development will be provided by the wet pond in accordance with guidance presented in the MECP SMWPDM. The proposed wet pond will provide 'Enhanced' (80% TSS removal) protection level. The preliminary permanent pool and extended detention storage volumes were estimated based on the design drainage area, the estimated impervious coverage, and the criteria presented in the MECP SMPDM, as summarized in **Table 5.2**.

Table 5-2: Water Quality Storage Requirements (MECP 2003)

Parameter	Required/Provided
Wet Pond Catchment Area	22.17 ha
Impervious Level (assumed)	85%
Protection Level	Enhanced (80% TSS Removal)
Facility Type	Wet Pond
Required Total Water Quality Control Volume ¹	250 m ³ /ha
Required Extended Detention Volume ²	40 m ³ /ha
Required Permanent Pool Volume	4656 m³ (22.17 ha x (250-40))
Provided Permanent Pool Volume	6457 m³

¹Determined from MECP SMPDM Table 3.2 for imperviousness of 85% for the entire drainage area of 22.17 ha (conservative approach since pond block is considered to have imperviousness of 85%).

²Value specified in the MECP SMPDM.

The model was used to simulate the runoff response of the developed site for the 25 mm, 4-hour water quality storm. Refer to **Appendix E** for the 25mm storm modelling results and to **Appendix F** for drawdown calculations (minimum of 24-hour drawdown was provided).

The proposed wet pond will provide the required 'Enhanced' Protection Level (80% of TSS removal) of water quality.

5.3.2 Stormwater Management - Quantity Control

The proposed pond is designed to attenuate the post-development peak discharges to below the target rates outlined in **Table 4-4**. A comparison of the target rate (pre-development) and the post-development flow rates is provided in **Table 5.3**

Table 5-3: Target Rates and Post-development (Controlled) Flow Comparison

Storm Event	Target Release Rates to Rath Harris Municipal Drain (m ³ /s)	Post-Development Controlled Peak Discharges to Rath Harris Municipal Drain (m ³ /s)
2-year	0.289	0.250
5-year	0.302	0.271
10-year	0.409	0.399
25-year	0.546	0.505
50-year	0.617	0.586
100-year	0.767	0.656

5.3.3 Preliminary Stage-Storage-Discharge Assessment

The preliminary stage-storage-discharge relationship for the proposed SWM pond is presented in the following table. Note that elevations provided in **Table 5-4** are conceptual only to confirm pond sizing. As shown in **Table 5-4** below, the proposed wet pond has sufficient capacity to provide quantity control for the 100-year storm event and provide 0.3 m of vertical free board. The complete stage-storage-discharge relationship is provided in **Appendix F**.

Table 5-4: Stage Storage Discharge Relationship

Stage (conceptual)	Permanent Pool Volume (m ³)	Active Storage Volume (m ³)	Discharge (m ³ /s)	Description
275.00	0.000	0.000		Bottom of Pond
276.00	6,458	0.000		Top of Permanent Pool
276.30	6,458	2,326		
276.43	6,458	3,445	0.061	25 mm Storm WSE ¹
276.60	6,458	4,844		
276.90	6,458	7,558		
277.20	6,458	10,474		
277.27	6,458	11,166	0.658	1:100-Year WSE ¹
277.30	6,458	11,492		
277.60	6,458	14,686		
277.70	6,458	15,798		Top of the Pond

¹WSE denotes conceptual water surface elevation.

DONNYBROOK ROAD

HIGHWAY 401

APPROX. LOCATION OF EX. CB
(TO BE CONFIRMED)

APPROX. LOCATION OF NEWTON
CAPSTICK DRAIN - 300mm TILE DRAIN

EXISTING RATH HARRIS
DRAIN - SURFACE CHANNEL

SILVERMOON SUBDIVISION

STARLIGHT LANE

KEY

AREA NUMBER
A01
1.00 0%
IMPERVIOUS AREA
AREA (IN ha)

CATCHMENT AREA

MAJOR OVERLAND FLOW

EX. MUNICIPAL DRAINS

FIG.2

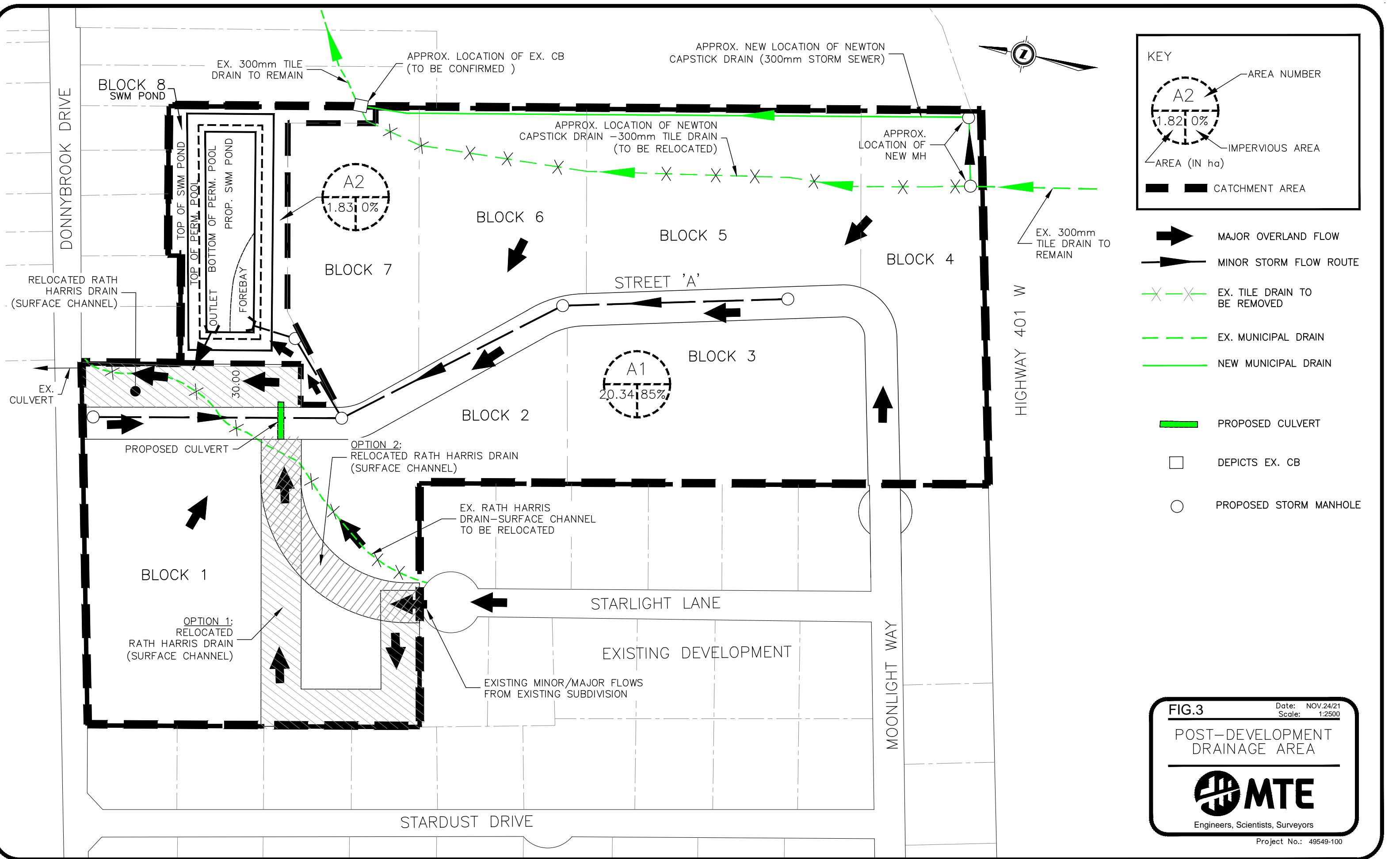
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PRE-DEVELOPMENT
DRAINAGE AREA



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KEY

- AREA NUMBER
- IMPERVIOUS AREA
- AREA (IN ha)
- CATCHMENT AREA

- MAJOR OVERLAND FLOW
- MINOR STORM FLOW ROUTE
- EX. TILE DRAIN TO BE REMOVED
- EX. MUNICIPAL DRAIN
- NEW MUNICIPAL DRAIN
- PROPOSED CULVERT
- DEPICTS EX. CB
- PROPOSED STORM MANHOLE

FIG.3 Date: NOV.24/21 Scale: 1:2500

POST-DEVELOPMENT DRAINAGE AREA

MTE
Engineers, Scientists, Surveyors

Project No.: 49549-100

6.0 Conclusions and Recommendations

Based on the foregoing analysis, it is concluded that:

- i. The presented preliminary stormwater management strategy will meet the corresponding local and provincial stormwater management policies such that the development will not result in adverse stormwater impacts on the downstream lands.
- ii. The preliminary SWM wet pond design provides post-development peak flow attenuation to below the pre-development levels and will provide quality control to achieve 'Enhanced' Protection Level water quality treatment.
- iii. As outlined, this report is a preliminary SWM report for support of the draft plan application. A more detailed, final SWM report will be prepared during the future subdivision detailed engineering design process.

All of which is respectfully submitted,

MTE Consultants Inc.

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Design Engineer

519-204-6510 ext. 2286

dsredojevic@mte85.com

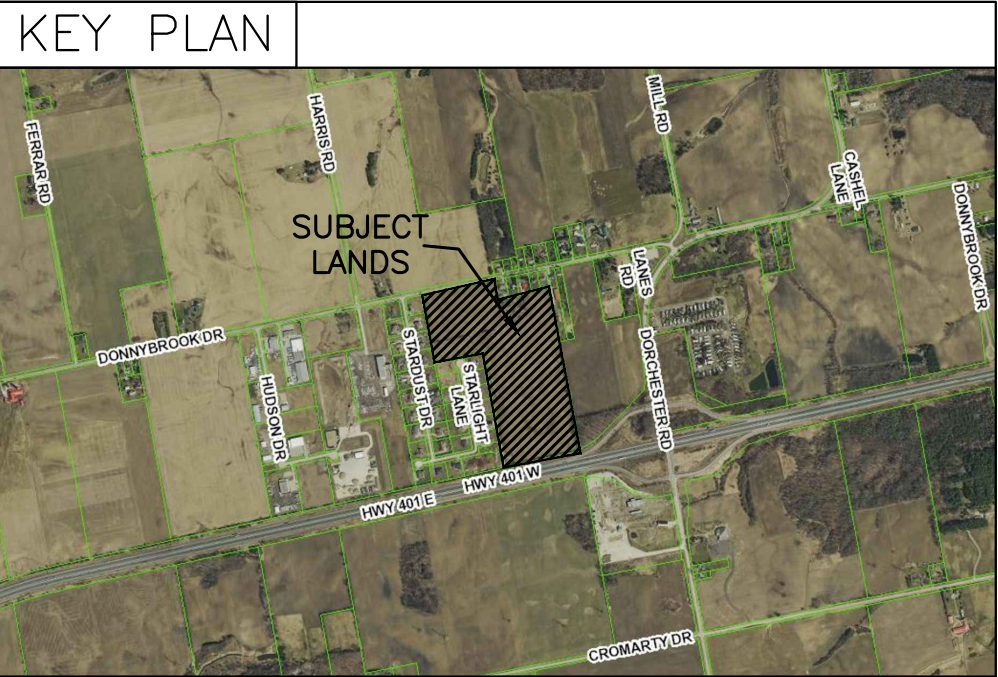
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Appendix A

Draft Plan of Subdivision



OF PART OF
CON 1 SRT PT LOTS 19,20

TOWN OF DORCHESTER
COUNTY OF MIDDLESEX

A) As shown
B) As shown
C) As shown
D) As listed above
E) As shown
F) As shown

G) As shown
H) Municipal water supply available
I) Mix of Silt Sand & Silty Clay
J) As shown
K) All municipal services to be available
L) As shown

INDUSTRIAL (BLOCKS 1-11)	17.31ha
STORMWATER MANAGEMENT (12&13)	3.47 ha
ROADS	1.39 ha

OWNER'S CERTIFICATE

LANTERN CAPITAL
HEREBY CONSENTS TO THE FILING OF THIS PLAN IN DRAFT
FORM

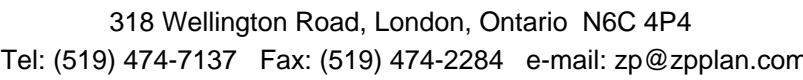
SURVEYOR'S CERTIFICATE

I HEREBY CERTIFY THAT THE BOUNDARIES OF THE LAND
TO BE SUBDIVIDED AND THEIR RELATIONSHIP TO THE
ADJACENT LANDS ARE ACCURATELY SHOWN ON THIS PLAN.



1045 DONNYBROOK
DRIVE

LANTERN CAPITAL

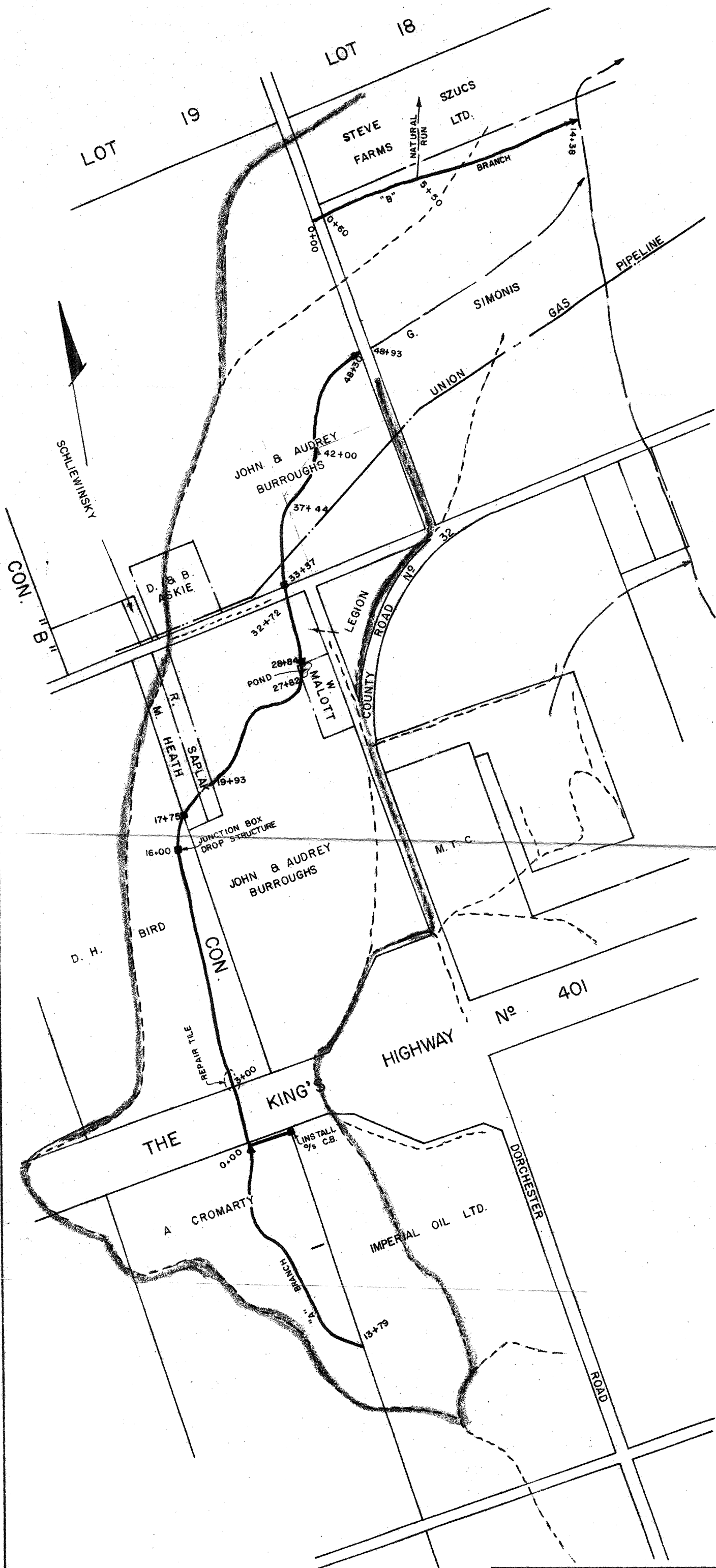


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JANUARY 2022	1:1,350

Appendix B

Existing Municipal Drain Information and Existing Silvermoon Subdivision SWM Report



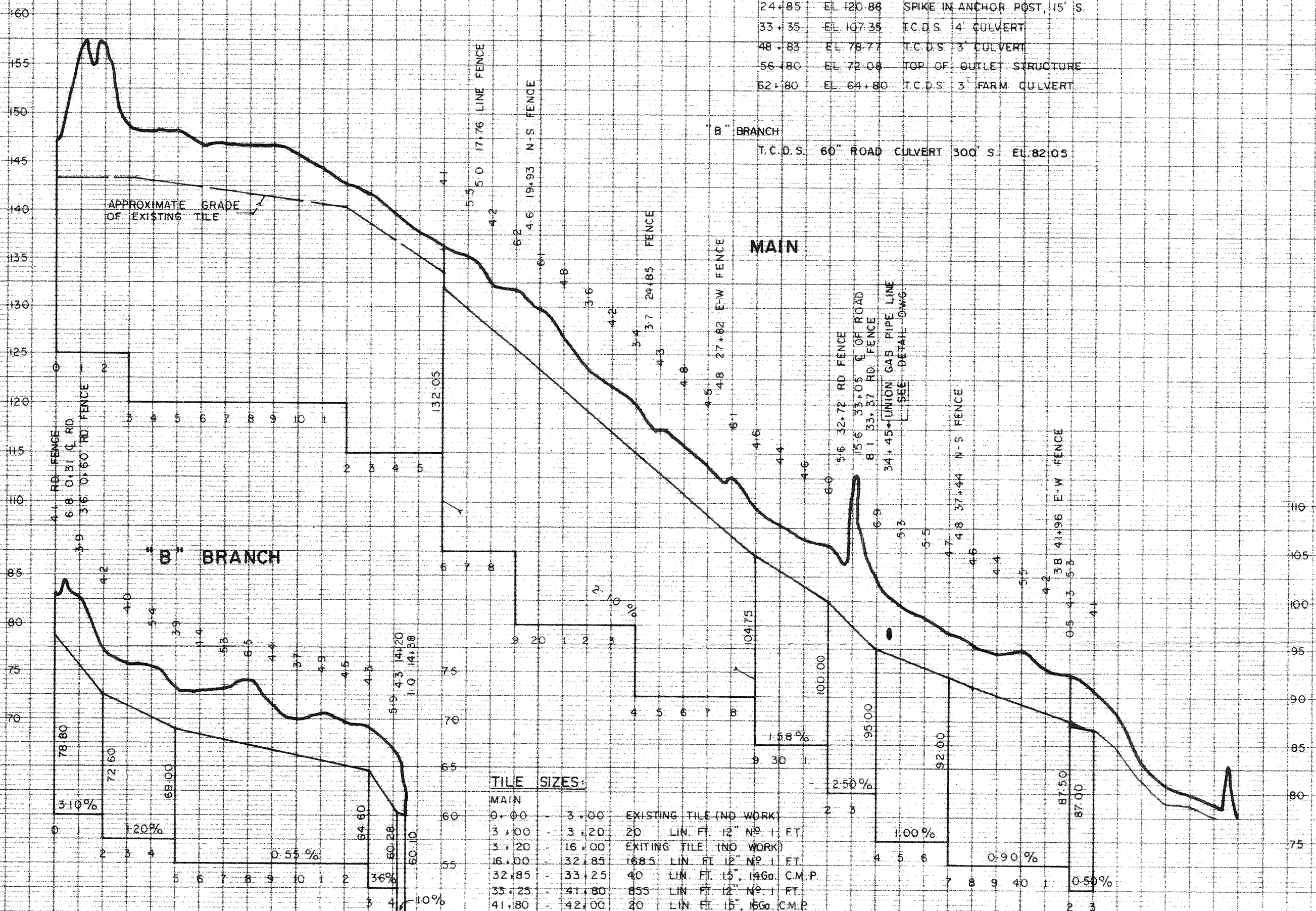
H. M. GIBSON LTD CONSULTING ENGINEERS LONDON - KINCARDINE	
NEWTON CAPSTICK DRAIN	
TWP. OF NORTH DORCHESTER	
SCALE 1" = 500'	FILE NO
DATE 8 AUG. 1977	35 - 106

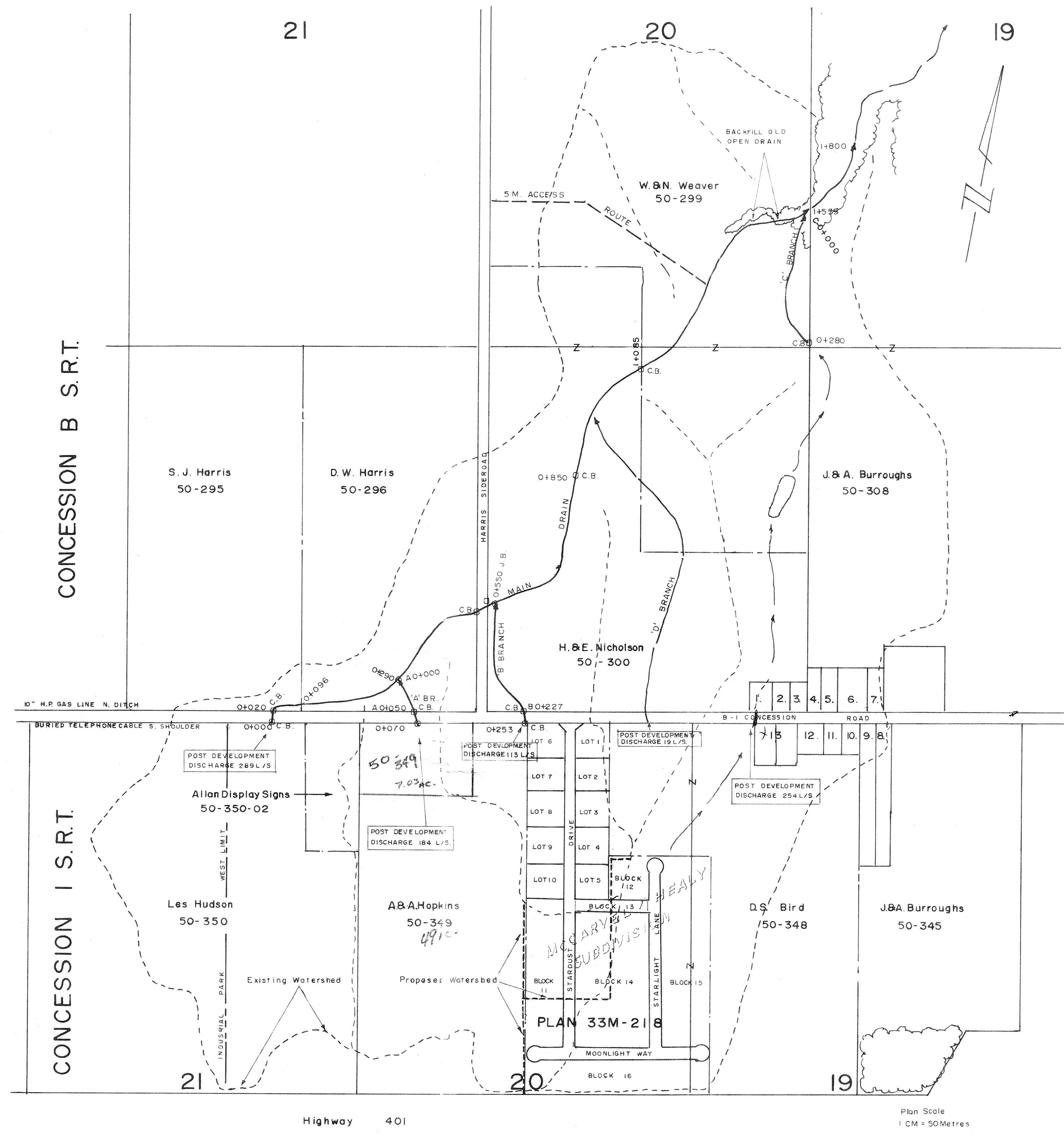
BENCH MARK:

MAIN	0+05	EL 147.24	TOP: SW. CORNER OF C.B.
	0+65	EL 150.00	T.C.D.S. 40' CULVERT
	2+02	EL 150.26	T.C.D.S. 40' CULVERT
	10+00	EL 152.09	SPIKE IN TREE 150'E
	19+07	EL 131.37	T.C.D.S. 15" CONC. SEWER PIPE
	24+85	EL 120.88	SPIKE IN ANCHOR POST, 15' S.
	33+35	EL 107.35	T.C.D.S. 4' CULVERT
	48+83	EL 78.77	T.C.D.S. 3' CULVERT
	56+80	EL 72.08	TOP OF OUTLET STRUCTURE
	62+80	EL 64.80	T.C.D.S. 3' FARM CULVERT

"B" BRANCH

T.C.D.S. 60" ROAD CULVERT 300' S. EL. 82.05





BENCH MARKS			WORKING SPACE	
0+018	Spike in hydro pole 25 M. East	270.38	The working space for the construction, maintenance and repair shall be an average width of 20 metres along the course of the drain excepting from 0+150 to 0+450, 0+950 to 1+050 and 1+225 to 1+275 where the width shall be 35 metres.	
0+530	Spike in hydro pole 10 M. North	268.99		
0+850	Spike in 600 mm. dia. Ash tree 30 Meters West	265.76		
0+050	Spike in hydro pole 5 M. East	272.86	Access to the working space shall be gained from the Harris sideroad, the Concession road and via the 5 metre wide access route shown on the plan.	
0+227	Spike in hydro pole 5 M. East	272.61		
0+280	Spike in 650 mm dia. Maple 40 Metres North.	261.31		
			SEED MIX	
			Kentucky Tall Fescue	30 Kg. / Ha.
			Birdsfoot Trefoil	20 Kg. / Ha.
			10:10:10: Fertilizer	450 Kg. / Ha.

CLEARING
All trees, brush, logs and stumps shall be cleared back an average width of 25 metres. All trees larger than 150mm. (6") in dia. shall be cut and piled for the use or disposal by the owner. No cleared material to be buried by soil.

1	50-300-01	P. & S. Nicholson
2	50-301	H. & I. Laidlaw
3	50-302	U. & B. Bell
4	50-303	H. Schlievinsky
5	50-304	R. & H. Anderson
6	50-305	P. & S. Baker
7	50-306	G. & I. Schlievinsky
8	50-346	S.D. Driver
9	50-347	J. & K. McConnell
10	50-347-02	J. & J. Periera
11	50-347-04	J. & A. Drake
12	50-347-06	N.L. Bird
13	50-347-08	J. & S. Teeple

McCarvel/Healy Subdivision
Plan 33M-218

Lot 1	50-348-12	722998 Ontario Ltd.
Lot 2	50-348-14	"
Lot 3	50-348-18	Jack Baribeau
Lot 4	50-348-20	M. Matte & G. Bernardi
Lot 5	50-348-22	Frank Prato
Lot 6	50-348-52	722998 Ontario Ltd.
Lot 7	50-348-54	D. & R. Melvin
Lot 8	50-348-56	722998 Ontario Ltd.
Lot 9	50-348-58	D. LaRose & E. Allender
Lot 10	50-348-60	722998 Ontario Ltd.

Blk 11	50-348-92	722998 Ontario Ltd.
Blk 12	50-348-50	"
Blk 13	50-348-24	"
Blk 14	50-348-28	"
Blk 15	50-348-52	"
Blk 16	50-348-64	"

TILE SIZES		
0+000 - 0+020	20 Lin. H.	700 mm. dia. 2.0 mm. wall c.m.p.
0+020 - 0+290	270 Lin. H.	600 mm. dia. concrete drain tile
0+290 - 0+512	222 Lin. H.	675 mm. dia. concrete drain tile
0+512 - 0+530	18 Lin. H.	750 mm. dia. 2.0 mm. wall c.m.p.
0+530 - 1+085	555 Lin. H.	675 mm. dia. concrete drain tile
1+085 - 1+549	464 Lin. H.	750 mm. dia. concrete drain tile
1+549 - 1+555	6 Lin. H.	1000 mm. dia. 1.6 mm. wall c.m.p.

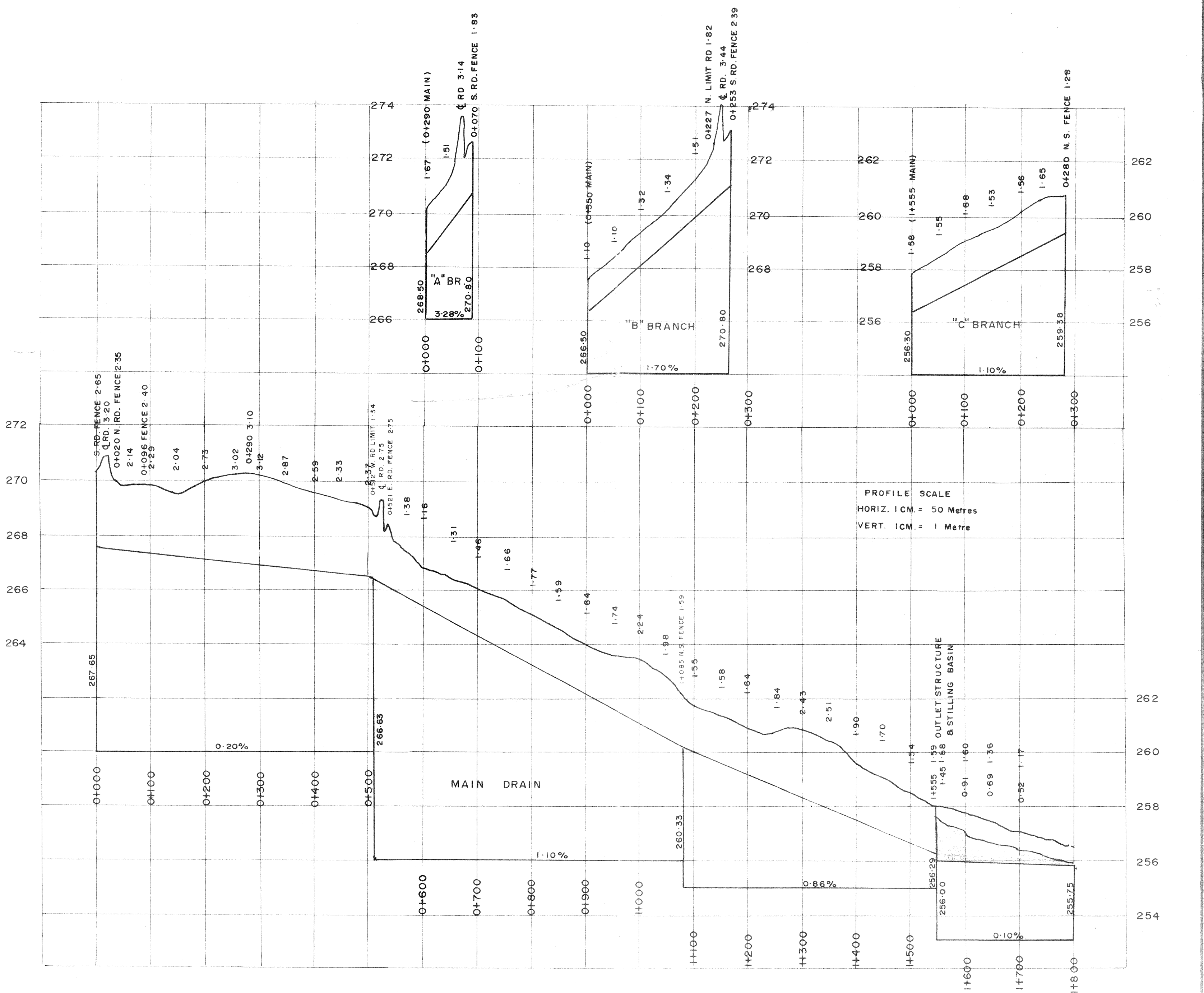
0+000 - 0+050	50 Lin. H.	300 mm. dia. concrete drain tile
0+050 - 0+176	20 Lin. H.	375 mm. dia. 2.0 mm. wall c.m.p.

0+000 - 0+227	227 Lin. H.	300 mm. dia. concrete drain tile
0+227 - 0+253	26 Lin. H.	375 mm. dia. 2.0 mm. wall c.m.p.

0+000 - 0+006	6 Lin. H.	700 mm. dia. 1.6 mm. wall c.m.p.
0+006 - 0+280	274 Lin. H.	525 mm. dia. concrete drain tile

CATCHBASINS AND JUNCTION BOXES		
Main Drain		
900 mm X 1200 mm inline ditch inlet catchbasin - 0+000, 0+020, 0+513, 0+850, & 1+085.		
600 mm X 600 mm offset ditch inlet catchbasin - 0+530		
900 mm X 1200 mm junction boxes - 0+290 & 0+550		
Branch A		
900 mm X 1200 mm inline ditch inlet catchbasin	0+070	
600 mm X 600 mm offset ditch inlet catchbasin	0+050	
Branch B		
900 mm X 1200 mm inline ditch inlet catchbasin	0+253	
600 mm X 600 mm offset ditch inlet catchbasin	0+227	
Branch C		
900 mm X 1200 mm inline ditch inlet catchbasin	0+280	

- Deep Excavation: Station 0+020 to station 0+513 will require compaction of backfill as noted on the accompanying detail drawings.
- Stripping of Topsoil: In areas requiring stripping of topsoil, station 0+150 to station 0+450, 0+950 to 1+050 and 1+225 to 1+375, the topsoil shall be stripped, stockpiled, and replaced after the tile have been installed. The stripped area shall not be less than 10 metres in width.
- Wrapping of Joints: All tile joints shall be completely wrapped with a double layer of geotextile filter fabric. The joint wrap shall be not less than 40 cm. in width and shall overlap at the ends not less than 40 cm.
- Rip Rap: Catchbasin protection - 300mm dia. 20 cubic metres. Stilling Basin - 350 mm. dia. 33 cubic metres.



NO.	REVISION	BY	DATE

W.J. BARTLETT & ASSOCIATES LTD.

CONSULTING CIVIL ENGINEERS

DORCHESTER 519-268-7091 ONTARIO

DESIGN R.B.H.

CHECKED W.J.B.

DRAWN R.B.H.

SCALE AS NOTED

RATH-HARRIS

MUNICIPAL DRAIN IMPROVEMENT

TOWNSHIP OF NORTH DORCHESTER

PLAN AND PROFILE

DATE SEPTEMBER 14, 1989

SHEET 1 OF 3

FILE NO. 890906-9

SILVERMOON SUBDIVISION

STORMWATER MANAGEMENT REPORT

FOR

980238 Ontario Ltd.

and

Anand Investments Ltd

June 17, 2004

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E	MIDUSS OUTPUT 100 YEAR STORM – POST DEVELOPMENT

1.0 INTRODUCTION

The proposed development occupies 8.40ha in Dorchester, Ontario and is known collectively as Part of Block 14, Block 15, and Block 16, Plan 33M-218. The site is bounded by Hwy. 401 to the south, Stardust Drive to the west and Donnybrook Drive to the North.

The development known as "Silvermoon Subdivision" will be comprised of 16 lots. Storm Drainage is to be conveyed by road side ditch, which ultimately discharges at the northeast corner of the site. Sanitary servicing will be provided by way of septic system on each lot with water supplied by well. Mainline Hydro, Bell and cable will be on poles along the right of way with underground servicing. Buried gasmain will also be installed to service each lot.

2.0 STORMWATER MANAGEMENT PLAN

2.1. Stormwater Management Criteria

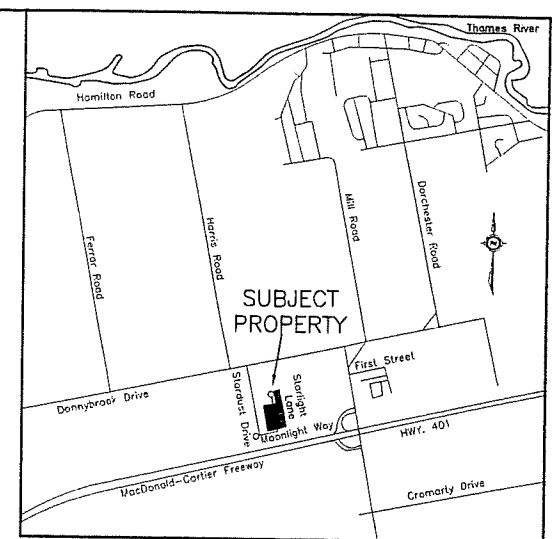
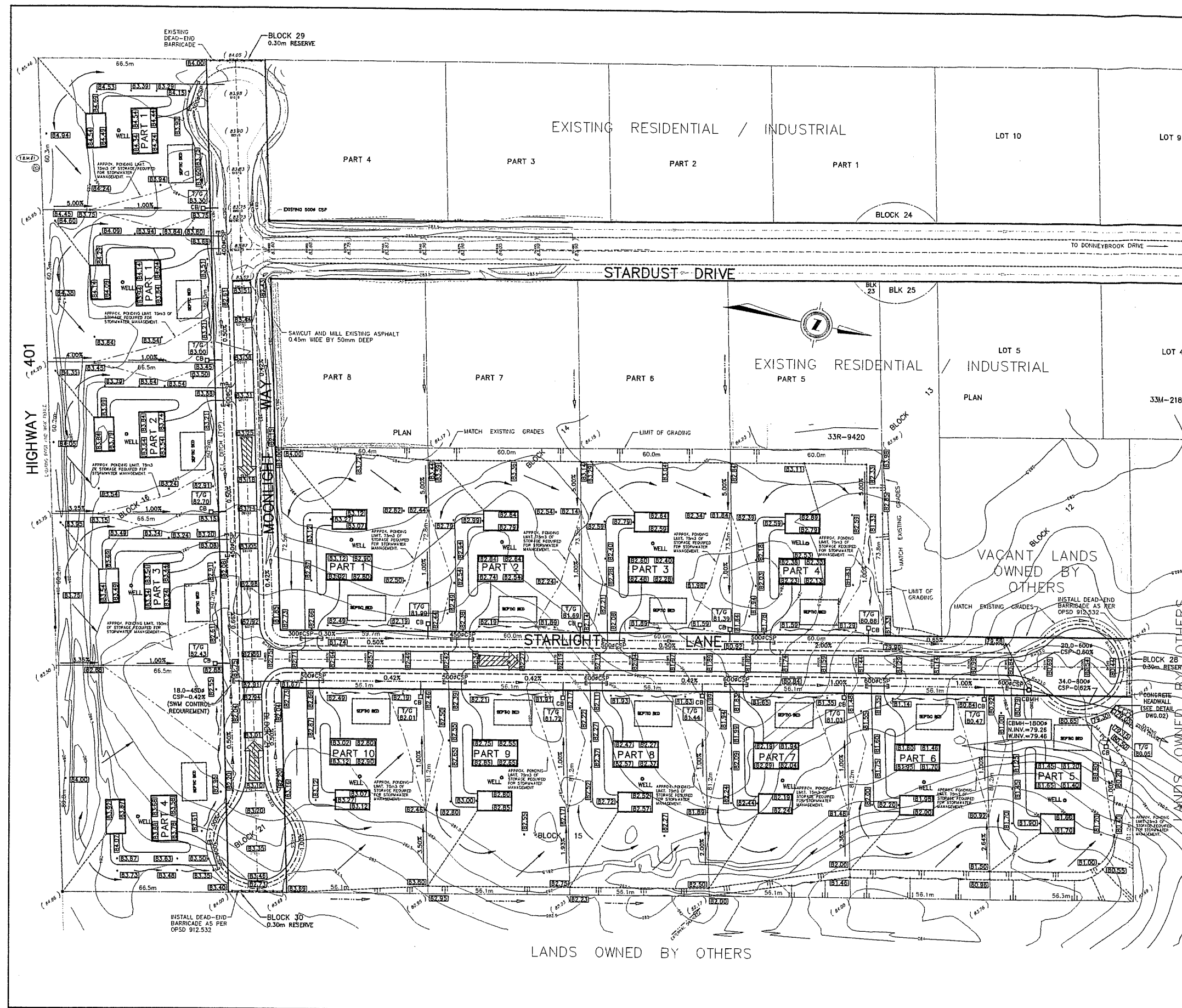
The design of the proposed stormwater management measures follow criteria presented in The Ministry of the Environment's *Stormwater Management Practices Planning and Design Manual* (2003).

Stormwater flows for the site will be restricted to predevelopment levels from the 2-year to 100-year storm event by way of lot level controls for the 2 year storm and a combination of lot level controls and roadside ditch controls for the 100 year storm.

2.2. Site Design and Stormwater Management

Grading for each lot will be such that storm flows are directed toward a surface storage swale on the low-lying side of the lot, which is to be sized to provide 75 cubic metres of surface storage. An orifice plate placed on the outlet pipe in each catchbasin located at the end of each storage area will control flow to the road side ditch during the 2 year storm. A goss trap shall be installed on each catchbasin to prevent clogging of the orifice. Flows in excess of the 2 year storm will overtop the lot storage areas to the road side ditch. Road culverts and driveway culverts have been sized to restrict flows to predevelopment levels during the 100 year storm, thereby using the road side ditches for storage. The site grading plan has been enclosed (Figure 1)

The cumulative storage volumes achieved by lot level storage is sufficient to control the 2 year storm to the predevelopment level. For the 100 year storm, control is achieved by a combination of lot level storage and road side ditch storage in order to restrict flows to predevelopment levels.



EROSION & SEDIMENTATION CONTROL NOTES:

1. PROTECT ALL EXPOSED SURFACES AND CONTROL ALL RUNOFF DURING CONSTRUCTION.
2. ALL EROSION CONTROL MEASURES TO BE IN PLACE BEFORE STARTING CONSTRUCTION AND REMAIN IN PLACE UNTIL RESTORATION IS COMPLETE.
3. MAINTAIN EROSION CONTROL MEASURES DURING CONSTRUCTION.
4. ALL COLLECTED SEDIMENT TO BE DISPOSED OF AT AN APPROVED LOCATION.
5. MINIMIZE AREA DISTURBED DURING CONSTRUCTION.
6. ALL DEWATERING TO BE DISPOSED OF IN AN APPROVED SEDIMENTATION BASIN.
7. PROTECT ALL CATCHBASINS AND MAINHOLES FROM SEDIMENTATION INTRUSION WITH GEOTEXTILE (TERRAZ SILT SACK OR APPROVED EQUIVALENT).
8. MAINTAIN DEPRESSED AREA AROUND CATCHBASINS DURING CONSTRUCTION TO PROTECT FROM SEDIMENTATION INTRUSION.
9. KEEP ALL SUMPS CLEAN DURING CONSTRUCTION.
10. PREVENT WIND-BLOWN DUST.
11. ALL OF THE ABOVE NOTES AND ANY SEDIMENT & EROSION CONTROL MEASURES ARE AT THE MINIMUM TO BE IN ACCORDANCE WITH THE MINISTRY OF NATURAL RESOURCES GUIDELINES ON EROSION AND SEDIMENT CONTROL FOR URBAN CONSTRUCTION SITES.

LEGEND

- OVERLAND FLOW ROUTE
- PROPOSED TOP OF GRATE ELEVATION
- PROPOSED FINISHED GROUND ELEVATION
- EXISTING ELEVATION
- PROPOSED CURB INLET CATCHBASIN
- PROPOSED CATCHBASIN
- PROPOSED CATCHBASIN MAINHOLE
- PROPOSED DITCH INLET CATCHBASIN
- EXISTING CURB INLET CATCHBASIN
- EXISTING CATCHBASIN
- EXISTING CATCHBASIN MAINHOLE
- EXISTING DITCH INLET CATCHBASIN
- PROPOSED CSP CULVERT

BENCHMARK

MTD MONUMENT 66-38
NORTH SIDE OF HIGHWAY 401, APPROXIMATELY 45m EAST
OF THE WEST LIMIT OF THIS SUBDIVISION.
ELEVATION 285.923

NOTE:

ADD 200 METRES TO OBTAIN GEODETIC DESIGN ELEVATIONS.

AS CONSTRUCTED NOTES	AS CONSTRUCTED SERVICES	COMPLETION	DESIGN	DATE	BY	CONSULTANT OF DIVISION	ENGINEER'S STAMP	SCALE	TITLE	PROJECT No.	SHEET No.	PLAN FILE No.
			DESIGN: JRB SPB DRAWN: GSB JRM CHECKED: DTW APPROVED: SPB DATE: JUNE 18 2004				AGM ARCHIBALD, GRAY & MCKAY ENGINEERING LTD. SURVEYING • ENGINEERING LONDON 685-5300		980238 Ontario Ltd. and Anand Investments Ltd.	1133-1/1135-1	01	

2.2.1. Hydrologic Modeling

Stormwater runoff rates were determined by hydrologic modeling using MIDUSS (Microcomputer Interactive Design of Urban Stormwater Systems). This program allows the user to test the impact on new and existing systems, utilizing accepted rainfall data to represent design storms of various durations. The 2 year storm event and 100 year storm events were used to model the site for peak flow control. Modeling parameters used can be seen in Appendix A.

The model was first run to determine the predevelopment flow from the site. Based on a total drainage area of 10.57 ha, the peak runoff from the 2 year storm is .138 cubic metres per second (138 l/s). The peak runoff from the 100 year storm is .923 cubic metres per second (923 l/s). A schematic of the model can be seen in Figure 2. The predevelopment catchment plan, modeling data and output can be seen in Appendix B and Appendix C for the 2 year and 100 year storms respectively.

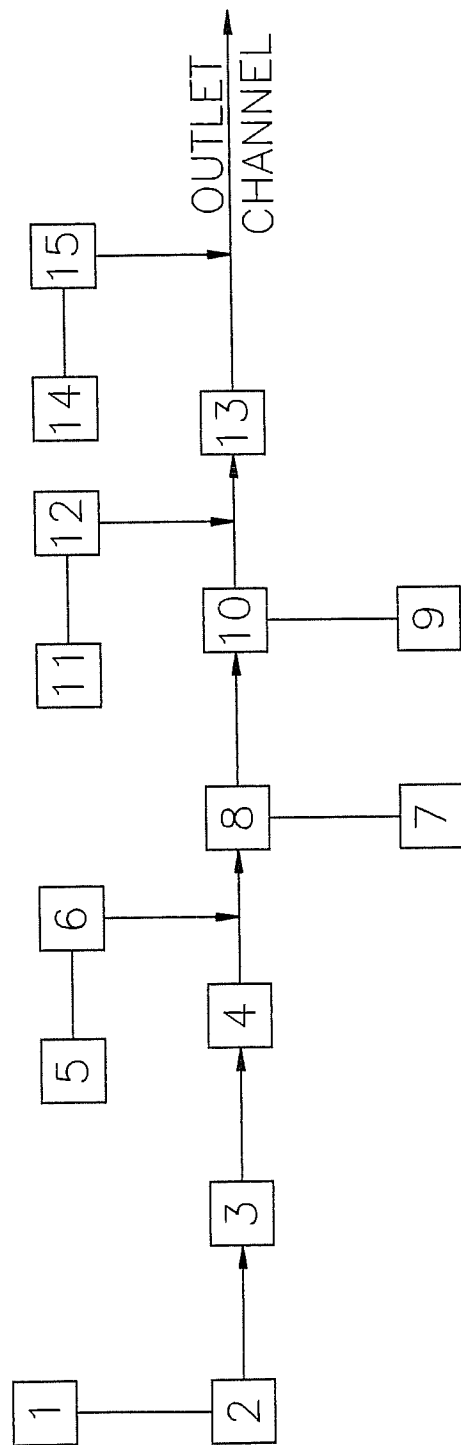
The model was run several times with various ditch storage volumes, and outlet controls (orifice, culverts) until a combination was determined that limited peak storm flows to the predevelopment level for the 2 year and 100 year storm events. A schematic of the model can be seen in Figure 3. The post development catchment plan, modeling data and output can be seen in Appendix D and E for the 2 year and 100 year storms respectively.

2.2.2. Outlet Controls

The first level of control is provided by surface storage on each lot within the development. Each lot is to provide a total of 75 cubic metres of storage. A 25mm orifice within each side yard catchbasin will restrict discharge to the roadside ditch with a peak outflow of 1.0 l/s. As stated, the cumulative storage volumes achieved by lot level storage is sufficient to control the 2 year storm to the predevelopment level. A detail of the catchbasins and orifice can be seen in Figure 4. The Inflow-Outflow Hydrograph can be seen in Appendix D.

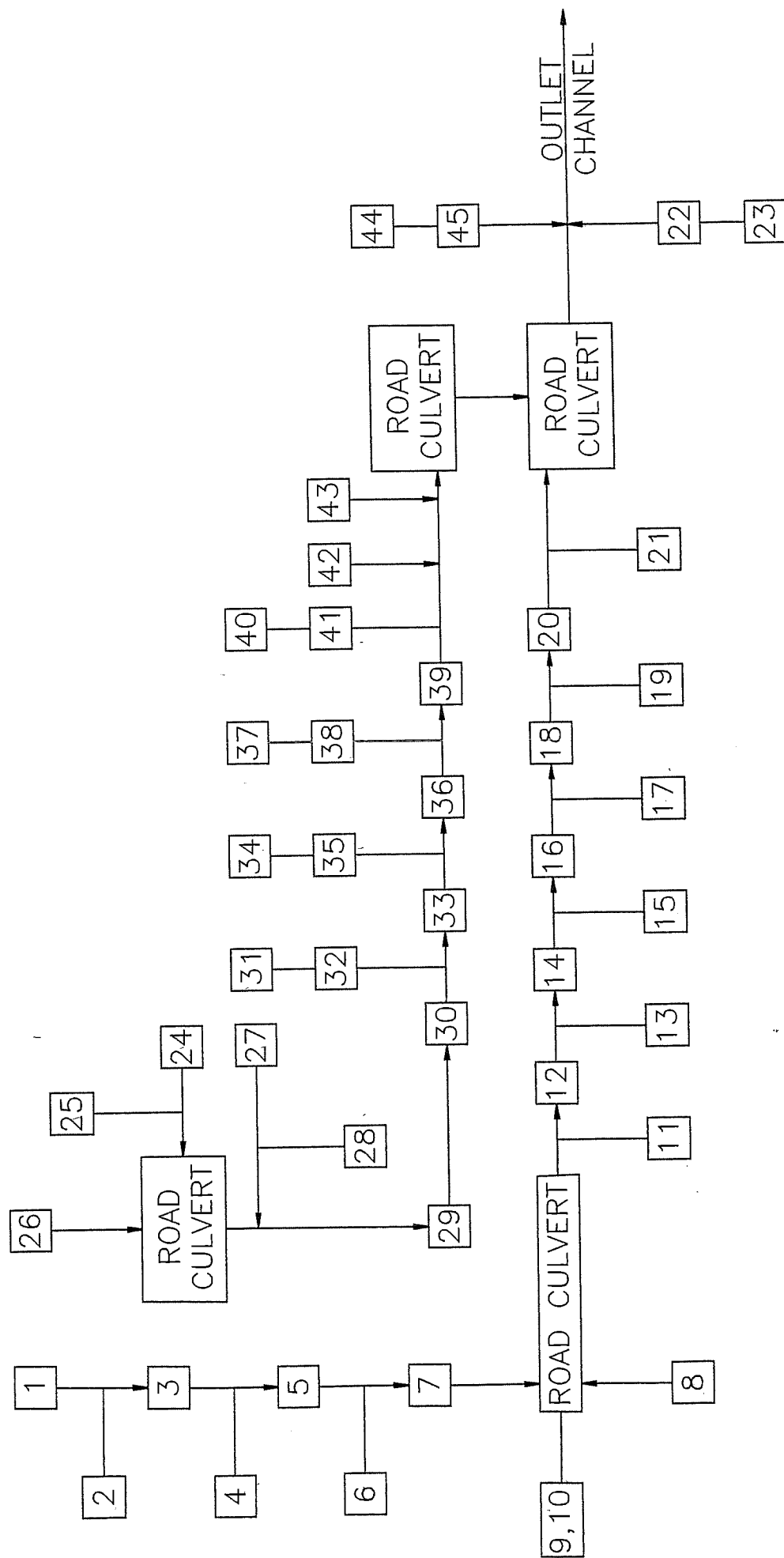
The second level of control is by surface storage within the roadside ditches. Culverts have been sized to restrict flows during the 100 year storm. The culverts utilized as flow restrictions are the 450 dia. CSP crossing Moonlight Way, The 300 dia. CSP for Part 1, Starlight Lane, and the 600 dia. CSP for Part 7, Starlight Lane. The combination of lot storage and road side ditch storage restrict flows to predevelopment levels for the 100 year storm. The Inflow-Outflow Hydrograph can be seen in Appendix E.

Discharge from the site is at the northeast corner of the site through an open channel, which is to be lined with rip-rap. Should development occur to the north, the road side ditches would need to be extended to accept flows from the subdivision and be sized accordingly.



9 CATCHMENT
AREA NUMBER

FIGURE No. 2
MIDUSS MODELING SCHEMATIC
PREDEVELOPMENT



9 CATCHMENT
AREA NUMBER

FIGURE No. 3
MIDUSS MODELING SCHEMATIC
POST DEVELOPMENT

LOT STORAGE REQUIRED = 75 m³

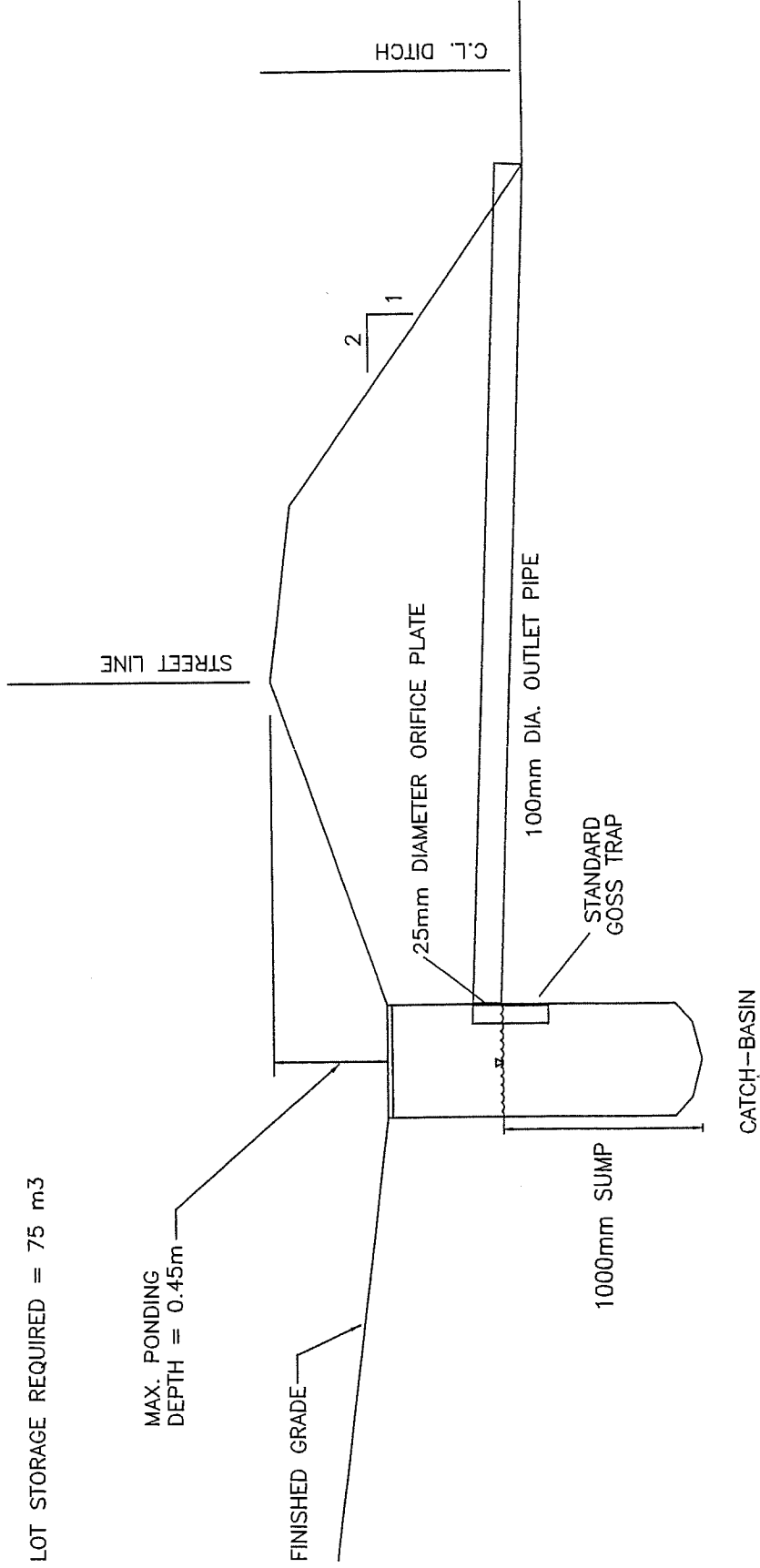


FIGURE No. 4
LOT LEVEL CONTROL

3.0 EROSION AND SEDIMENTATION CONTROL

The following measures are to be incorporated during and after construction and have been added to the appropriate drawings for construction:

1. Protect all exposed surfaces and control runoff during construction.
2. All erosion control measures are to be in place before starting construction and remain in place until restoration is complete.
3. Maintain all erosion control measures during construction.
4. All collected sediment to be disposed of at an approved site.
5. Minimize area disturbed during construction.
6. All dewatering is to be disposed of in an approved sediment basin.
7. Protect all catchbasins and manholes from sediment intrusion with geotextile (Terrafix silt sack of approved equivalent).
8. Maintain depressed area around catchbasins during construction to prevent sedimentation intrusion.
9. Keep all sumps clean during construction
10. Prevent wind-blown dust.
11. All of the above notes and any sediment and erosion control measures are at a minimum to be in accordance with the Ministry of Natural Resources guidelines on erosion and sediment control for urban construction sites.

4.0 CONCLUSION

The Stormwater Management measures to be incorporated in the subdivision will restrict post development flows to predevelopment levels by way of lot level controls for the 2 year storm and a combination of lot level controls and roadside ditch controls for the 100 year storm.

Yours truly,

Archibald, Gray and McKay Engineering Ltd.

Steve Brown, P.Eng.
Project Engineer



APPENDIX A

HYDROLOGIC MODELING PARAMETERS

SCS Soil Types

The following four classifications of soil are used.

Type A	Deep, very well drained sand or gravel
Type B	Moderately well drained soil with medium texture
Type C	Fine soil with an infiltration impeding layer
Type D	Clay; soil over rock; soil with a permanent high water table

Click here to return to [Pervious SCS Curve Number](#)

Click here to return to the [Catchment Command](#).

Pervious SCS Curve number

CN depends on Soil Type, Antecedent Moisture and Land Use.

Click [Soil Types](#) for classification

Click [Dry and Wet CN values](#) for variation from normal conditions.

Land Use	Soil type	A	B	C	D
Cultivated land with no conservation treatment		72	81	88	91
Cultivated land with conservation treatment		62	71	78	81
Pasture in poor condition		68	79	86	89
Pasture in good condition		39	61	74	81
Woodland - poor cover		45	66	77	83
Woodland - good cover		25	55	70	77
Park land - >75% grass		39	61	74	80
Park land - 50-75% grass		49	69	79	84

In some texts you may see values of *CN* quoted as a function of the percentage of impervious area. These are usually calculated as a weighted average assuming $CN_{\text{impervious}} = 98$ and CN_{pervious} equal to the value for 'Pasture in good condition' for the various soil types A, B, C or D. This is often done using an equation of the form:

$$[3.10] \quad CN_{\text{equiv}} = (\%I \, CN_{\text{imperv}} + (100 - \%I) \, CN_{\text{perv}}) / 100$$

where %I is the percentage of impervious area.

Values of *CN* estimated in this way are intended to be applied to the **total** catchment assuming other parameters to be the same for both pervious and impervious areas. Many programs (including MIDUSS 98) compute the runoff from the pervious and impervious fractions separately and then add the two hydrographs. In such cases, it is most important that you **do not use** a composite value of *CN* since this would 'double count' the impervious fraction and greatly exaggerate the runoff prediction.

Impervious

Set Parameters for the Trapezoidal Channel

CHANNEL DESIGN		
Current peak flow	0.95	c.m/sec
Manning 'n'	0.04	

Figure 4-12 – Setting the Manning 'n' value for the channel

A value for Manning "n" must be entered in order for the table of feasible designs to be shown. The initial default value as shown here is 0.04. The table below shows some suggested values for different types and conditions of channel. Notice that the roughness for channel flow is very different from that for overland flow.

Description	"n"
Concrete lined, screeded and smoothed	0.014
Gunit concrete, not smoothed with sandy deposits	0.018
Irrigation canal in hard-packed smooth sand	0.020
Canal excavated in silty clay	0.024
Channel with cobble stone bottom	0.028
Natural channel with fairly regular cross-section	0.035
Natural channel, irregular section, grass slopes	0.040
Dredged channel, irregular side slopes, grass and weeds	0.050
Irregular channel with dense growth, little foliage	0.080
Irregular channel with dense growth, with much foliage and vegetation	0.110

☐ Define arbitrary cross-section

Basewidth	0.60	metre
Left bank slope	3.00	H : 1V
Right bank slope	3.00	H : 1V

Figure 4_13 - Defining a trapezoidal cross-section.

The base width and side slopes are self-explanatory. By selecting appropriate values, trapezoidal, rectangular or triangular sections can be defined. You will find that a trapezoidal section can often be a good approximation for a natural channel. Negative (i.e. overhanging) sideslopes are not allowed with the trapezoidal cross-section.

With flow and roughness defined you can now [Review the Feasible Designs](#)

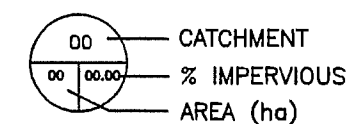
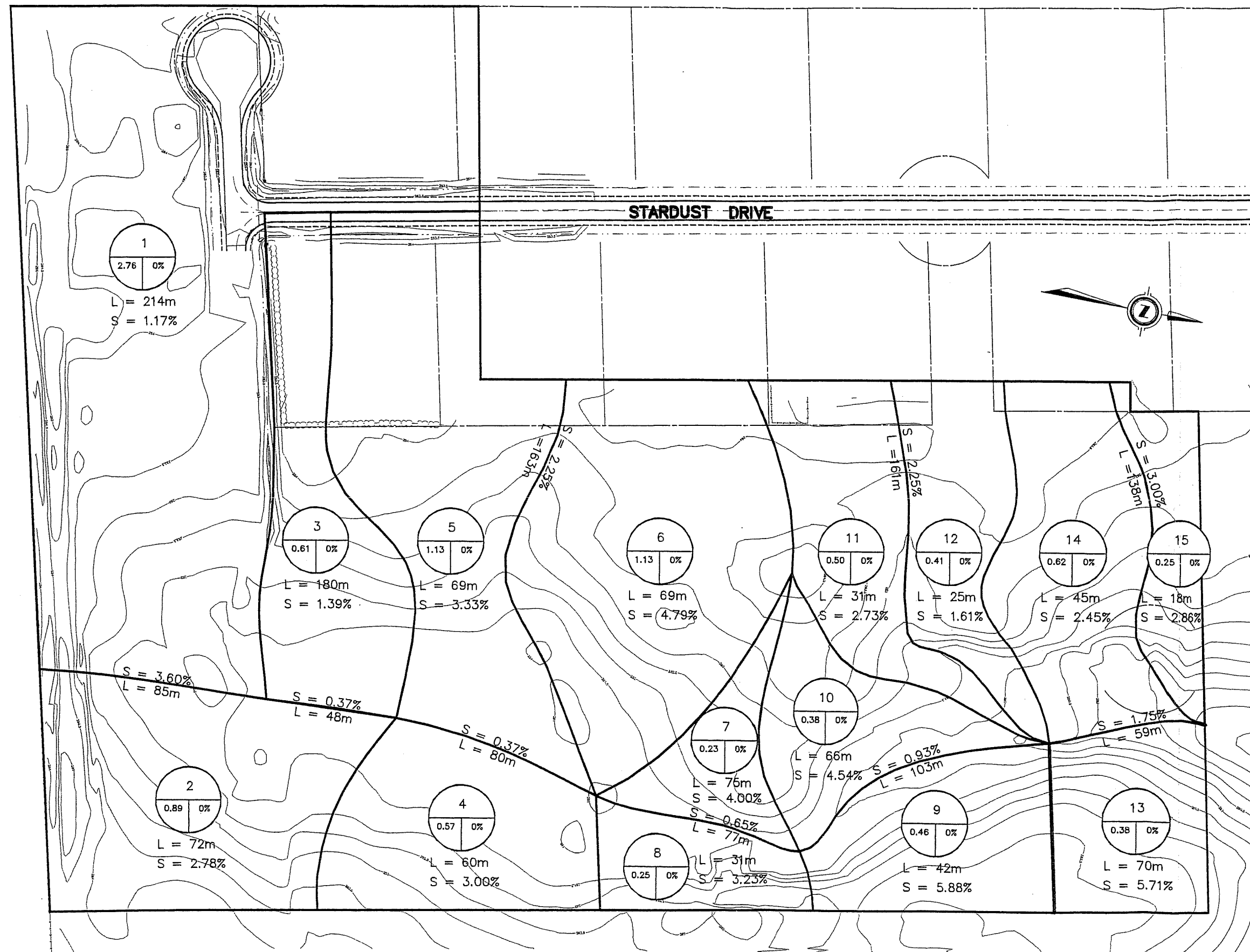
Click to return to [Channel Design](#).

APPENDIX B

CATCHMENT AREA PLAN

MIDUSS OUTPUT

2 YEAR STORM - PREDEVELOPMENT



PREDEVELOPMENT CATCHMENT AREAS

SCALE 1:1500
DATE : JUNE 1, 2004

```

"          MIDUSS 98 Output----->"
"          MIDUSS 98 version number          1.00"
"          MIDUSS 98 created          October 10, 2001"
"          10 Units used:          ie METRIC"
"          Project filename:          G:\CLIENT\1133\1\MIDUSS\
"          Output filename:          2yrfRE.Out"
"          Licensee name:          Steve Brown"
"          Company          AGM Engineering Ltd."
"          Date & Time last used:          01/06/04 at 10:17:03 AM"
" 31 TIME PARAMETERS"
"      5.000 Time Step"
"      180.000 Max. Storm length"
"      1200.000 Max. Hydrograph"
" 32 STORM Chicago storm"
"      1 Chicago storm"
"      724.690 Coefficient A"
"      5.500 Constant B"
"      0.800 Exponent C"
"      0.350 Fraction R"
"      180.000 Duration"
"      1.000 Time step multiplier"
"      Maximum intensity          104.382 mm/hr"
"      Total depth          33.312 mm"
"      6 002hyd Hydrograph extension used in this file"
=====
"          CATCHMENT 1
=====
" 33 CATCHMENT 1"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      1 ID number"
"      0.000 % Impervious"
"      2.760 Total Area"
"      214.000 Flow length"
"      1.170 Overland Slope"
"      2.760 Pervious Area"
"      214.000 Pervious length"
"      1.170 Pervious slope"
"      0.000 Impervious Area"
"      214.000 Impervious length"
"      1.170 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.024 0.000 0.000 0.000 c.m/sec"
"      Catchment 1 Pervious Impervious Total Area "
"      Surface Area 2.760 0.000 2.760 hectare"
"      Time of concentration 91.149 8.718 91.149 minutes"
"      Time to Centroid 203.771 0.000 203.771 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 919.41 0.00 919.41 c.m"
"      Rainfall losses 24.706 33.312 24.706 mm"
"      Runoff depth 8.606 0.000 8.606 mm"
"      Runoff volume 237.53 0.00 237.53 c.m"
"      Maximum flow 0.024 0.000 0.024 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.024 0.024 0.000 0.000"
=====
"          CATCHMENT 2
=====
" 33 CATCHMENT 2"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      2 ID number"
"      0.000 % Impervious"
"      0.890 Total Area"
"      72.000 Flow length"
"      2.780 Overland Slope"
"      0.890 Pervious Area"
"      72.000 Pervious length"
"      2.780 Pervious slope"
"      0.000 Impervious Area"
"      72.000 Impervious length"
"      2.780 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.016 0.024 0.000 0.000 c.m/sec"
"      Catchment 2 Pervious Impervious Total Area "
"      Surface Area 0.890 0.000 0.890 hectare"
"      Time of concentration 36.572 3.498 36.572 minutes"
"      Time to Centroid 138.712 87.608 138.712 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 296.48 0.00 296.48 c.m"
"      Rainfall losses 24.707 5.630 24.707 mm"

```

```

"      5 Next link "
"      0.005      0.040      0.040      0.000"
=====

```

CATCHMENT 4

```

=====
" 33 CATCHMENT 4"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      4 ID number"
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"      0.570 Total Area"
"      60.000 Flow length"
"      3.000 Overland Slope"
"      0.570 Pervious Area"
"      60.000 Pervious length"
"      3.000 Pervious slope"
"      0.000 Impervious Area"
"      60.000 Impervious length"
"      3.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.011      0.040      0.040      0.000 c.m/sec"
"      Catchment 4 Pervious Impervious Total Area "
"      Surface Area 0.570 0.000 0.570 hectare"
"      Time of concentration 32.042 3.065 32.042 minutes"
"      Time to Centroid 133.326 86.868 133.326 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 189.88 0.00 189.88 c.m"
"      Rainfall losses 24.710 5.554 24.710 mm"
"      Runoff depth 8.602 27.758 8.602 mm"
"      Runoff volume 49.03 0.00 49.03 c.m"
"      Maximum flow 0.011 0.000 0.011 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.011      0.045      0.040      0.000"
" 52 CHANNEL DESIGN"
"      0.045 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      0.000 Basewidth metre"
"      72.000 Left bank slope"
"      33.000 Right bank slope"
"      1.000 Channel depth metre"
"      0.370 Gradient %"
"      Depth of flow 0.072 metre"
"      Velocity 0.166 m/sec"
"      Channel capacity 50.287 c.m/sec"
"      Critical depth 0.043 metre"
" 53 ROUTE 80"
"      80.00 Reach length( metre)"
"      0.409 X-factor <= 0.5"
"      181.182 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      300.000 Routing time step ( seconds)"
"      2 No. of sub-reaches"
"      Peak outflow 0.045 c.m/sec"
"      0.011      0.045      0.045      0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1"
"      6 Combine "
"      1 Node #"
"      Maximum flow 0.045 c.m/sec"
"      Hydrograph volume 415.633 c.m"
"      0.011      0.045      0.045      0.045"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.011      0.000      0.045      0.045"
=====

```

CATCHMENT 5

```

=====
" 33 CATCHMENT 5"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      5 ID number"
"      0.000 % Impervious"
"      1.130 Total Area"
"      69.000 Flow length"
"      3.330 Overland Slope"
"      1.130 Pervious Area"
"      69.000 Pervious length"
"      3.330 Pervious slope"
"      0.000 Impervious Area"
"      69.000 Impervious length"
"      3.330 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"

```

```

=====
" 33      CATCHMENT 7"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          7 ID number"
"          0.000 % Impervious"
"          0.230 Total Area"
"          75.000 Flow length"
"          4.000 Overland Slope"
"          0.230 Pervious Area"
"          75.000 Pervious length"
"          4.000 Pervious slope"
"          0.000 Impervious Area"
"          75.000 Impervious length"
"          4.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.258 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.850 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"              0.004 0.081 0.044 0.000 c.m/sec"
"          Catchment 7 Pervious Impervious Total Area "
"          Surface Area 0.230 0.000 0.230 hectare"
"          Time of concentration 33.603 3.214 33.603 minutes"
"          Time to Centroid 135.176 87.121 135.176 minutes"
"          Rainfall depth 33.312 33.312 33.312 mm"
"          Rainfall volume 76.62 0.00 76.62 c.m"
"          Rainfall losses 24.709 5.556 24.709 mm"
"          Runoff depth 8.603 27.756 8.603 mm"
"          Runoff volume 19.79 0.00 19.79 c.m"
"          Maximum flow 0.004 0.000 0.004 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"              0.004 0.085 0.044 0.000"
=====
                        CATCHMENT 8
=====
" 33      CATCHMENT 8"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          8 ID number"
"          0.000 % Impervious"
"          0.250 Total Area"
"          31.000 Flow length"
"          3.230 Overland Slope"
"          0.250 Pervious Area"
"          31.000 Pervious length"
"          3.230 Pervious slope"
"          0.000 Impervious Area"
"          31.000 Impervious length"
"          3.230 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.258 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.850 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"              0.006 0.085 0.044 0.000 c.m/sec"
"          Catchment 8 Pervious Impervious Total Area "
"          Surface Area 0.250 0.000 0.250 hectare"
"          Time of concentration 21.087 2.017 21.087 minutes"
"          Time to Centroid 120.257 85.202 120.257 minutes"
"          Rainfall depth 33.312 33.312 33.312 mm"
"          Rainfall volume 83.28 0.00 83.28 c.m"
"          Rainfall losses 24.711 5.386 24.711 mm"
"          Runoff depth 8.601 27.926 8.601 mm"
"          Runoff volume 21.50 0.00 21.50 c.m"
"          Maximum flow 0.006 0.000 0.006 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"              0.006 0.088 0.044 0.000"
" 52      CHANNEL DESIGN"
"          0.088 Current peak flow c.m/sec"
"          0.040 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          0.000 Basewidth metre"
"          25.000 Left bank slope"
"          31.000 Right bank slope"
"          1.000 Channel depth metre"
"          0.650 Gradient %"
"          Depth of flow 0.105 metre"
"          Velocity 0.283 m/sec"
"          Channel capacity 35.537 c.m/sec"
"          Critical depth 0.073 metre"
" 53      ROUTE 77"
"          77.00 Reach length( metre)"
"          0.460 X-factor <= 0.5"
"          203.855 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"

```

```

"          Velocity          0.366   m/sec"
"          Channel capacity  29.590   c.m/sec"
"          Critical depth    0.088   metre"
" 53 ROUTE 103"
"      103.00 Reach length( metre)"
"      0.477 X-factor <= 0.5"
"      211.042 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow          0.100   c.m/sec"
"      0.008 0.100 0.100 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2"
"      6 Combine "
"      2 Node #"
"      Maximum flow          0.100   c.m/sec"
"      Hydrograph volume     723.613 c.m"
"      0.008 0.100 0.100 0.100"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.008 0.000 0.100 0.100"
=====
CATCHMENT 11
=====
" 33 CATCHMENT 11"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      11 ID number"
"      0.000 % Impervious"
"      0.500 Total Area"
"      31.000 Flow length"
"      2.730 Overland Slope"
"      0.500 Pervious Area"
"      31.000 Pervious length"
"      2.730 Pervious slope"
"      0.000 Impervious Area"
"      31.000 Impervious length"
"      2.730 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.012 0.000 0.100 0.100 c.m/sec"
"      Catchment 11 Pervious Impervious Total Area "
"      Surface Area 0.500 0.000 0.500 hectare"
"      Time of concentration 22.178 2.121 22.178 minutes"
"      Time to Centroid 121.571 85.364 121.571 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 166.56 0.00 166.56 c.m"
"      Rainfall losses 24.721 5.370 24.721 mm"
"      Runoff depth 8.591 27.942 8.591 mm"
"      Runoff volume 42.95 0.00 42.95 c.m"
"      Maximum Flow 0.012 0.000 0.012 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.012 0.012 0.100 0.100"
=====
CATCHMENT 12
=====
" 33 CATCHMENT 12"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      12 ID number"
"      0.000 % Impervious"
"      0.410 Total Area"
"      25.000 Flow length"
"      1.610 Overland Slope"
"      0.410 Pervious Area"
"      25.000 Pervious length"
"      1.610 Pervious slope"
"      0.000 Impervious Area"
"      25.000 Impervious length"
"      1.610 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.010 0.012 0.100 0.100 c.m/sec"
"      Catchment 12 Pervious Impervious Total Area "
"      Surface Area 0.410 0.000 0.410 hectare"
"      Time of concentration 22.839 2.184 22.839 minutes"
"      Time to Centroid 122.356 85.457 122.356 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 136.58 0.00 136.58 c.m"

```

```

"      59.00 Reach length( metre)"
"      0.482 X-factor <= 0.5"
"      99.700 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.123 c.m/sec"
"      0.008      0.124      0.123      0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3"
"      6 Combine "
"      3 Node #"
"      "
"      Maximum flow      0.123 c.m/sec"
"      Hydrograph volume 834.498 c.m"
"      0.008      0.124      0.123      0.123"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.008      0.000      0.123      0.123"

```

CATCHMENT 14

```

" 33 CATCHMENT 14"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      14 ID number"
"      0.000 % Impervious"
"      0.620 Total Area"
"      45.000 Flow length"
"      2.450 Overland Slope"
"      0.620 Pervious Area"
"      45.000 Pervious length"
"      2.450 Pervious slope"
"      0.000 Impervious Area"
"      45.000 Impervious length"
"      2.450 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.013      0.000      0.123      0.123 c.m/sec"
"      Catchment 14 Pervious Impervious Total Area "
"      Surface Area 0.620 0.000 0.620 hectare"
"      Time of concentration 28.651 2.740 28.651 minutes"
"      Time to Centroid 129.280 86.343 129.280 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 206.53 0.00 206.53 c.m"
"      Rainfall losses 24.715 5.461 24.715 mm"
"      Runoff depth 8.597 27.851 8.597 mm"
"      Runoff volume 53.30 0.00 53.30 c.m"
"      Maximum flow 0.013 0.000 0.013 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.013      0.013      0.123      0.123"

```

CATCHMENT 15

```

" 33 CATCHMENT 15"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      15 ID number"
"      0.000 % Impervious"
"      0.250 Total Area"
"      18.000 Flow length"
"      2.860 Overland Slope"
"      0.250 Pervious Area"
"      18.000 Pervious length"
"      2.860 Pervious slope"
"      0.000 Impervious Area"
"      18.000 Impervious length"
"      2.860 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.008      0.013      0.123      0.123 c.m/sec"
"      Catchment 15 Pervious Impervious Total Area "
"      Surface Area 0.250 0.000 0.250 hectare"
"      Time of concentration 15.784 1.510 15.784 minutes"
"      Time to Centroid 113.997 84.410 113.997 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 83.28 0.00 83.28 c.m"
"      Rainfall losses 24.739 5.436 24.739 mm"
"      Runoff depth 8.573 27.876 8.573 mm"
"      Runoff volume 21.43 0.00 21.43 c.m"
"      Maximum flow 0.008 0.000 0.008 c.m/sec"

```


minutes	120
Inflow	0.1194
Outflow	0.1197

00 minutes

[illegible]

No.	Comment	Runoff	Inflow	Outflow	Retention
61	Channel Design	0.008	0.019	0.123	0.123
62	Channel Route 138	0.008	0.019	0.019	0.123
63	Combine 3	0.008	0.019	0.019	0.138
64	Confluence 3	0.008	0.138	0.019	0.000
65	Channel Design	0.008	0.138	0.019	0.000

APPENDIX C

MIDUSS OUTPUT

100 YEAR STORM – PREDEVELOPMENT

```

"          MIDUSS 98 Output----->"
"          MIDUSS 98 version number          1.00"
"          MIDUSS 98 created          October 10, 2001"
"          10 Units used:          ie METRIC"
"          Project filename:          G:\CLIENT\1133\1\MIDUSS\"
"          Output filename:          100yrPREL.Out"
"          Licensee name:          Steve Brown"
"          Company          AGM Engineering Ltd."
"          Date & Time last used:          01/06/04 at 11:42:11 AM"

```

```

" 31      TIME PARAMETERS"
"          5.000 Time Step"
"          180.000 Max. Storm length"
"          1200.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"          1 Chicago storm"
"          1499.530 Coefficient A"
"          3.297 Constant B"
"          0.794 Exponent C"
"          0.350 Fraction R"
"          180.000 Duration"
"          1.000 Time step multiplier"
"          Maximum intensity          264.015 mm/hr"
"          Total depth          71.801 mm"
"          6 100hyd Hydrograph extension used in this file"

```

CATCHMENT 1

```

" 33      CATCHMENT 1"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          1 ID number"
"          0.000 % Impervious"
"          2.760 Total Area"
"          214.000 Flow length"
"          1.170 Overland Slope"
"          2.760 Pervious Area"
"          214.000 Pervious length"
"          1.170 Pervious slope"
"          0.000 Impervious Area"
"          214.000 Impervious length"
"          1.170 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.179 0.000 0.000 0.000 c.m/sec"
"          Catchment 1 Pervious Impervious Total Area "
"          Surface Area 2.760 0.000 2.760 hectare"
"          Time of concentration 43.811 5.823 43.811 minutes"
"          Time to Centroid 149.555 88.852 149.555 minutes"
"          Rainfall depth 71.801 71.801 1981.71 c.m"
"          Rainfall volume 1981.71 0.00 37.247 mm"
"          Rainfall losses 37.247 5.586 34.554 mm"
"          Runoff depth 34.554 66.215 953.70 c.m"
"          Runoff volume 953.70 0.00 0.179 c.m/sec"
"          Maximum flow 0.179 0.000 0.179 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.179 0.179 0.000 0.000"

```

CATCHMENT 2

```

" 33      CATCHMENT 2"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          2 ID number"
"          0.000 % Impervious"
"          0.890 Total Area"
"          72.000 Flow length"
"          2.780 Overland Slope"
"          0.890 Pervious Area"
"          72.000 Pervious length"
"          2.780 Pervious slope"
"          0.000 Impervious Area"
"          72.000 Impervious length"
"          2.780 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.111 0.179 0.000 0.000 c.m/sec"
"          Catchment 2 Pervious Impervious Total Area "
"          Surface Area 0.890 0.000 0.890 hectare"
"          Time of concentration 17.578 2.337 17.578 minutes"
"          Time to Centroid 113.102 83.260 113.102 minutes"
"          Rainfall depth 71.801 71.801 639.03 c.m"
"          Rainfall volume 639.03 0.00 37.245 mm"
"          Rainfall losses 37.245 6.103 37.245 mm"

```

```

"      5 Next link "
"      0.045      0.287      0.287      0.000"
=====

```

CATCHMENT 4

```

=====
" 33 CATCHMENT 4"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      4 ID number"
"      0.000 % Impervious"
"      0.570 Total Area"
"      60.000 Flow length"
"      3.000 Overland Slope"
"      0.570 Pervious Area"
"      60.000 Pervious length"
"      3.000 Pervious slope"
"      0.000 Impervious Area"
"      60.000 Impervious length"
"      3.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.077      0.287      0.287      0.000 c.m/sec"
"      Catchment 4      Pervious      Impervious      Total Area "
"      Surface Area      0.570      0.000      0.570      hectare"
"      Time of concentration      15.401      2.047      15.401      minutes"
"      Time to Centroid      110.103      82.820      110.103      minutes"
"      Rainfall depth      71.801      71.801      71.801      mm"
"      Rainfall volume      409.27      0.00      409.27      c.m"
"      Rainfall losses      37.284      6.111      37.284      mm"
"      Runoff depth      34.517      65.690      34.517      mm"
"      Runoff volume      196.75      0.00      196.75      c.m"
"      Maximum flow      0.077      0.000      0.077      c.m/sec"
"      HYDROGRAPH Add Runoff "
" 40 4 Add Runoff "
"      0.077      0.328      0.287      0.000"
" 52 CHANNEL DESIGN"
"      0.328 Current peak flow      c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      0.000 Basewidth      metre"
"      72.000 Left bank slope"
"      33.000 Right bank slope"
"      1.000 Channel depth      metre"
"      0.370 Gradient %"
"      Depth of flow      0.151      metre"
"      Velocity      0.272      m/sec"
"      Channel capacity      50.287      c.m/sec"
"      Critical depth      0.096      metre"
" 53 ROUTE 80"
"      80.00 Reach length( metre)"
"      0.404 X-factor <= 0.5"
"      220.436 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.325      c.m/sec"
"      0.077      0.328      0.325      0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1"
"      6 Combine "
"      1 Node #"
"      Maximum flow      0.325      c.m/sec"
"      Hydrograph volume      1668.733      c.m"
"      0.077      0.328      0.325      0.325"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.077      0.000      0.325      0.325"
=====

```

CATCHMENT 5

```

=====
" 33 CATCHMENT 5"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      5 ID number"
"      0.000 % Impervious"
"      1.130 Total Area"
"      69.000 Flow length"
"      3.330 Overland Slope"
"      1.130 Pervious Area"
"      69.000 Pervious length"
"      3.330 Pervious slope"
"      0.000 Impervious Area"
"      69.000 Impervious length"
"      3.330 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"

```

```

=====
" 33      CATCHMENT 7"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          7 ID number"
"          0.000 % Impervious"
"          0.230 Total Area"
"          75.000 Flow length"
"          4.000 Overland Slope"
"          0.230 Pervious Area"
"          75.000 Pervious length"
"          4.000 Pervious slope"
"          0.000 Impervious Area"
"          75.000 Impervious length"
"          4.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"              0.030 0.567 0.301 0.000 c.m/sec"
"          Catchment 7 Pervious Impervious Total Area "
"          Surface Area 0.230 0.000 0.230 hectare"
"          Time of concentration 16.151 2.147 16.151 minutes"
"          Time to Centroid 111.188 82.948 111.188 minutes"
"          Rainfall depth 71.801 71.801 71.801 mm"
"          Rainfall volume 165.14 0.00 165.14 c.m"
"          Rainfall losses 37.381 6.073 37.381 mm"
"          Runoff depth 34.420 65.728 34.420 mm"
"          Runoff volume 79.17 0.00 79.17 c.m"
"          Maximum flow 0.030 0.000 0.030 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"              0.030 0.594 0.301 0.000"
=====
"          CATCHMENT 8"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          8 ID number"
"          0.000 % Impervious"
"          0.250 Total Area"
"          31.000 Flow length"
"          3.230 Overland Slope"
"          0.250 Pervious Area"
"          31.000 Pervious length"
"          3.230 Pervious slope"
"          0.000 Impervious Area"
"          31.000 Impervious length"
"          3.230 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"              0.043 0.594 0.301 0.000 c.m/sec"
"          Catchment 8 Pervious Impervious Total Area "
"          Surface Area 0.250 0.000 0.250 hectare"
"          Time of concentration 10.135 1.347 10.135 minutes"
"          Time to Centroid 102.810 81.753 102.810 minutes"
"          Rainfall depth 71.801 71.801 71.801 mm"
"          Rainfall volume 179.50 0.00 179.50 c.m"
"          Rainfall losses 37.420 6.661 37.420 mm"
"          Runoff depth 34.381 65.140 34.381 mm"
"          Runoff volume 85.95 0.00 85.95 c.m"
"          Maximum flow 0.043 0.000 0.043 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"              0.043 0.617 0.301 0.000"
" 52      CHANNEL DESIGN"
"          0.617 Current peak flow c.m/sec"
"          0.040 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          0.000 Basewidth metre"
"          25.000 Left bank slope"
"          31.000 Right bank slope"
"          1.000 Channel depth metre"
"          0.650 Gradient %"
"          Depth of flow 0.219 metre"
"          Velocity 0.461 m/sec"
"          Channel capacity 35.537 c.m/sec"
"          Critical depth 0.158 metre"
" 53      ROUTE 77"
"          77.00 Reach length( metre)"
"          0.418 X-factor <= 0.5"
"          125.342 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"

```

```

"          Velocity                0.592    m/sec"
"          Channel capacity        29.590    c.m/sec"
"          Critical depth          0.191    metre"
" 53      ROUTE 103"
"          103.00 Reach length( metre)"
"          0.452 X-factor <= 0.5"
"          130.405 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500 Beta weighting factor"
"          100.000 Routing time step ( seconds)"
"          1 No. of sub-reaches"
"          Peak outflow                0.675    c.m/sec"
"          0.053 0.687 0.675 0.000 c.m/sec"
" 40      HYDROGRAPH Combine 2"
"          6 Combine "
"          2 Node #"
"          Maximum flow                0.675    c.m/sec"
"          Hydrograph volume          2902.604    c.m"
"          0.053 0.687 0.675 0.675"
" 40      HYDROGRAPH Start - New Tributary"
"          2 Start - New Tributary"
"          0.053 0.000 0.675 0.675"
=====
CATCHMENT 11
=====
" 33      CATCHMENT 11"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          11 ID number"
"          0.000 % Impervious"
"          0.500 Total Area"
"          31.000 Flow length"
"          2.730 Overland Slope"
"          0.500 Pervious Area"
"          31.000 Pervious length"
"          2.730 Pervious slope"
"          0.000 Impervious Area"
"          31.000 Impervious length"
"          2.730 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.083 0.000 0.675 0.675 c.m/sec"
"          Catchment 11 Pervious Impervious Total Area "
"          Surface Area 0.500 0.000 0.500 hectare"
"          Time of concentration 10.660 1.417 10.660 minutes"
"          Time to Centroid 103.505 81.818 103.505 minutes"
"          Rainfall depth 71.801 71.801 71.801 mm"
"          Rainfall volume 359.01 0.00 359.01 c.m"
"          Rainfall losses 37.365 6.554 37.365 mm"
"          Runoff depth 34.436 65.247 34.436 mm"
"          Runoff volume 172.18 0.00 172.18 c.m"
"          Maximum flow 0.083 0.000 0.083 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.083 0.083 0.675 0.675"
=====
CATCHMENT 12
=====
" 33      CATCHMENT 12"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          12 ID number"
"          0.000 % Impervious"
"          0.410 Total Area"
"          25.000 Flow length"
"          1.610 Overland Slope"
"          0.410 Pervious Area"
"          25.000 Pervious length"
"          1.610 Pervious slope"
"          0.000 Impervious Area"
"          25.000 Impervious length"
"          1.610 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.067 0.083 0.675 0.675 c.m/sec"
"          Catchment 12 Pervious Impervious Total Area "
"          Surface Area 0.410 0.000 0.410 hectare"
"          Time of concentration 10.977 1.459 10.977 minutes"
"          Time to Centroid 103.942 81.847 103.942 minutes"
"          Rainfall depth 71.801 71.801 71.801 mm"
"          Rainfall volume 294.38 0.00 294.38 c.m"

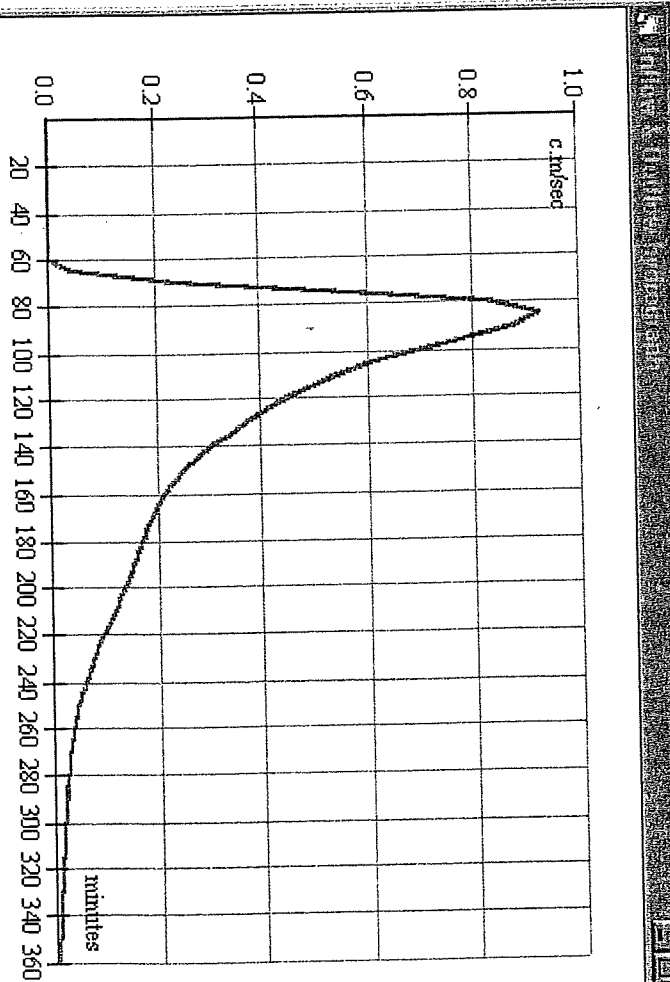
```

```

"      59.00 Reach length( metre)"
"      0.464 X-factor <= 0.5"
"      61.932 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      60.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.812 c.m/sec"
"      0.056 0.830 0.812 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3"
"      6 Combine "
"      3 Node #"
"      Maximum flow 0.812 c.m/sec"
"      Hydrograph volume 3347.078 c.m"
"      0.056 0.830 0.812 0.812"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.056 0.000 0.812 0.812"
=====
CATCHMENT 14
=====
" 33 CATCHMENT 14"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      14 ID number"
"      0.000 % Impervious"
"      0.620 Total Area"
"      45.000 Flow length"
"      2.450 Overland Slope"
"      0.620 Pervious Area"
"      45.000 Pervious length"
"      2.450 Pervious slope"
"      0.000 Impervious Area"
"      45.000 Impervious length"
"      2.450 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.091 0.000 0.812 0.812 c.m/sec"
"      Catchment 14 Pervious Impervious Total Area "
"      Surface Area 0.620 0.000 0.620 hectare"
"      Time of concentration 13.771 1.830 13.771 minutes"
"      Time to Centroid 107.853 82.493 107.853 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 445.17 0.00 445.17 c.m"
"      Rainfall losses 37.329 6.225 37.329 mm"
"      Runoff depth 34.472 65.577 34.472 mm"
"      Runoff volume 213.73 0.00 213.73 c.m"
"      Maximum flow 0.091 0.000 0.091 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.091 0.091 0.812 0.812"
=====
CATCHMENT 15
=====
" 33 CATCHMENT 15"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      15 ID number"
"      0.000 % Impervious"
"      0.250 Total Area"
"      18.000 Flow length"
"      2.860 Overland Slope"
"      0.250 Pervious Area"
"      18.000 Pervious length"
"      2.860 Pervious slope"
"      0.000 Impervious Area"
"      18.000 Impervious length"
"      2.860 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.049 0.091 0.812 0.812 c.m/sec"
"      Catchment 15 Pervious Impervious Total Area "
"      Surface Area 0.250 0.000 0.250 hectare"
"      Time of concentration 7.586 1.008 7.586 minutes"
"      Time to Centroid 99.305 81.202 99.305 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 179.50 0.00 179.50 c.m"
"      Rainfall losses 37.358 7.725 37.358 mm"
"      Runoff depth 34.443 64.076 34.443 mm"
"      Runoff volume 86.11 0.00 86.11 c.m"
"      Maximum flow 0.049 0.000 0.049 c.m/sec"

```


ROUTE		UNIT	
Class (curriculum)		Room no.	0024
Type	Channel type	Room length	5
Channel depth	1.000	Room no. U.S.	0052
Gradient	1.250	Room	5
Measuring by	0.000	Room	0.002
Depth of flow	0.209	Room	0.002
Flow depth	59.869	Room	0.002
	0.00250	Room	0.002
Used	Reason: length 5.00 m	Room	0.002
Using	Unit: length 5.00 m	Room	0.002

[illegible]

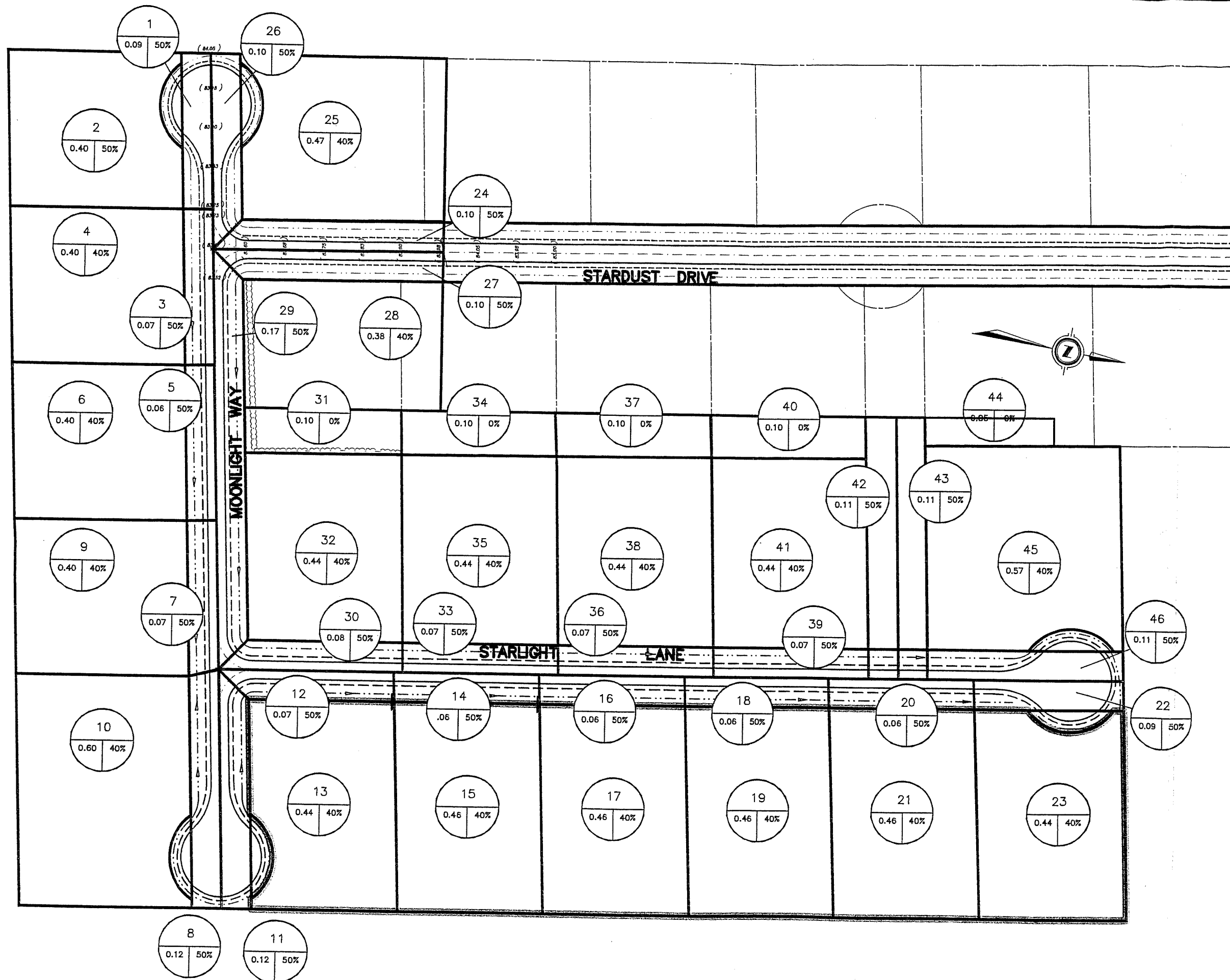
No.	Command	Runoff	Follow	Outflow	Injection
61	Channel Design	0.049	0.133	0.812	0.812
62	Channel Route 138	0.049	0.133	0.128	0.812
63	Combine 3	0.049	0.133	0.128	0.924
64	Confluence 3	0.049	0.924	0.128	0.000
65	Channel Design	0.049	0.924	0.128	0.000

APPENDIX D

CATCHMENT AREA PLAN

MIDUSS OUTPUT

2 YEAR STORM – POST DEVELOPMENT



POST DEVELOPMENT CATCHMENT AREAS

SCALE 1:1500
DATE : MAY 31 2004

```

" MIDUSS 98 Output-----"
" MIDUSS 98 version number 1.00"
" MIDUSS 98 created October 10, 2001"
" 10 Units used: ie METRIC"
" Project filename: G:\CLIENT\1133\1\MIDUSS\
" Output filename: 2yrpost1.Out"
" Licensee name: Steve Brown"
" Company AGM Engineering Ltd."
" Date & Time last used: 08/06/04 at 10:57:57 AM"
" 5.000 Time Step"
" 180.000 Max. Storm length"
" 1200.000 Max. Hydrograph"
=====
2 YEAR STORM
=====
" 32 STORM Chicago storm"
" 1 Chicago storm"
" 724.690 Coefficient A"
" 5.500 Constant B"
" 0.800 Exponent C"
" 0.350 Fraction R"
" 180.000 Duration"
" 1.000 Time step multiplier"
" Maximum intensity 104.382 mm/hr"
" Total depth 33.312 mm"
" 6 002hyd Hydrograph extension used in this file"
=====
CATCHMENT 1
=====
" 33 CATCHMENT 1"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 1 ID number"
" 50.000 % Impervious"
" 0.090 Total Area"
" 5.750 Flow length"
" 2.000 Overland Slope"
" 0.045 Pervious Area"
" 5.750 Pervious length"
" 2.000 Pervious slope"
" 0.045 Impervious Area"
" 5.750 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.258 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.850 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.010 0.000 0.000 0.000 c.m/sec"
" Catchment 1 Pervious Impervious Total Area "
" Surface Area 0.045 0.045 0.090 hectare"
" Time of concentration 8.860 0.847 2.779 minutes"
" Time to Centroid 105.679 83.592 88.917 minutes"
" Rainfall depth 33.312 33.312 33.312 mm"
" Rainfall volume 14.99 14.99 29.98 c.m"
" Rainfall losses 24.731 6.304 15.518 mm"
" Runoff depth 8.581 27.008 17.794 mm"
" Runoff volume 3.86 12.15 16.01 c.m"
" Maximum flow 0.002 0.010 0.010 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.010 0.010 0.000 0.000"
" 52 CHANNEL DESIGN"
" 0.010 Current peak flow c.m/sec"
" 0.035 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 1.500 Basewidth metre"
" 2.000 Left bank slope"
" 2.000 Right bank slope"
" 0.900 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.033 metre"
" Velocity 0.199 m/sec"
" Channel capacity 3.967 c.m/sec"
" Critical depth 0.017 metre"
" 53 ROUTE 72"
" 72.00 Reach length( metre)"
" 0.473 X-factor <= 0.5"
" 271.319 K-lag ( seconds)"
" 0.000 Default (0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.009 c.m/sec"
" 0.010 0.010 0.009 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1"
" 6 Combine "
" 1 Node #"
" Maximum flow 0.009 c.m/sec"
" Hydrograph volume 16.015 c.m"
" 0.010 0.010 0.009 0.009"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"

```

```

"      0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.008      0.010      0.001      0.000 c.m/sec"
"      Catchment 3      Pervious      Impervious      Total Area      "
"      Surface Area      0.035      0.035      0.070      hectare"
"      Time of concentration      8.860      0.847      2.779      minutes"
"      Time to Centroid      105.679      83.592      88.917      minutes"
"      Rainfall depth      33.312      33.312      33.312      mm"
"      Rainfall volume      11.66      11.66      23.32      c.m"
"      Rainfall losses      24.731      6.304      15.518      mm"
"      Runoff depth      8.581      27.008      17.794      mm"
"      Runoff volume      3.00      9.45      12.46      c.m"
"      Maximum flow      0.001      0.008      0.008      c.m/sec"
" 40      HYDROGRAPH Add Runoff      "
"      4      Add Runoff      "
"          0.008      0.016      0.001      0.000"
" 52      CHANNEL DESIGN"
"      0.016 Current peak flow      c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth      metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth      metre"
"      0.500 Gradient      %"
"          Depth of flow      0.043      metre"
"          Velocity      0.236      m/sec"
"          Channel capacity      3.967      c.m/sec"
"          Critical depth      0.022      metre"
" 53      ROUTE 60"
"      60.20 Reach length( metre)"
"      0.458 X-factor <= 0.5"
"      191.124 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"          Peak outflow      0.015      c.m/sec"
"          0.008      0.016      0.015      0.000 c.m/sec"
" 40      HYDROGRAPH Combine 2"
"      6 Combine      "
"      2 Node #      "
"          Maximum flow      0.015      c.m/sec"
"          Hydrograph volume      93.446      c.m"
"          0.008      0.016      0.015      0.015"
" 40      HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"          0.008      0.000      0.015      0.015"
=====
CATCHMENT 4
=====
" 33      CATCHMENT 4"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      3 ID number"
"      40.000 % Impervious"
"      0.400 Total Area"
"      60.200 Flow length"
"      2.000 Overland Slope"
"      0.240 Pervious Area"
"      60.200 Pervious length"
"      2.000 Pervious slope"
"      0.160 Impervious Area"
"      60.200 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.033      0.000      0.015      0.015 c.m/sec"
"      Catchment 3      Pervious      Impervious      Total Area      "
"      Surface Area      0.240      0.160      0.400      hectare"
"      Time of concentration      36.259      3.468      13.892      minutes"
"      Time to Centroid      138.336      87.562      103.703      minutes"
"      Rainfall depth      33.312      33.312      33.312      mm"
"      Rainfall volume      79.95      53.30      133.25      c.m"
"      Rainfall losses      24.708      5.619      17.072      mm"
"      Runoff depth      8.604      27.693      16.240      mm"
"      Runoff volume      20.65      44.31      64.96      c.m"
"      Maximum flow      0.004      0.032      0.033      c.m/sec"
" 40      HYDROGRAPH Add Runoff      "
"      4      Add Runoff      "
"          0.033      0.033      0.015      0.015"
" 54      POND DESIGN"
"      0.033 Current peak flow      c.m/sec"
"      65.0 Hydrograph volume      c.m/sec"
"      5. Number of stages"
"      0.000 Minimum water level      c.m/sec"
"      0.750 Maximum water level      c.m/sec"

```



```

"          Hydrograph volume      169.098    c.m"
"          0.007    0.020    0.019    0.019"
" 40      HYDROGRAPH Start - New Tributary"
"          2 Start - New Tributary"
"          0.007    0.000    0.019    0.019"

```

=====

CATCHMENT 6

=====

```

" 33      CATCHMENT 6"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          6 ID number"
"          40.000 % Impervious"
"          0.400 Total Area"
"          60.200 Flow length"
"          2.000 Overland Slope"
"          0.240 Pervious Area"
"          60.200 Pervious length"
"          2.000 Pervious slope"
"          0.160 Impervious Area"
"          60.200 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.258 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.850 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.033    0.000    0.019    0.019 c.m/sec"
"          Catchment 6 Pervious Impervious Total Area "
"          Surface Area 0.240 0.160 0.400 hectare"
"          Time of concentration 36.259 3.468 13.892 minutes"
"          Time to Centroid 138.336 87.562 103.703 minutes"
"          Rainfall depth 33.312 33.312 33.312 mm"
"          Rainfall volume 79.95 53.30 133.25 c.m"
"          Rainfall losses 24.708 5.619 17.072 mm"
"          Runoff depth 8.604 27.693 16.240 mm"
"          Runoff volume 20.65 44.31 64.96 c.m"
"          Maximum flow 0.004 0.032 0.033 c.m/sec"

```

```

" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.033    0.033    0.019    0.019"

```

```

" 54      POND DESIGN"
"          0.033 Current peak flow c.m/sec"
"          65.0 Hydrograph volume c.m/sec"
"          5. Number of stages"
"          0.000 Minimum water level c.m/sec"
"          0.750 Maximum water level c.m/sec"
"          0 Keep Design Data: 1 = True; 0 = False"
"          Level Discharge Volume"
"          0.000 0.000 0.0"
"          0.300 0.001 0.1"
"          0.450 0.001 4.7"
"          0.600 0.001 37.1"
"          0.750 0.001 75.0"
"          1. ORIFICES"
"          Orifice Orifice Orifice Number of"
"          invert coefficie diameter orifices"
"          0.000 0.600 0.025 1.000"
"          Peak outflow 0.001 c.m/sec"
"          Maximum level 0.661 metre"
"          Maximum storage 52.585 c.m"
"          Centroidal lag 9.870 hours"
"          0.033 0.033 0.001 0.019 c.m/sec"

```

```

" 40      HYDROGRAPH Combine 3"
"          6 Combine "
"          3 Node #"
"          "
"          Maximum flow 0.020 c.m/sec"
"          Hydrograph volume 234.073 c.m"
"          0.033 0.033 0.001 0.020"
" 40      HYDROGRAPH Confluence 3"
"          7 Confluence "
"          3 Node #"
"          "
"          Maximum flow 0.020 c.m/sec"
"          Hydrograph volume 234.073 c.m"
"          0.033 0.020 0.001 0.000"

```

=====

CATCHMENT 7

=====

```

" 33      CATCHMENT 7"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          7 ID number"
"          50.000 % Impervious"
"          0.070 Total Area"
"          5.750 Flow length"
"          2.000 Overland Slope"
"          0.035 Pervious Area"
"          5.750 Pervious length"
"          2.000 Pervious slope"
"          0.035 Impervious Area"
"          5.750 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"

```

```

"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.039 metre"
"      Velocity 0.222 m/sec"
"      Channel capacity 3.967 c.m/sec"
"      Critical depth 0.020 metre"
" 53 ROUTE 96"
"      96.00 Reach length( metre)"
"      0.452 X-factor <= 0.5"
"      162.278 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      300.000 Routing time step ( seconds)"
"      2 No. of sub-reaches"
"      Peak outflow 0.013 c.m/sec"
"      0.014 0.014 0.013 0.024 c.m/sec"
" 40 HYDROGRAPH Combine 4"
"      6 Combine "
"      4 Node #"
"      Maximum flow 0.037 c.m/sec"
"      Hydrograph volume 267.877 c.m"
"      0.014 0.014 0.013 0.037"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.014 0.000 0.013 0.037"
=====
CATCHMENT 9
=====
" 33 CATCHMENT 9"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      9 ID number"
"      40.000 % Impervious"
"      0.400 Total Area"
"      60.200 Flow length"
"      2.000 Overland Slope"
"      0.240 Pervious Area"
"      60.200 Pervious length"
"      2.000 Pervious slope"
"      0.160 Impervious Area"
"      60.200 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.033 0.000 0.013 0.037 c.m/sec"
"      Catchment 9 Pervious Impervious Total Area "
"      Surface Area 0.240 0.160 0.400 hectare"
"      Time of concentration 36.259 3.468 13.892 minutes"
"      Time to Centroid 138.336 87.562 103.703 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 79.95 53.30 133.25 c.m"
"      Rainfall losses 24.708 5.619 17.072 mm"
"      Runoff depth 8.604 27.693 16.240 mm"
"      Runoff volume 20.65 44.31 64.96 c.m"
"      Maximum flow 0.004 0.032 0.033 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.033 0.033 0.013 0.037"
=====
CATCHMENT 10
=====
" 33 CATCHMENT 10"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      10 ID number"
"      40.000 % Impervious"
"      0.600 Total Area"
"      89.800 Flow length"
"      2.000 Overland Slope"
"      0.360 Pervious Area"
"      89.800 Pervious length"
"      2.000 Pervious slope"
"      0.240 Impervious Area"
"      89.800 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"

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"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.014      0.000      0.038      0.038 c.m/sec"
"      Catchment 11      Pervious      Impervious      Total Area "
"      Surface Area      0.060      0.060      0.120      hectare"
"      Time of concentration      8.860      0.847      2.779      minutes"
"      Time to Centroid      105.679      83.592      88.917      minutes"
"      Rainfall depth      33.312      33.312      33.312      mm"
"      Rainfall volume      19.99      19.99      39.97      c.m"
"      Rainfall losses      24.731      6.304      15.518      mm"
"      Runoff depth      8.581      27.008      17.794      mm"
"      Runoff volume      5.15      16.20      21.35      c.m"
"      Maximum flow      0.002      0.013      0.014      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4      Add Runoff "
"      0.014      0.014      0.038      0.038"
" 52      CHANNEL DESIGN"
"      0.014 Current peak flow      c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth      metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth      metre"
"      0.500 Gradient      %"
"      Depth of flow      0.039      metre"
"      Velocity      0.222      m/sec"
"      Channel capacity      3.967      c.m/sec"
"      Critical depth      0.020      metre"
" 53      ROUTE 96"
"      96.00 Reach length( metre)"
"      0.452 X-factor <= 0.5"
"      162.278 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      300.000 Routing time step ( seconds)"
"      2 No. of sub-reaches"
"      Peak outflow      0.013      c.m/sec"
"      0.014      0.014      0.013      0.038 c.m/sec"
" 40      HYDROGRAPH Combine 5"
"      6 Combine "
"      5 Node #"
"      "
"      Maximum flow      0.051      c.m/sec"
"      Hydrograph volume      362.869      c.m"
"      0.014      0.014      0.013      0.051"
" 40      HYDROGRAPH Confluence 5"
"      7 Confluence "
"      5 Node #"
"      "
"      Maximum flow      0.051      c.m/sec"
"      Hydrograph volume      362.869      c.m"
"      0.014      0.051      0.013      0.000"
=====
CATCHMENT 12
=====
" 33      CATCHMENT 12"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      12 ID number"
"      50.000 % Impervious"
"      0.070 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.035 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.035 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.008      0.051      0.013      0.000 c.m/sec"
"      Catchment 12      Pervious      Impervious      Total Area "
"      Surface Area      0.035      0.035      0.070      hectare"
"      Time of concentration      8.860      0.847      2.779      minutes"
"      Time to Centroid      105.679      83.592      88.917      minutes"
"      Rainfall depth      33.312      33.312      33.312      mm"
"      Rainfall volume      11.66      11.66      23.32      c.m"
"      Rainfall losses      24.731      6.304      15.518      mm"
"      Runoff depth      8.581      27.008      17.794      mm"
"      Runoff volume      3.00      9.45      12.46      c.m"

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"      0.036      0.036      0.001      0.052 c.m/sec"
" 40      HYDROGRAPH      Combine      6"
"      6      Combine "
"      6      Node #"
"      "
"      Maximum flow      0.053      c.m/sec"
"      Hydrograph volume      442.894      c.m"
"      0.036      0.036      0.001      0.053"
" 40      HYDROGRAPH      Confluence      6"
"      7      Confluence "
"      6      Node #"
"      "
"      Maximum flow      0.053      c.m/sec"
"      Hydrograph volume      442.894      c.m"
"      0.036      0.053      0.001      0.000"
=====
CATCHMENT 14
=====
" 33      CATCHMENT 14"
"      1      Triangular SCS"
"      1      Equal length"
"      1      SCS method"
"      14      ID number"
"      50.000      % Impervious"
"      0.060      Total Area"
"      5.750      Flow length"
"      2.000      Overland Slope"
"      0.030      Pervious Area"
"      5.750      Pervious length"
"      2.000      Pervious slope"
"      0.030      Impervious Area"
"      5.750      Impervious length"
"      2.000      Impervious slope"
"      0.250      Pervious Manning 'n'"
"      81.000      Pervious SCS Curve No."
"      0.258      Pervious Runoff coefficient"
"      0.100      Pervious Ia/S coefficient"
"      5.958      Pervious Initial abstraction"
"      0.015      Impervious Manning 'n'"
"      98.000      Impervious SCS Curve No."
"      0.850      Impervious Runoff coefficient"
"      0.100      Impervious Ia/S coefficient"
"      0.518      Impervious Initial abstraction"
"      0.007      0.053      0.001      0.000 c.m/sec"
"      Catchment 14      Pervious      Impervious      Total Area      "
"      Surface Area      0.030      0.030      0.060      hectare"
"      Time of concentration      8.860      0.847      2.779      minutes"
"      Time to Centroid      105.679      83.592      88.917      minutes"
"      Rainfall depth      33.312      33.312      33.312      mm"
"      Rainfall volume      9.99      9.99      19.99      c.m"
"      Rainfall losses      24.731      6.304      15.518      mm"
"      Runoff depth      8.581      27.008      17.794      mm"
"      Runoff volume      2.57      8.10      10.68      c.m"
"      Maximum flow      0.001      0.007      0.007      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4      Add Runoff "
"      0.007      0.056      0.001      0.000"
" 52      CHANNEL DESIGN"
"      0.056      Current peak flow      c.m/sec"
"      0.035      Manning 'n'"
"      0.      Cross-section type: 0=trapezoidal; 1=general"
"      1.500      Basewidth      metre"
"      2.000      Left bank slope"
"      2.000      Right bank slope"
"      0.900      Channel depth      metre"
"      0.420      Gradient      %"
"      Depth of flow      0.095      metre"
"      Velocity      0.353      m/sec"
"      Channel capacity      3.636      c.m/sec"
"      Critical depth      0.051      metre"
" 53      ROUTE 56"
"      56.10      Reach length( metre)"
"      0.382      X-factor <= 0.5"
"      119.226      K-lag ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag ( seconds)"
"      0.500      Beta weighting factor"
"      100.000      Routing time step ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      0.052      c.m/sec"
"      0.007      0.056      0.052      0.000 c.m/sec"
" 40      HYDROGRAPH      Combine      7"
"      6      Combine "
"      7      Node #"
"      "
"      Maximum flow      0.052      c.m/sec"
"      Hydrograph volume      453.306      c.m"
"      0.007      0.056      0.052      0.052"
" 40      HYDROGRAPH Start - New Tributary"
"      2      Start - New Tributary"
"      0.007      0.000      0.052      0.052"
=====
CATCHMENT 15
=====
" 33      CATCHMENT 15"
"      1      Triangular SCS"
"      1      Equal length"
"      1      SCS method"
"      15      ID number"
"      40.000      % Impervious"
"      0.460      Total Area"

```

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"          Rainfall volume      9.99      9.99      19.99      c.m"
"          Rainfall losses      24.731    6.304    15.518    mm"
"          Runoff depth         8.581    27.008    17.794    mm"
"          Runoff volume        2.57     8.10     10.68     c.m"
"          Maximum flow         0.001    0.007    0.007     c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"              0.007      0.056      0.001      0.000"
" 52      CHANNEL DESIGN"
"          0.056 Current peak flow c.m/sec"
"          0.035 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          1.500 Basewidth metre"
"          2.000 Left bank slope"
"          2.000 Right bank slope"
"          0.900 Channel depth metre"
"          0.420 Gradient %"
"          Depth of flow              0.095 metre"
"          Velocity                   0.353 m/sec"
"          Channel capacity            3.636 c.m/sec"
"          Critical depth              0.051 metre"
" 53      ROUTE 56"
"          56.10 Reach length( metre)"
"          0.382 X-factor <= 0.5"
"          119.275 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500 Beta weighting factor"
"          100.000 Routing time step ( seconds)"
"          1 No. of sub-reaches"
"          Peak outflow              0.056 c.m/sec"
"              0.007      0.056      0.056      0.000 c.m/sec"
" 40      HYDROGRAPH Combine 8"
"          6 Combine "
"          8 Node #"
"          "
"          Maximum flow              0.056 c.m/sec"
"          Hydrograph volume          532.031 c.m"
"              0.007      0.056      0.056      0.056"
" 40      HYDROGRAPH Start - New Tributary"
"          2 Start - New Tributary"
"              0.007      0.000      0.056      0.056"
"=====
"          CATCHMENT 17
"=====
" 33      CATCHMENT 17"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          17 ID number"
"          40.000 % Impervious"
"          0.460 Total Area"
"          56.100 Flow length"
"          2.000 Overland Slope"
"          0.276 Pervious Area"
"          56.100 Pervious length"
"          2.000 Pervious slope"
"          0.184 Impervious Area"
"          56.100 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.258 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.850 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"              0.038      0.000      0.056      0.056 c.m/sec"
"          Catchment 17 Pervious Impervious Total Area "
"          Surface Area      0.276      0.184      0.460 hectare"
"          Time of concentration 34.756      3.324      13.302 minutes"
"          Time to Centroid 136.551      87.301      102.935 minutes"
"          Rainfall depth      33.312      33.312      33.312 mm"
"          Rainfall volume      91.94      61.29      153.23 c.m"
"          Rainfall losses      24.711      5.571      17.055 mm"
"          Runoff depth          8.601      27.741      16.257 mm"
"          Runoff volume          23.74      51.04      74.78 c.m"
"          Maximum flow          0.005      0.037      0.038 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"              0.038      0.038      0.056      0.056"
" 54      POND DESIGN"
"          0.038 Current peak flow c.m/sec"
"          75.0 Hydrograph volume c.m/sec"
"          5. Number of stages"
"          0.000 Minimum water level c.m/sec"
"          0.750 Maximum water level c.m/sec"
"          0 Keep Design Data: 1 = True; 0 = False"
"              Level Discharge Volume"
"              0.000      0.000      0.0"
"              0.300      0.001      0.1"
"              0.450      0.001      4.7"
"              0.600      0.001      37.1"
"              0.750      0.001      75.0"
"          1. ORIFICES"
"              Orifice Orifice Number of"
"              invert coefficient diameter orifices"
"              0.000      0.600      0.025      1.000"

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"      1 SCS method"
"      19 ID number"
"  40.000 % Impervious"
"      0.460 Total Area"
"  56.100 Flow length"
"      2.000 Overland Slope"
"      0.276 Pervious Area"
"  56.100 Pervious length"
"      2.000 Pervious slope"
"      0.184 Impervious Area"
"  56.100 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"  81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"  98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.038 0.000 0.058 0.058 c.m/sec"
"      Catchment 19 Pervious Impervious Total Area "
"      Surface Area 0.276 0.184 0.460 hectare"
"      Time of concentration 34.756 3.324 13.302 minutes"
"      Time to Centroid 136.551 87.301 102.935 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 91.94 61.29 153.23 c.m"
"      Rainfall losses 24.711 5.571 17.055 mm"
"      Runoff depth 8.601 27.741 16.257 mm"
"      Runoff volume 23.74 51.04 74.78 c.m"
"      Maximum flow 0.005 0.037 0.038 c.m/sec"
"  40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.038 0.038 0.058 0.058"
"  54 POND DESIGN"
"      0.038 Current peak flow c.m/sec"
"      75.0 Hydrograph volume c.m/sec"
"      5. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.750 0.001 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.001 c.m/sec"
"      Maximum level 0.698 metre"
"      Maximum storage 61.910 c.m"
"      Centroidal lag 10.917 hours"
"      0.038 0.038 0.001 0.058 c.m/sec"
"  40 HYDROGRAPH Combine 9"
"      6 Combine "
"      9 Node #"
"      "
"      Maximum flow 0.059 c.m/sec"
"      Hydrograph volume 679.132 c.m"
"      0.038 0.038 0.001 0.059"
"  40 HYDROGRAPH Confluence 9"
"      7 Confluence "
"      9 Node #"
"      "
"      Maximum flow 0.059 c.m/sec"
"      Hydrograph volume 679.132 c.m"
"      0.038 0.059 0.001 0.000"
"=====
" CATCHMENT 20
"=====
" 33 CATCHMENT 20"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      20 ID number"
"      50.000 % Impervious"
"      0.060 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.030 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.030 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.007 0.059 0.001 0.000 c.m/sec"
"      Catchment 20 Pervious Impervious Total Area "

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```

"      1.  ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.001 c.m/sec"
"      Maximum level 0.698 metre"
"      Maximum storage 61.910 c.m"
"      Centroidal lag 10.917 hours"
"      0.038 0.038 0.001 0.060 c.m/sec"
" 40  HYDROGRAPH Combine 10"
"      6 Combine "
"      10 Node #"
"      Maximum flow 0.061 c.m/sec"
"      Hydrograph volume 757.772 c.m"
"      0.038 0.038 0.001 0.061"
" 40  HYDROGRAPH Confluence 10"
"      7 Confluence "
"      10 Node #"
"      Maximum flow 0.061 c.m/sec"
"      Hydrograph volume 757.772 c.m"
"      0.038 0.061 0.001 0.000"
" 52  CHANNEL DESIGN"
"      0.061 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      1.000 Gradient %"
"      Depth of flow 0.077 metre"
"      Velocity 0.481 m/sec"
"      Channel capacity 5.610 c.m/sec"
"      Critical depth 0.054 metre"
" 53  ROUTE 17"
"      17.00 Reach length( metre)"
"      0.366 X-factor <= 0.5"
"      26.486 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      33.333 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.061 c.m/sec"
"      0.038 0.061 0.061 0.000 c.m/sec"
" 40  HYDROGRAPH Combine 11"
"      6 Combine "
"      11 Node #"
"      Maximum flow 0.061 c.m/sec"
"      Hydrograph volume 757.598 c.m"
"      0.038 0.061 0.061 0.061"
" 40  HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.038 0.000 0.061 0.061"
" 33  CATCHMENT 24"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      24 ID number"
"      50.000 % Impervious"
"      0.100 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.050 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.050 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.011 0.000 0.061 0.061 c.m/sec"
"      Catchment 24 Pervious Impervious Total Area "
"      Surface Area 0.050 0.050 0.100 hectare"
"      Time of concentration 8.860 0.847 2.779 minutes"
"      Time to Centroid 105.679 83.592 88.917 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 16.66 16.66 33.31 c.m"
"      Rainfall losses 24.731 6.304 15.518 mm"
"      Runoff depth 8.581 27.008 17.794 mm"
"      Runoff volume 4.29 13.50 17.79 c.m"
"      Maximum flow 0.002 0.011 0.011 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.011 0.011 0.061 0.061"
" 52  CHANNEL DESIGN"
"      0.011 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"

```

CATCHMENT 26

```

=====
" 33 CATCHMENT 26"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      26 ID number"
"      50.000 % Impervious"
"      0.100 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.050 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.050 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.011 0.000 0.001 0.011 c.m/sec"
"      Catchment 26 Pervious Impervious Total Area "
"      Surface Area 0.050 0.050 0.100 hectare"
"      Time of concentration 8.860 0.847 2.779 minutes"
"      Time to Centroid 105.679 83.592 88.917 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 16.66 16.66 33.31 c.m"
"      Rainfall losses 24.731 6.304 15.518 mm"
"      Runoff depth 8.581 27.008 17.794 mm"
"      Runoff volume 4.29 13.50 17.79 c.m"
"      Maximum flow 0.002 0.011 0.011 c.m/sec"
"      HYDROGRAPH Add Runoff "
" 40 4 Add Runoff "
"      0.011 0.011 0.001 0.011"
" 52 CHANNEL DESIGN"
"      0.011 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.035 metre"
"      Velocity 0.207 m/sec"
"      Channel capacity 3.967 c.m/sec"
"      Critical depth 0.018 metre"
" 53 ROUTE 78"
"      78.00 Reach length( metre)"
"      0.474 X-factor <= 0.5"
"      282.444 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.010 c.m/sec"
"      0.011 0.011 0.010 0.011 c.m/sec"
" 40 HYDROGRAPH Combine 12"
"      6 Combine "
"      12 Node #"
"      "
"      Maximum flow 0.021 c.m/sec"
"      Hydrograph volume 104.833 c.m"
"      0.011 0.011 0.010 0.021"
" 40 HYDROGRAPH Confluence 12"
"      7 Confluence "
"      12 Node #"
"      "
"      Maximum flow 0.021 c.m/sec"
"      Hydrograph volume 104.833 c.m"
"      0.011 0.021 0.010 0.000"
" 51 PIPE DESIGN"
"      0.021 Current peak flow c.m/sec"
"      0.015 Manning 'n'"
"      0.450 Diameter metre"
"      0.500 Gradient %"
"      Depth of flow 0.106 metre"
"      Velocity 0.742 m/sec"
"      Pipe capacity 0.175 c.m/sec"
"      Critical depth 0.098 metre"
" 53 ROUTE 20"
"      20.00 Reach length( metre)"
"      0.229 X-factor <= 0.5"
"      20.214 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      30.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.020 c.m/sec"
"      0.011 0.021 0.020 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 13"

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"      73.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.031 0.000 0.010 0.030 c.m/sec"
"      Catchment 28 Pervious Impervious Total Area "
"      Surface Area 0.228 0.152 0.380 hectare"
"      Time of concentration 40.705 3.893 15.556 minutes"
"      Time to Centroid 143.648 88.168 105.746 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 75.95 50.63 126.58 c.m"
"      Rainfall losses 24.709 5.488 17.021 mm"
"      Runoff depth 8.602 27.824 16.291 mm"
"      Runoff volume 19.61 42.29 61.91 c.m"
"      Maximum flow 0.004 0.031 0.031 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.031 0.031 0.010 0.030"
" 54 POND DESIGN"
"      0.031 Current peak flow c.m/sec"
"      62.0 Hydrograph volume c.m/sec"
"      5. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"          Level Discharge Volume"
"          0.000 0.000 0.0"
"          0.188 0.001 1.0"
"          0.375 0.001 4.0"
"          0.563 0.001 30.0"
"          0.750 0.001 70.0"
"      Peak outflow 0.001 c.m/sec"
"      Maximum level 1.#IO metre"
"      Maximum storage 1.#IO c.m"
"      Centroidal lag 9.435 hours"
"          0.031 0.031 0.001 0.030 c.m/sec"
" 40 HYDROGRAPH Combine 13"
"      6 Combine "
"      13 Node #"
"          Maximum flow 0.031 c.m/sec"
"          Hydrograph volume 184.506 c.m"
"          0.031 0.031 0.001 0.031"
" 40 HYDROGRAPH Confluence 13"
"      7 Confluence "
"      13 Node #"
"          Maximum flow 0.031 c.m/sec"
"          Hydrograph volume 184.506 c.m"
"          0.031 0.031 0.001 0.000"
"=====
" CATCHMENT 29
"=====
" 33 CATCHMENT 29"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      29 ID number"
"      50.000 % Impervious"
"      0.170 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.085 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.085 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.019 0.031 0.001 0.000 c.m/sec"
"      Catchment 29 Pervious Impervious Total Area "
"      Surface Area 0.085 0.085 0.170 hectare"
"      Time of concentration 8.860 0.847 2.779 minutes"
"      Time to Centroid 105.679 83.592 88.917 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 28.32 28.32 56.63 c.m"
"      Rainfall losses 24.731 6.304 15.518 mm"
"      Runoff depth 8.581 27.008 17.794 mm"
"      Runoff volume 7.29 22.96 30.25 c.m"
"      Maximum flow 0.003 0.019 0.019 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.019 0.046 0.001 0.000"
" 52 CHANNEL DESIGN"
"      0.046 Current peak flow c.m/sec"

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"          0.009    0.000    0.045    0.045"
=====
CATCHMENT 31
=====
" 33      CATCHMENT 31"
"          1    Triangular SCS"
"          1    Equal length"
"          1    SCS method"
"          31    ID number"
"          0.000 % Impervious"
"          0.100 Total Area"
"          17.000 Flow length"
"          2.000 Overland Slope"
"          0.100 Pervious Area"
"          17.000 Pervious length"
"          2.000 Pervious slope"
"          0.000 Impervious Area"
"          17.000 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.258 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.850 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.003    0.000    0.045    0.045 c.m/sec"
"          Catchment 31    Pervious    Impervious    Total Area "
"          Surface Area    0.100    0.000    0.100    hectare"
"          Time of concentration    16.979    1.624    16.979    minutes"
"          Time to Centroid    115.358    84.509    115.358    minutes"
"          Rainfall depth    33.312    33.312    33.312    mm"
"          Rainfall volume    33.31    0.00    33.31    c.m"
"          Rainfall losses    24.712    5.402    24.712    mm"
"          Runoff depth    8.600    27.910    8.600    mm"
"          Runoff volume    8.60    0.00    8.60    c.m"
"          Maximum flow    0.003    0.000    0.003    c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4    Add Runoff "
"          0.003    0.003    0.045    0.045"
=====
CATCHMENT 32
=====
" 33      CATCHMENT 32"
"          1    Triangular SCS"
"          1    Equal length"
"          1    SCS method"
"          32    ID number"
"          40.000 % Impervious"
"          0.440 Total Area"
"          59.700 Flow length"
"          2.000 Overland Slope"
"          0.264 Pervious Area"
"          59.700 Pervious length"
"          2.000 Pervious slope"
"          0.176 Impervious Area"
"          59.700 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.258 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.850 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.036    0.003    0.045    0.045 c.m/sec"
"          Catchment 32    Pervious    Impervious    Total Area "
"          Surface Area    0.264    0.176    0.440    hectare"
"          Time of concentration    36.078    3.451    13.821    minutes"
"          Time to Centroid    138.121    87.530    103.610    minutes"
"          Rainfall depth    33.312    33.312    33.312    mm"
"          Rainfall volume    87.94    58.63    146.57    c.m"
"          Rainfall losses    24.708    5.611    17.069    mm"
"          Runoff depth    8.604    27.700    16.243    mm"
"          Runoff volume    22.71    48.75    71.47    c.m"
"          Maximum flow    0.005    0.036    0.036    c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4    Add Runoff "
"          0.036    0.038    0.045    0.045"
" 54      POND DESIGN"
"          0.038 Current peak flow    c.m/sec"
"          81.0 Hydrograph volume    c.m/sec"
"          5. Number of stages"
"          0.000 Minimum water level    c.m/sec"
"          0.750 Maximum water level    c.m/sec"
"          0 Keep Design Data: 1 = True; 0 = False"
"          Level Discharge    Volume"
"          0.000    0.000    0.0"
"          0.300    0.001    0.1"
"          0.450    0.001    4.7"
"          0.600    0.001    37.1"
"          0.750    0.001    75.0"
"          1. ORIFICES"
"          Orifice    Orifice    Orifice Number of"
"          invert coefficient    diameter    orifices"
"          0.000    0.600    0.025    1.000"

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"      1 SCS method"
"      34 ID number"
"      0.000 % Impervious"
"      0.100 Total Area"
"     17.000 Flow length"
"      2.000 Overland Slope"
"      0.100 Pervious Area"
"     17.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"     17.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"     81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"     98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.003 0.000 0.049 0.049 c.m/sec"
"      Catchment 34 Pervious Impervious Total Area "
"      Surface Area 0.100 0.000 0.100 hectare"
"      Time of concentration 16.979 1.624 16.979 minutes"
"      Time to Centroid 115.358 84.509 115.358 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 33.31 0.00 33.31 c.m"
"      Rainfall losses 24.712 5.402 24.712 mm"
"      Runoff depth 8.600 27.910 8.600 mm"
"      Runoff volume 8.60 0.00 8.60 c.m"
"      Maximum flow 0.003 0.000 0.003 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.003 0.003 0.049 0.049"
=====
CATCHMENT 35
=====
" 33 CATCHMENT 35"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      35 ID number"
"     40.000 % Impervious"
"      0.440 Total Area"
"     60.000 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"     60.000 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"     60.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"     81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"     98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.036 0.003 0.049 0.049 c.m/sec"
"      Catchment 35 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"
"      Time of concentration 36.186 3.461 13.863 minutes"
"      Time to Centroid 138.250 87.549 103.665 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 87.94 58.63 146.57 c.m"
"      Rainfall losses 24.708 5.616 17.071 mm"
"      Runoff depth 8.604 27.696 16.241 mm"
"      Runoff volume 22.71 48.75 71.46 c.m"
"      Maximum flow 0.005 0.036 0.036 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.036 0.038 0.049 0.049"
" 54 POND DESIGN"
"      0.038 Current peak flow c.m/sec"
"      81.0 Hydrograph volume c.m/sec"
"      5. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.750 0.001 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.001 c.m/sec"
"      Maximum level 0.718 metre"
"      Maximum storage 66.863 c.m"
"      Centroidal lag 11.401 hours"
"      0.036 0.038 0.001 0.049 c.m/sec"
" 40 HYDROGRAPH Combine 15"
"      6 Combine "

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"      17.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"      17.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.003 0.000 0.052 0.052 c.m/sec"
"      Catchment 37 Pervious Impervious Total Area "
"      Surface Area 0.100 0.000 0.100 hectare"
"      Time of concentration 16.979 1.624 16.979 minutes"
"      Time to Centroid 115.358 84.509 115.358 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 33.31 0.00 33.31 c.m"
"      Rainfall losses 24.712 5.402 24.712 mm"
"      Runoff depth 8.600 27.910 8.600 mm"
"      Runoff volume 8.60 0.00 8.60 c.m"
"      Maximum flow 0.003 0.000 0.003 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.003 0.003 0.052 0.052"
=====
CATCHMENT 38
=====
" 33 CATCHMENT 38"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      38 ID number"
"      40.000 % Impervious"
"      0.440 Total Area"
"      60.000 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"      60.000 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"      60.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.036 0.003 0.052 0.052 c.m/sec"
"      Catchment 38 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"
"      Time of concentration 36.186 3.461 13.863 minutes"
"      Time to Centroid 138.250 87.549 103.665 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 87.94 58.63 146.57 c.m"
"      Rainfall losses 24.708 5.616 17.071 mm"
"      Runoff depth 8.604 27.696 16.241 mm"
"      Runoff volume 22.71 48.75 71.46 c.m"
"      Maximum flow 0.005 0.036 0.036 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.036 0.038 0.052 0.052"
" 54 POND DESIGN"
"      0.038 Current peak flow c.m/sec"
"      81.0 Hydrograph volume c.m/sec"
"      5. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.750 0.001 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.001 c.m/sec"
"      Maximum level 0.718 metre"
"      Maximum storage 66.863 c.m"
"      Centroidal lag 11.401 hours"
"      0.036 0.038 0.001 0.052 c.m/sec"
" 40 HYDROGRAPH Combine 16"
"      6 Combine "
"      16 Node #"
"      Maximum flow 0.053 c.m/sec"
"      Hydrograph volume 461.514 c.m"
"      0.036 0.038 0.001 0.053"
" 40 HYDROGRAPH Confluence 16"
"      7 Confluence "

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"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.003 0.000 0.054 0.054 c.m/sec"
"      Catchment 40 Pervious Impervious Total Area "
"      Surface Area 0.100 0.000 0.100 hectare"
"      Time of concentration 16.979 1.624 16.979 minutes"
"      Time to Centroid 115.358 84.509 115.358 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 33.31 0.00 33.31 c.m"
"      Rainfall losses 24.712 5.402 24.712 mm"
"      Runoff depth 8.600 27.910 8.600 mm"
"      Runoff volume 8.60 0.00 8.60 c.m"
"      Maximum flow 0.003 0.000 0.003 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.003 0.003 0.054 0.054"
=====
CATCHMENT 41
=====
" 33 CATCHMENT 41"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      41 ID number"
"      40.000 % Impervious"
"      0.440 Total Area"
"      60.000 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"      60.000 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"      60.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.036 0.003 0.054 0.054 c.m/sec"
"      Catchment 41 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"
"      Time of concentration 36.186 3.461 13.863 minutes"
"      Time to Centroid 138.250 87.549 103.665 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 87.94 58.63 146.57 c.m"
"      Rainfall losses 24.708 5.616 17.071 mm"
"      Runoff depth 8.604 27.696 16.241 mm"
"      Runoff volume 22.71 48.75 71.46 c.m"
"      Maximum flow 0.005 0.036 0.036 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.036 0.038 0.054 0.054"
" 54 POND DESIGN"
"      0.038 Current peak flow c.m/sec"
"      81.0 Hydrograph volume c.m/sec"
"      5. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.750 0.001 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.001 c.m/sec"
"      Maximum level 0.718 metre"
"      Maximum storage 66.863 c.m"
"      Centroidal lag 11.401 hours"
"      0.036 0.038 0.001 0.054 c.m/sec"
" 40 HYDROGRAPH Combine 17"
"      6 Combine "
"      17 Node #"
"      "
"      Maximum flow 0.055 c.m/sec"
"      Hydrograph volume 543.224 c.m"
"      0.036 0.038 0.001 0.055"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.036 0.000 0.001 0.055"
=====
CATCHMENT 42
=====
" 33 CATCHMENT 42"
"      1 Triangular SCS"
"      1 Equal length"

```



```

"      18  Node #"
"
"      Maximum flow          0.061  c.m/sec"
"      Hydrograph volume     562.638 c.m"
"      0.012  0.061  0.061  0.061"
" 40      HYDROGRAPH Start - New Tributary"
"      2  Start - New Tributary"
"      0.012  0.000  0.061  0.061"
=====
CATCHMENT 43
=====
" 33      CATCHMENT 43"
"      1  Triangular SCS"
"      1  Equal length"
"      1  SCS method"
"      43  ID number"
"      50.000 % Impervious"
"      0.110 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.055 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.055 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.012  0.000  0.061  0.061 c.m/sec"
"      Catchment 43      Pervious      Impervious      Total Area "
"      Surface Area      0.055      0.055      0.110      hectare"
"      Time of concentration 8.860      0.847      2.779      minutes"
"      Time to Centroid 105.679      83.592      88.917      minutes"
"      Rainfall depth      33.312      33.312      33.312      mm"
"      Rainfall volume      18.32      18.32      36.64      c.m"
"      Rainfall losses      24.731      6.304      15.518      mm"
"      Runoff depth      8.581      27.008      17.794      mm"
"      Runoff volume      4.72      14.85      19.57      c.m"
"      Maximum flow      0.002      0.012      0.012      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"      0.012  0.012  0.061  0.061"
" 52      CHANNEL DESIGN"
"      0.012 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      3.000 Gradient %"
"      Depth of flow      0.021      metre"
"      Velocity      0.374      m/sec"
"      Channel capacity      9.717      c.m/sec"
"      Critical depth      0.019      metre"
" 53      ROUTE 93"
"      93.00 Reach length( metre)"
"      0.498 X-factor <= 0.5"
"      186.651 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step ( seconds)"
"      1  No. of sub-reaches"
"      Peak outflow      0.011      c.m/sec"
"      0.012  0.012  0.011  0.061 c.m/sec"
" 40      HYDROGRAPH Combine 18"
"      6  Combine "
"      18  Node #"
"      "
"      Maximum flow      0.066      c.m/sec"
"      Hydrograph volume      582.212 c.m"
"      0.012  0.012  0.011  0.066"
" 40      HYDROGRAPH Confluence 18"
"      7  Confluence "
"      18  Node #"
"      "
"      Maximum flow      0.066      c.m/sec"
"      Hydrograph volume      582.212 c.m"
"      0.012  0.066  0.011  0.000"
" 52      CHANNEL DESIGN"
"      0.066 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.700 Gradient %"
"      Depth of flow      0.090      metre"
"      Velocity      0.441      m/sec"
"      Channel capacity      4.694      c.m/sec"
"      Critical depth      0.057      metre"

```

```

"      0.045 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.010 0.000 0.126 0.126 c.m/sec"
"      Catchment 22 Pervious Impervious Total Area "
"      Surface Area 0.045 0.045 0.090 hectare"
"      Time of concentration 8.860 0.847 2.779 minutes"
"      Time to Centroid 105.679 83.592 88.917 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 14.99 14.99 29.98 c.m"
"      Rainfall losses 24.731 6.304 15.518 mm"
"      Runoff depth 8.581 27.008 17.794 mm"
"      Runoff volume 3.86 12.15 16.01 c.m"
"      Maximum flow 0.002 0.010 0.010 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.010 0.010 0.126 0.126"
" 52 CHANNEL DESIGN"
"      0.010 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.033 metre"
"      Velocity 0.199 m/sec"
"      Channel capacity 3.967 c.m/sec"
"      Critical depth 0.017 metre"
" 53 ROUTE 32"
"      32.00 Reach length( metre)"
"      0.439 X-factor <= 0.5"
"      120.586 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.009 c.m/sec"
"      0.010 0.010 0.009 0.126 c.m/sec"
" 40 HYDROGRAPH Combine 19"
"      6 Combine "
"      19 Node #"
"      "
"      Maximum flow 0.130 c.m/sec"
"      Hydrograph volume 1355.317 c.m"
"      0.010 0.010 0.009 0.130"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.010 0.000 0.009 0.130"
=====
CATCHMENT 23
=====
" 33 CATCHMENT 23"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      23 ID number"
"      40.000 % Impervious"
"      0.440 Total Area"
"      56.300 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"      56.300 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"      56.300 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.258 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.850 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.036 0.000 0.009 0.130 c.m/sec"
"      Catchment 23 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"
"      Time of concentration 34.830 3.331 13.331 minutes"
"      Time to Centroid 136.639 87.314 102.972 minutes"
"      Rainfall depth 33.312 33.312 33.312 mm"
"      Rainfall volume 87.94 58.63 146.57 c.m"
"      Rainfall losses 24.711 5.573 17.056 mm"
"      Runoff depth 8.601 27.739 16.256 mm"
"      Runoff volume 22.71 48.82 71.53 c.m"
"      Maximum flow 0.005 0.036 0.036 c.m/sec"
" 40 HYDROGRAPH Add Runoff "

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"          Maximum flow          0.001    c.m/sec"
"          Hydrograph volume      71.968    c.m"
"          0.047    0.047    0.001    0.001"
" 40      HYDROGRAPH Start - New Tributary"
"          2      Start - New Tributary"
"          0.047    0.000    0.001    0.001"
=====
CATCHMENT 46
=====
" 33      CATCHMENT 46"
"          1      Triangular SCS"
"          1      Equal length"
"          1      SCS method"
"          46      ID number"
"          50.000  % Impervious"
"          0.110  Total Area"
"          5.750  Flow length"
"          2.000  Overland Slope"
"          0.055  Pervious Area"
"          5.750  Pervious length"
"          2.000  Pervious slope"
"          0.055  Impervious Area"
"          5.750  Impervious length"
"          2.000  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          81.000  Pervious SCS Curve No."
"          0.258  Pervious Runoff coefficient"
"          0.100  Pervious Ia/S coefficient"
"          5.958  Pervious Initial abstraction"
"          0.015  Impervious Manning 'n'"
"          98.000  Impervious SCS Curve No."
"          0.850  Impervious Runoff coefficient"
"          0.100  Impervious Ia/S coefficient"
"          0.518  Impervious Initial abstraction"
"          0.012    0.000    0.001    0.001 c.m/sec"
"          Catchment 46      Pervious      Impervious      Total Area "
"          Surface Area      0.055      0.055      0.110      hectare"
"          Time of concentration 8.860      0.847      2.779      minutes"
"          Time to Centroid 105.679      83.592      88.917      minutes"
"          Rainfall depth 33.312      33.312      33.312      mm"
"          Rainfall volume 18.32      18.32      36.64      c.m"
"          Rainfall losses 24.731      6.304      15.518      mm"
"          Runoff depth 8.581      27.008      17.794      mm"
"          Runoff volume 4.72      14.85      19.57      c.m"
"          Maximum flow 0.002      0.012      0.012      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4      Add Runoff "
"          0.012    0.012    0.001    0.001"
" 52      CHANNEL DESIGN"
"          0.012  Current peak flow    c.m/sec"
"          0.035  Manning 'n'"
"          0.    Cross-section type: 0=trapezoidal; 1=general"
"          1.500  Basewidth    metre"
"          2.000  Left bank slope"
"          2.000  Right bank slope"
"          0.900  Channel depth    metre"
"          0.500  Gradient    %"
"          Depth of flow          0.037    metre"
"          Velocity          0.215    m/sec"
"          Channel capacity          3.967    c.m/sec"
"          Critical depth          0.019    metre"
" 53      ROUTE 47"
"          47.00  Reach length( metre)"
"          0.454  X-factor <= 0.5"
"          164.182 K-lag ( seconds)"
"          0.000  Default(0) or user spec.(1) values used"
"          0.500  X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500  Beta weighting factor"
"          150.000 Routing time step ( seconds)"
"          1      No. of sub-reaches"
"          Peak outflow          0.011    c.m/sec"
"          0.012    0.012    0.011    0.001 c.m/sec"
" 40      HYDROGRAPH Combine 20"
"          6      Combine "
"          20     Node #"
"          "
"          Maximum flow          0.012    c.m/sec"
"          Hydrograph volume          91.542    c.m"
"          0.012    0.012    0.011    0.012"
" 40      HYDROGRAPH Confluence 20"
"          7      Confluence "
"          20     Node #"
"          "
"          Maximum flow          0.012    c.m/sec"
"          Hydrograph volume          91.542    c.m"
"          0.012    0.012    0.011    0.000"
" 52      CHANNEL DESIGN"
"          0.012  Current peak flow    c.m/sec"
"          0.035  Manning 'n'"
"          0.    Cross-section type: 0=trapezoidal; 1=general"
"          1.500  Basewidth    metre"
"          2.000  Left bank slope"
"          2.000  Right bank slope"
"          0.900  Channel depth    metre"
"          0.500  Gradient    %"
"          Depth of flow          0.036    metre"
"          Velocity          0.212    m/sec"
"          Channel capacity          3.967    c.m/sec"
"          Critical depth          0.018    metre"
" 53      ROUTE 35"
"          35.00  Reach length( metre)"

```

Hydrograph

Last rainfall:

Type: Channel: simple

Channel depth: 0.900 m

Gradient: 0.500

Manning n: 0.035

Depth of flow: 0.182 m

Flow capacity: 3.967 c.m/sec

Peak inflow: 0.139 c.m/sec

Reach length: 10 m

X-factor: 0.5

K lag: 14.8 seconds

Peak duration: 0.138 c.m/sec

☐ Specify values for X and K

Route: L100 Cancel

Using 1 reaches of length 10.0 m

Using 8 time steps of duration 37.5 seconds

Hydrograph

Total volume: 1514.07 c.m. Maximum flow: 0.138 c.m/sec 0.0 minutes

Time (minutes)	Flow (c.m/sec)
0.000	0.000
0.019	0.028
0.037	0.058
0.054	0.033
0.072	0.022
0.089	0.018
0.107	0.018
0.125	0.018
0.143	0.018
0.161	0.018
0.179	0.018
0.197	0.018
0.215	0.018
0.233	0.018
0.251	0.018
0.269	0.018
0.287	0.018
0.305	0.018
0.323	0.018
0.341	0.018
0.359	0.018
0.377	0.018
0.395	0.018
0.413	0.018
0.431	0.018
0.449	0.018
0.467	0.018
0.485	0.018
0.503	0.018
0.521	0.018
0.539	0.018
0.557	0.018
0.575	0.018
0.593	0.018
0.611	0.018
0.629	0.018
0.647	0.018
0.665	0.018
0.683	0.018
0.701	0.018
0.719	0.018
0.737	0.018
0.755	0.018
0.773	0.018
0.791	0.018
0.809	0.018
0.827	0.018
0.845	0.018
0.863	0.018
0.881	0.018
0.899	0.018
0.917	0.018
0.935	0.018
0.953	0.018
0.971	0.018
0.989	0.018
1.007	0.018
1.025	0.018
1.043	0.018
1.061	0.018
1.079	0.018
1.097	0.018
1.115	0.018
1.133	0.018
1.151	0.018
1.169	0.018
1.187	0.018
1.205	0.018
1.223	0.018
1.241	0.018
1.259	0.018
1.277	0.018
1.295	0.018
1.313	0.018
1.331	0.018
1.349	0.018
1.367	0.018
1.385	0.018
1.403	0.018
1.421	0.018
1.439	0.018
1.457	0.018
1.475	0.018
1.493	0.018
1.511	0.018
1.529	0.018
1.547	0.018
1.565	0.018
1.583	0.018
1.601	0.018
1.619	0.018
1.637	0.018
1.655	0.018
1.673	0.018
1.691	0.018
1.709	0.018
1.727	0.018
1.745	0.018
1.763	0.018
1.781	0.018
1.799	0.018
1.817	0.018
1.835	0.018
1.853	0.018
1.871	0.018
1.889	0.018
1.907	0.018
1.925	0.018
1.943	0.018
1.961	0.018
1.979	0.018
1.997	0.018
2.015	0.018
2.033	0.018
2.051	0.018
2.069	0.018
2.087	0.018
2.105	0.018
2.123	0.018
2.141	0.018
2.159	0.018
2.177	0.018
2.195	0.018
2.213	0.018
2.231	0.018
2.249	0.018
2.267	0.018
2.285	0.018
2.303	0.018
2.321	0.018
2.339	0.018
2.357	0.018
2.375	0.018
2.393	0.018
2.411	0.018
2.429	0.018
2.447	0.018
2.465	0.018
2.483	0.018
2.501	0.018
2.519	0.018
2.537	0.018
2.555	0.018
2.573	0.018
2.591	0.018
2.609	0.018
2.627	0.018
2.645	0.018
2.663	0.018
2.681	0.018
2.699	0.018
2.717	0.018
2.735	0.018
2.753	0.018
2.771	0.018
2.789	0.018
2.807	0.018
2.825	0.018
2.843	0.018
2.861	0.018
2.879	0.018
2.897	0.018
2.915	0.018
2.933	0.018
2.951	0.018
2.969	0.018
2.987	0.018
3.005	0.018
3.023	0.018
3.041	0.018
3.059	0.018
3.077	0.018
3.095	0.018
3.113	0.018
3.131	0.018
3.149	0.018
3.167	0.018
3.185	0.018
3.203	0.018
3.221	0.018
3.239	0.018
3.257	0.018
3.275	0.018
3.293	0.018
3.311	0.018
3.329	0.018
3.347	0.018
3.365	0.018
3.383	0.018
3.401	0.018
3.419	0.018
3.437	0.018
3.455	0.018
3.473	0.018
3.491	0.018
3.509	0.018
3.527	0.018
3.545	0.018
3.563	0.018
3.581	0.018
3.599	0.018
3.617	0.018
3.635	0.018
3.653	0.018
3.671	0.018
3.689	0.018
3.707	0.018
3.725	0.018
3.743	0.018
3.761	0.018
3.779	0.018
3.797	0.018
3.815	0.018
3.833	0.018
3.851	0.018
3.869	0.018
3.887	0.018
3.905	0.018
3.923	0.018
3.941	0.018
3.959	0.018
3.977	0.018
3.995	0.018
4.013	0.018
4.031	0.018
4.049	0.018
4.067	0.018
4.085	0.018
4.103	0.018
4.121	0.018
4.139	0.018
4.157	0.018
4.175	0.018
4.193	0.018
4.211	0.018
4.229	0.018
4.247	0.018
4.265	0.018
4.283	0.018
4.301	0.018
4.319	0.018
4.337	0.018
4.355	0.018
4.373	0.018
4.391	0.018
4.409	0.018
4.427	0.018
4.445	0.018
4.463	0.018
4.481	0.018
4.499	0.018
4.517	0.018
4.535	0.018
4.553	0.018
4.571	0.018
4.589	0.018
4.607	0.018
4.625	0.018
4.643	0.018
4.661	0.018
4.679	0.018
4.697	0.018
4.715	0.018
4.733	0.018
4.751	0.018
4.769	0.018
4.787	0.018
4.805	0.018
4.823	0.018
4.841	0.018
4.859	0.018
4.877	0.018
4.895	0.018
4.913	0.018
4.931	0.018
4.949	0.018
4.967	0.018
4.985	0.018
5.003	0.018
5.021	0.018
5.039	0.018
5.057	0.018
5.075	0.018
5.093	0.018
5.111	0.018
5.129	0.018
5.147	0.018
5.165	0.018
5.183	0.018
5.201	0.018
5.219	0.018
5.237	0.018
5.255	0.018
5.273	0.018
5.291	0.018
5.309	0.018
5.327	0.018
5.345	0.018
5.363	0.018
5.381	0.018
5.399	0.018
5.417	0.018
5.435	0.018
5.453	0.018
5.471	0.018
5.489	0.018
5.507	0.018
5.525	0.018
5.543	0.018
5.561	0.018
5.579	0.018
5.597	0.018
5.615	0.018
5.633	0.018
5.651	0.018
5.669	0.018
5.687	0.018
5.705	0.018
5.723	0.018
5.741	0.018
5.759	0.018
5.777	0.018
5.795	0.018
5.813	0.018
5.831	0.018
5.849	0.018
5.867	0.018
5.885	0.018
5.903	0.018
5.921	0.018
5.939	0.018
5.957	0.018
5.975	0.018
5.993	0.018
6.011	0.018
6.029	0.018
6.047	0.018
6.065	0.018
6.083	0.018
6.101	0.018
6.119	0.018
6.137	0.018
6.155	0.018
6.173	0.018
6.191	0.018
6.209	0.018
6.227	0.018
6.245	0.018
6.263	0.018
6.281	0.018
6.299	0.018
6.317	0.018
6.335	0.018
6.353	0.018
6.371	0.018
6.389	0.018
6.407	0.018
6.425	0.018
6.443	0.018
6.461	0.018
6.479	0.018
6.497	0.018
6.515	0.018
6.533	0.018
6.551	0.018
6.569	0.018
6.587	0.018
6.605	0.018
6.623	0.018
6.641	0.018
6.659	0.018
6.677	0.018
6.695	0.018
6.713	0.018
6.731	0.018
6.749	0.018
6.767	0.018
6.785	0.018
6.803	0.018
6.821	0.018
6.839	0.018
6.857	0.018
6.875	0.018
6.893	0.018
6.911	0.018
6.929	0.018
6.947	0.018
6.965	0.018
6.983	0.018
7.001	0.018
7.019	0.018
7.037	0.018
7.055	0.018
7.073	0.018
7.091	0.018
7.109	0.018
7.127	0.018
7.145	0.018
7.163	0.018
7.181	0.018
7.199	0.018
7.217	0.018
7.235	0.018
7.253	0.018
7.271	0.018
7.289	0.018
7.307	0.018
7.325	0.018
7.343	0.018
7.361	0.018
7.379	0.018
7.397	0.018
7.415	0.018
7.433	0.018
7.451	0.018
7.469	0.018
7.487	0.018
7.505	0.018
7.523	0.018
7.541	0.018
7.559	0.018
7.577	0.018
7.595	0.018
7.613	0.018
7.631	0.018
7.649	0.018
7.667	0.018
7.685	0.018
7.703	0.018
7.721	0.018
7.739	0.018
7.757	0.018
7.775	0.018
7.793	0.018
7.811	0.018
7.829	0.018
7.847	0.018
7.865	0.018
7.883	0.018
7.901	0.018
7.919	0.018
7.937	0.018
7.955	0.018
7.973	0.018
7.991	0.018
8.009	0.018
8.027	0.018
8.045	0.018
8.063	0.018
8.081	0.018
8.099	0.018
8.117	0.018
8.135	0.018
8.153	0.018
8.171	0.018
8.189	0.018
8.207	0.018
8.225	0.018
8.243	0.018
8.261	0.018
8.279	0.018
8.297	0.018
8.315	0.018
8.333	0.018
8.351	0.018
8.369	0.018
8.387	0.018
8.405	0.018
8.423	0.018
8.441	0.018
8.459	0.018
8.477	0.

APPENDIX E

MIDUSS OUTPUT

100 YEAR STORM – POST DEVELOPMENT

```

"          MIDUSS 98 Output----->"
"          MIDUSS 98 version number          1.00"
"          MIDUSS 98 created          October 10, 2001"
"          10 Units used:          ie METRIC"
"          Project filename:          G:\CLIENT\1133\1\MIDUSS\
"          Output filename:          100yrpst8.Out"
"          Licensee name:          Steve Brown"
"          Company          AGM Engineering Ltd."
"          Date & Time last used:          08/06/04 at 9:38:43 AM"
" 31      TIME PARAMETERS"
"          5.000 Time Step"
"          180.000 Max. Storm length"
"          1200.000 Max. Hydrograph"
=====
100 YEAR STORM
=====
" 32      STORM Chicago storm"
"          1 Chicago storm"
"          1499.530 Coefficient A"
"          3.297 Constant B"
"          0.794 Exponent C"
"          0.350 Fraction R"
"          180.000 Duration"
"          1.000 Time step multiplier"
"          Maximum intensity          264.015 mm/hr"
"          Total depth          71.801 mm"
"          6 100hyd Hydrograph extension used in this file"
=====
CATCHMENT 1
=====
" 33      CATCHMENT 1"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          1 ID number"
"          50.000 % Impervious"
"          0.090 Total Area"
"          5.750 Flow length"
"          2.000 Overland Slope"
"          0.045 Pervious Area"
"          5.750 Pervious length"
"          2.000 Pervious slope"
"          0.045 Impervious Area"
"          5.750 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.033 0.000 0.000 0.000 c.m/sec"
"          Catchment 1 Pervious Impervious Total Area "
"          Surface Area 0.045 0.045 0.090 hectare"
"          Time of concentration 4.259 0.566 1.893 minutes"
"          Time to Centroid 94.699 81.236 86.073 minutes"
"          Rainfall depth 71.801 71.801 71.801 mm"
"          Rainfall volume 32.31 32.31 64.62 c.m"
"          Rainfall losses 37.589 10.785 24.187 mm"
"          Runoff depth 34.212 61.017 47.614 mm"
"          Runoff volume 15.40 27.46 42.85 c.m"
"          Maximum flow 0.011 0.027 0.033 c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.033 0.033 0.000 0.000"
" 51      PIPE DESIGN"
"          0.033 Current peak flow c.m/sec"
"          0.013 Manning 'n'"
"          0.300 Diameter metre"
"          0.500 Gradient %"
"          Depth of flow 0.147 metre"
"          Velocity 0.958 m/sec"
"          Pipe capacity 0.068 c.m/sec"
"          Critical depth 0.139 metre"
" 53      ROUTE 10"
"          10.00 Reach length( metre)"
"          0.000 X-factor <= 0.5"
"          7.830 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.639 Beta weighting factor"
"          20.000 Routing time step ( seconds)"
"          1 No. of sub-reaches"
"          Peak outflow 0.032 c.m/sec"
"          0.033 0.033 0.032 0.000 c.m/sec"
" 40      HYDROGRAPH Next link "
"          5 Next link "
"          0.033 0.032 0.032 0.000"
" 52      CHANNEL DESIGN"
"          0.032 Current peak flow c.m/sec"
"          0.035 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          1.500 Basewidth metre"
"          2.000 Left bank slope"
"          2.000 Right bank slope"
"          0.900 Channel depth metre"
"          0.500 Gradient %"

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"          Maximum flow          0.062    c.m/sec"
"          Hydrograph volume     212.513  c.m"
"          0.091    0.062    0.050    0.000"
=====
CATCHMENT 3
=====
" 33 CATCHMENT 3"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      3 ID number"
"      50.000 % Impervious"
"      0.070 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.035 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.035 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.026    0.062    0.050    0.000 c.m/sec"
"      Catchment 3 Pervious Impervious Total Area "
"      Surface Area 0.035 0.035 0.070 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 25.13 25.13 50.26 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 11.97 21.36 33.33 c.m"
"      Maximum flow 0.008 0.021 0.026 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.026    0.069    0.050    0.000"
" 51 PIPE DESIGN"
"      0.069 Current peak flow c.m/sec"
"      0.014 Manning 'n'"
"      0.400 Diameter metre"
"      0.500 Gradient %"
"      Depth of flow 0.201 metre"
"      Velocity 1.090 m/sec"
"      Pipe capacity 0.137 c.m/sec"
"      Critical depth 0.187 metre"
" 53 ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      6.880 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.704 Beta weighting factor"
"      23.077 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.068 c.m/sec"
"          0.026    0.069    0.068    0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"          0.026    0.068    0.068    0.000"
" 52 CHANNEL DESIGN"
"      0.068 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.100 metre"
"      Velocity 0.398 m/sec"
"      Channel capacity 3.967 c.m/sec"
"      Critical depth 0.058 metre"
" 53 ROUTE 50"
"      50.20 Reach length( metre)"
"      0.383 X-factor <= 0.5"
"      94.506 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.060 c.m/sec"
"          0.026    0.068    0.060    0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2"
"      6 Combine "
"      2 Node #"
"      Maximum flow 0.060 c.m/sec"
"      Hydrograph volume 245.751 c.m"
"          0.026    0.068    0.060    0.060"
" 40 HYDROGRAPH Start - New Tributary"

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"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.022 0.106 0.050 0.000 c.m/sec"
"      Catchment 5 Pervious Impervious Total Area "
"      Surface Area 0.030 0.030 0.060 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 21.54 21.54 43.08 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 10.26 18.30 28.57 c.m"
"      Maximum flow 0.007 0.018 0.022 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.022 0.112 0.050 0.000"
" 51 PIPE DESIGN"
"      0.112 Current peak flow c.m/sec"
"      0.014 Manning 'n'"
"      0.400 Diameter metre"
"      0.500 Gradient %"
"      Depth of flow 0.276 metre"
"      Velocity 1.215 m/sec"
"      Pipe capacity 0.137 c.m/sec"
"      Critical depth 0.242 metre"
" 53 ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      6.174 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.829 Beta weighting factor"
"      30.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.111 c.m/sec"
"      0.022 0.112 0.111 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.022 0.111 0.111 0.000"
" 52 CHANNEL DESIGN"
"      0.111 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.133 metre"
"      Velocity 0.471 m/sec"
"      Channel capacity 3.967 c.m/sec"
"      Critical depth 0.079 metre"
" 53 ROUTE 50"
"      50.20 Reach length( metre)"
"      0.346 X-factor <= 0.5"
"      79.978 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.108 c.m/sec"
"      0.022 0.111 0.108 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3"
"      6 Combine "
"      3 Node #"
"      "
"      Maximum flow 0.108 c.m/sec"
"      Hydrograph volume 443.824 c.m"
"      0.022 0.111 0.108 0.108"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.022 0.000 0.108 0.108"
=====
CATCHMENT 6
=====
" 33 CATCHMENT 6"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      6 ID number"
"      40.000 % Impervious"
"      0.400 Total Area"
"      60.200 Flow length"
"      2.000 Overland Slope"
"      0.240 Pervious Area"
"      60.200 Pervious length"
"      2.000 Pervious slope"
"      0.160 Impervious Area"
"      60.200 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"

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"      0.450 Diameter      metre"
"      0.500 Gradient      %"
"      Depth of flow      0.331 metre"
"      Velocity            1.242 m/sec"
"      Pipe capacity       0.175 c.m/sec"
"      Critical depth      0.277 metre"
" 53 ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      6.040 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.859 Beta weighting factor"
"      37.500 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.156 c.m/sec"
"      0.026 0.156 0.156 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.026 0.156 0.156 0.000"
" 52 CHANNEL DESIGN"
"      0.156 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.650 Gradient %"
"      Depth of flow      0.150 metre"
"      Velocity            0.575 m/sec"
"      Channel capacity    4.523 c.m/sec"
"      Critical depth      0.099 metre"
" 53 ROUTE 50"
"      50.20 Reach length( metre)"
"      0.367 X-factor <= 0.5"
"      65.499 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      75.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.154 c.m/sec"
"      0.026 0.156 0.154 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 4"
"      6 Combine "
"      4 Node #"
"      "
"      Maximum flow      0.154 c.m/sec"
"      Hydrograph volume  646.620 c.m"
"      0.026 0.156 0.154 0.154"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.026 0.000 0.154 0.154"
"=====
" CATCHMENT 8
"=====
" 33 CATCHMENT 8"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      8 ID number"
"      50.000 % Impervious"
"      0.120 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.060 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.060 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.044 0.000 0.154 0.154 c.m/sec"
"      Catchment 8 Pervious Impervious Total Area "
"      Surface Area 0.060 0.060 0.120 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 43.08 43.08 86.16 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 20.53 36.61 57.14 c.m"
"      Maximum flow 0.014 0.036 0.044 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.044 0.044 0.154 0.154"
" 52 CHANNEL DESIGN"
"      0.044 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"

```

```

"      Catchment 10      Pervious  Impervious  Total Area  "
"      Surface Area      0.360      0.240      0.600      hectare"
"      Time of concentration 22.154      2.945      11.433      minutes"
"      Time to Centroid 119.484      84.305      99.851      minutes"
"      Rainfall depth      71.801      71.801      71.801      mm"
"      Rainfall volume      258.48      172.32      430.81      c.m"
"      Rainfall losses      37.290      6.426      24.945      mm"
"      Runoff depth      34.511      65.375      46.857      mm"
"      Runoff volume      124.24      156.90      281.14      c.m"
"      Maximum flow      0.039      0.120      0.135      c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.135      0.226      0.038      0.165"
" 54 POND DESIGN"
"      0.226 Current peak flow c.m/sec"
"      470.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 12.0"
"      0.600 0.001 85.6"
"      0.740 0.001 144.0"
"      0.750 0.162 150.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.150 c.m/sec"
"      Maximum level 0.749 metre"
"      Maximum storage 149.562 c.m"
"      Centroidal lag 6.432 hours"
"      0.135 0.226 0.150 0.165 c.m/sec"
" 40 HYDROGRAPH Combine 4"
"      6 Combine "
"      4 Node #"
"      "
"      Maximum flow 0.268 c.m/sec"
"      Hydrograph volume 1088.806 c.m"
"      0.135 0.226 0.150 0.268"
" 40 HYDROGRAPH Confluence 4"
"      7 Confluence "
"      4 Node #"
"      "
"      Maximum flow 0.268 c.m/sec"
"      Hydrograph volume 1088.806 c.m"
"      0.135 0.268 0.150 0.000"
" 54 POND DESIGN"
"      0.268 Current peak flow c.m/sec"
"      1090.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      1.000 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.200 0.021 6.8"
"      0.400 0.086 29.4"
"      0.600 0.122 80.8"
"      0.800 0.150 146.1"
"      1.000 0.173 231.4"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.305 1.000"
"      Peak outflow 0.160 c.m/sec"
"      Maximum level 0.883 metre"
"      Maximum storage 181.542 c.m"
"      Centroidal lag 4.172 hours"
"      0.135 0.268 0.160 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.135 0.160 0.160 0.000"
=====
ROAD CULVERT
=====
" 51 PIPE DESIGN"
"      0.160 Current peak flow c.m/sec"
"      0.015 Manning 'n'"
"      0.450 Diameter metre"
"      0.420 Gradient %"
"      Depth of flow 0.395 metre"
"      Velocity 1.187 m/sec"
"      Pipe capacity 0.160 c.m/sec"
"      Critical depth 0.281 metre"
" 53 ROUTE 18"
"      18.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      11.373 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.834 Beta weighting factor"
"      50.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.160 c.m/sec"
"      0.135 0.160 0.160 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 5"
"      6 Combine "

```

```

"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.035 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.026 0.165 0.038 0.000 c.m/sec"
"      Catchment 12 Pervious Impervious Total Area "
"      Surface Area 0.035 0.035 0.070 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 25.13 25.13 50.26 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 11.97 21.36 33.33 c.m"
"      Maximum flow 0.008 0.021 0.025 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.026 0.168 0.038 0.000"
" 51 PIPE DESIGN"
"      0.168 Current peak flow c.m/sec"
"      0.015 Manning 'n'"
"      0.500 Diameter metre"
"      0.420 Gradient %"
"      Depth of flow 0.336 metre"
"      Velocity 1.198 m/sec"
"      Pipe capacity 0.212 c.m/sec"
"      Critical depth 0.279 metre"
" 53 ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      6.262 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.856 Beta weighting factor"
"      42.857 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.168 c.m/sec"
"          0.026 0.168 0.168 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"          0.026 0.168 0.168 0.000"
" 52 CHANNEL DESIGN"
"      0.168 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.420 Gradient %"
"      Depth of flow 0.178 metre"
"      Velocity 0.508 m/sec"
"      Channel capacity 3.636 c.m/sec"
"      Critical depth 0.103 metre"
" 53 ROUTE 46"
"      46.10 Reach length( metre)"
"      0.238 X-factor <= 0.5"
"      68.015 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.168 c.m/sec"
"          0.026 0.168 0.168 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6"
"      6 Combine "
"      6 Node #"
"      Maximum flow 0.168 c.m/sec"
"      Hydrograph volume 1177.083 c.m"
"          0.026 0.168 0.168 0.168"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"          0.026 0.000 0.168 0.168"
"=====
" CATCHMENT 13
"=====
" 33 CATCHMENT 13"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      13 ID number"
"      40.000 % Impervious"
"      0.440 Total Area"
"      56.100 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"      56.100 Pervious length"

```

```

"      Runoff volume      10.26      18.30      28.57      c.m"
"      Maximum flow      0.007      0.018      0.022      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.022      0.211      0.068      0.000"
" 51      PIPE DESIGN"
"      0.211 Current peak flow      c.m/sec"
"      0.015 Manning 'n'"
"      0.500 Diameter      metre"
"      0.420 Gradient      %"
"      Depth of flow      0.408      metre"
"      Velocity      1.231      m/sec"
"      Pipe capacity      0.212      c.m/sec"
"      Critical depth      0.314      metre"
" 53      ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      6.091 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.909 Beta weighting factor"
"      60.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.210      c.m/sec"
"          0.022      0.211      0.210      0.000 c.m/sec"
" 40      HYDROGRAPH Next link "
"      5 Next link "
"          0.022      0.210      0.210      0.000"
" 52      CHANNEL DESIGN"
"      0.210 Current peak flow      c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth      metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth      metre"
"      0.420 Gradient      %"
"      Depth of flow      0.202      metre"
"      Velocity      0.545      m/sec"
"      Channel capacity      3.636      c.m/sec"
"      Critical depth      0.119      metre"
" 53      ROUTE 46"
"      46.10 Reach length( metre)"
"      0.206 X-factor <= 0.5"
"      63.388 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.208      c.m/sec"
"          0.022      0.210      0.208      0.000 c.m/sec"
" 40      HYDROGRAPH Combine 7"
"      6 Combine "
"      7 Node #"
"      "
"      Maximum flow      0.208      c.m/sec"
"      Hydrograph volume      1404.083      c.m"
"          0.022      0.210      0.208      0.208"
" 40      HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"          0.022      0.000      0.208      0.208"
"=====
"                                CATCHMENT 15
"=====
" 33      CATCHMENT 15"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      15 ID number"
"      40.000 % Impervious"
"      0.460 Total Area"
"      56.100 Flow length"
"      2.000 Overland Slope"
"      0.276 Pervious Area"
"      56.100 Pervious length"
"      2.000 Pervious slope"
"      0.184 Impervious Area"
"      56.100 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.104      0.000      0.208      0.208 c.m/sec"
"      Catchment 15      Pervious      Impervious      Total Area "
"      Surface Area      0.276      0.184      0.460      hectare"
"      Time of concentration      16.705      2.221      8.601      minutes"
"      Time to Centroid      111.906      83.063      95.769      minutes"
"      Rainfall depth      71.801      71.801      71.801      mm"
"      Rainfall volume      198.17      132.11      330.29      c.m"
"      Rainfall losses      37.298      6.069      24.807      mm"
"      Runoff depth      34.503      65.732      46.994      mm"
"      Runoff volume      95.23      120.95      216.17      c.m"

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"      Peak outflow          0.322    c.m/sec"
"      0.022    0.323    0.322    0.000 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link "
"      0.022    0.322    0.322    0.000"
" 52  CHANNEL DESIGN"
"      0.322 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.580 Gradient %"
"      Depth of flow          0.235 metre"
"      Velocity              0.697 m/sec"
"      Channel capacity      4.273 c.m/sec"
"      Critical depth        0.156 metre"
" 53  ROUTE 46"
"      46.10 Reach length( metre)"
"      0.255 X-factor <= 0.5"
"      49.596 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      60.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow          0.321    c.m/sec"
"      0.022    0.322    0.321    0.000 c.m/sec"
" 40  HYDROGRAPH Combine 9"
"      6 Combine "
"      9 Node #"
"      "
"      Maximum flow          0.321    c.m/sec"
"      Hydrograph volume     1871.106 c.m"
"      0.022    0.322    0.321    0.321"
" 40  HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.022    0.000    0.321    0.321"
=====
CATCHMENT 19
=====
" 33  CATCHMENT 19"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      19 ID number"
"      40.000 % Impervious"
"      0.460 Total Area"
"      56.100 Flow length"
"      2.000 Overland Slope"
"      0.276 Pervious Area"
"      56.100 Pervious length"
"      2.000 Pervious slope"
"      0.184 Impervious Area"
"      56.100 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.104    0.000    0.321    0.321 c.m/sec"
"      Catchment 19 Pervious Impervious Total Area "
"      Surface Area          0.276    0.184    0.460 hectare"
"      Time of concentration  16.705    2.221    8.601 minutes"
"      Time to Centroid      111.906    83.063    95.769 minutes"
"      Rainfall depth        71.801    71.801    71.801 mm"
"      Rainfall volume       198.17    132.11    330.29 c.m"
"      Rainfall losses       37.298    6.069    24.807 mm"
"      Runoff depth          34.503    65.732    46.994 mm"
"      Runoff volume         95.23    120.95    216.17 c.m"
"      Maximum flow          0.036    0.092    0.104 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.104    0.104    0.321    0.321"
" 54  POND DESIGN"
"      0.104 Current peak flow c.m/sec"
"      220.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000    0.000    0.0"
"      0.300    0.001    0.1"
"      0.450    0.001    4.7"
"      0.600    0.001    37.1"
"      0.740    0.001    72.0"
"      0.750    0.076    75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coeffic diameter orifices"
"      0.000    0.600    0.025    1.000"
"      Peak outflow          0.076 c.m/sec"
"      Maximum level         0.750 metre"

```

```

"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      42.857 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.022 0.374 0.373 c.m/sec"
"      0.022 0.374 0.373 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 10"
"      6 Combine "
"      10 Node #"
"      "
"      Maximum flow 0.373 c.m/sec"
"      Hydrograph volume 2105.548 c.m"
"      0.022 0.374 0.373 0.373"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.022 0.000 0.373 0.373"
"=====
CATCHMENT 21
=====
" 33 CATCHMENT 21"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      21 ID number"
"      40.000 % Impervious"
"      0.460 Total Area"
"      56.100 Flow length"
"      2.000 Overland Slope"
"      0.276 Pervious Area"
"      56.100 Pervious length"
"      2.000 Pervious slope"
"      0.184 Impervious Area"
"      56.100 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.104 0.000 0.373 0.373 c.m/sec"
"      Catchment 21 Pervious Impervious Total Area "
"      Surface Area 0.276 0.184 0.460 hectare"
"      Time of concentration 16.705 2.221 8.601 minutes"
"      Time to Centroid 111.906 83.063 95.769 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 198.17 132.11 330.29 c.m"
"      Rainfall losses 37.298 6.069 24.807 mm"
"      Runoff depth 34.503 65.732 46.994 mm"
"      Runoff volume 95.23 120.95 216.17 c.m"
"      Maximum flow 0.036 0.092 0.104 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.104 0.104 0.373 0.373"
" 54 POND DESIGN"
"      0.104 Current peak flow c.m/sec"
"      220.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.740 0.001 72.0"
"      0.750 0.076 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.076 c.m/sec"
"      Maximum level 0.750 metre"
"      Maximum storage 74.987 c.m"
"      Centroidal lag 5.342 hours"
"      0.104 0.104 0.076 0.373 c.m/sec"
" 40 HYDROGRAPH Combine 10"
"      6 Combine "
"      10 Node #"
"      "
"      Maximum flow 0.421 c.m/sec"
"      Hydrograph volume 2311.736 c.m"
"      0.104 0.104 0.076 0.421"
" 40 HYDROGRAPH Confluence 10"
"      7 Confluence "
"      10 Node #"
"      "
"      Maximum flow 0.421 c.m/sec"
"      Hydrograph volume 2311.736 c.m"
"      0.104 0.421 0.076 0.000"
" 51 PIPE DESIGN"
"      0.421 Current peak flow c.m/sec"
"      0.016 Manning 'n'"
"      0.600 Diameter metre"
"      1.000 Gradient %"
"      Depth of flow 0.423 metre"
"      Velocity 1.978 m/sec"

```


CATCHMENT 25
EXISTING LOT

```

=====
" 33  CATCHMENT 25"
      1  Triangular SCS"
      1  Equal length"
      1  SCS method"
      25  ID number"
      40.000  % Impervious"
      0.470  Total Area"
      73.000  Flow length"
      2.000  Overland Slope"
      0.282  Pervious Area"
      73.000  Pervious length"
      2.000  Pervious slope"
      0.188  Impervious Area"
      73.000  Impervious length"
      2.000  Impervious slope"
      0.250  Pervious Manning 'n'"
      81.000  Pervious SCS Curve No."
      0.481  Pervious Runoff coefficient"
      0.100  Pervious Ia/S coefficient"
      5.958  Pervious Initial abstraction"
      0.015  Impervious Manning 'n'"
      98.000  Impervious SCS Curve No."
      0.925  Impervious Runoff coefficient"
      0.100  Impervious Ia/S coefficient"
      0.518  Impervious Initial abstraction"
      0.106  0.000  0.031  0.031 c.m/sec"
      Catchment 25  Pervious  Impervious Total Area "
      Surface Area  0.282  0.188  0.470  hectare"
      Time of concentration  19.565  2.601  10.094  minutes"
      Time to Centroid  115.891  83.742  97.943  minutes"
      Rainfall depth  71.801  71.801  71.801  mm"
      Rainfall volume  202.48  134.99  337.47  mm"
      Rainfall losses  37.290  6.373  24.923  mm"
      Runoff depth  34.511  65.428  46.878  mm"
      Runoff volume  97.32  123.01  220.33  c.m"
      Maximum flow  0.032  0.091  0.106  c.m/sec"
      40  HYDROGRAPH Add Runoff "
      4  Add Runoff " 0.106  0.106  0.031  0.031"
      54  POND DESIGN"
      0.106  Current peak flow  c.m/sec"
      230.0  Hydrograph volume  c.m/sec"
      5.  Number of stages"
      0.000  Minimum water level  c.m/sec"
      0.750  Maximum water level  c.m/sec"
      0  Keep Design Data: 1 = True; 0 = False"
      Level Discharge  Volume"
      0.000  0.000  0.0"
      0.188  0.001  1.0"
      0.375  0.001  4.0"
      0.563  0.001  30.0"
      0.750  0.050  75.0"
      Peak outflow  0.048  c.m/sec"
      Maximum level  0.741  metre"
      Maximum storage  72.736  c.m"
      Centroidal lag  2.883  hours"
      0.106  0.106  0.048  0.031 c.m/sec"
      40  HYDROGRAPH Combine 12"
      6  Combine "
      12  Node #"
      Maximum flow  0.062  c.m/sec"
      Hydrograph volume  267.802  c.m"
      0.106  0.106  0.048  0.062"
      40  HYDROGRAPH Start - New Tributary"
      2  Start - New Tributary"
      0.106  0.000  0.048  0.062"
=====

```

CATCHMENT 26

```

=====
" 33  CATCHMENT 26"
      1  Triangular SCS"
      1  Equal length"
      1  SCS method"
      26  ID number"
      50.000  % Impervious"
      0.100  Total Area"
      5.750  Flow length"
      2.000  Overland Slope"
      0.050  Pervious Area"
      5.750  Pervious length"
      2.000  Pervious slope"
      0.050  Impervious Area"
      5.750  Impervious length"
      2.000  Impervious slope"
      0.250  Pervious Manning 'n'"
      81.000  Pervious SCS Curve No."
      0.481  Pervious Runoff coefficient"
      0.100  Pervious Ia/S coefficient"
      5.958  Pervious Initial abstraction"
      0.015  Impervious Manning 'n'"
      98.000  Impervious SCS Curve No."
      0.925  Impervious Runoff coefficient"
      0.100  Impervious Ia/S coefficient"
      0.518  Impervious Initial abstraction"
      0.037  0.000  0.048  0.062 c.m/sec"
      Catchment 26  Pervious  Impervious Total Area "
      Surface Area  0.050  0.050  0.100  hectare"
      Time of concentration  4.259  0.566  1.893  minutes"

```

```

"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.037 0.000 0.085 0.085 c.m/sec"
"      Catchment 27 Pervious Impervious Total Area "
"      Surface Area 0.050 0.050 0.100 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 35.90 35.90 71.80 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 17.11 30.51 47.61 c.m"
"      Maximum flow 0.012 0.030 0.037 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.037 0.037 0.085 0.085"
" 52 CHANNEL DESIGN"
"      0.037 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"          Depth of flow 0.070 metre"
"          Velocity 0.320 m/sec"
"          Channel capacity 3.967 c.m/sec"
"          Critical depth 0.039 metre"
" 53 ROUTE 73"
"      73.00 Reach length( metre)"
"      0.444 X-factor <= 0.5"
"      171.111 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step ( seconds)"
"          1 No. of sub-reaches"
"          Peak outflow 0.031 c.m/sec"
"          0.037 0.037 0.031 0.085 c.m/sec"
" 40 HYDROGRAPH Combine 13"
"      6 Combine "
"      13 Node #"
"          Maximum flow 0.116 c.m/sec"
"          Hydrograph volume 363.032 c.m"
"          0.037 0.037 0.031 0.116"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"          0.037 0.000 0.031 0.116"
"=====
"                          CATCHMENT 28
"                          EXISTING LOT
"=====
" 33 CATCHMENT 28"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      28 ID number"
"      40.000 % Impervious"
"      0.380 Total Area"
"      73.000 Flow length"
"      2.000 Overland Slope"
"      0.228 Pervious Area"
"      73.000 Pervious length"
"      2.000 Pervious slope"
"      0.152 Impervious Area"
"      73.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.086 0.000 0.031 0.116 c.m/sec"
"      Catchment 28 Pervious Impervious Total Area "
"      Surface Area 0.228 0.152 0.380 hectare"
"      Time of concentration 19.565 2.601 10.094 minutes"
"      Time to Centroid 115.891 83.742 97.943 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 163.71 109.14 272.84 c.m"
"      Rainfall losses 37.290 6.373 24.923 mm"
"      Runoff depth 34.511 65.428 46.878 mm"
"      Runoff volume 78.69 99.45 178.14 c.m"
"      Maximum flow 0.026 0.074 0.086 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.086 0.086 0.031 0.116"
" 54 POND DESIGN"
"      0.086 Current peak flow c.m/sec"
"      180.0 Hydrograph volume c.m/sec"
"      5. Number of stages"

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"      0.000 Minimum water level c.m/sec"
"      0.900 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.150 0.008 4.8"
"      0.300 0.023 22.5"
"      0.450 0.030 57.9"
"      0.600 0.036 111.3"
"      0.750 0.041 172.3"
"      0.900 0.046 245.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      0.000 0.600 0.157 1.000"
"      Peak outflow 0.046 c.m/sec"
"      Maximum level 0.896 metre"
"      Maximum storage 243.140 c.m"
"      Centroidal lag 3.465 hours"
"      0.062 0.169 0.046 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.062 0.046 0.046 0.000"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.062 0.046 0.046 0.000"
"=====
" CATCHMENT 30
"=====
" 33 CATCHMENT 30"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      30 ID number"
"      50.000 % Impervious"
"      0.080 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.040 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.040 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.029 0.046 0.046 0.000 c.m/sec"
"      Catchment 30 Pervious Impervious Total Area "
"      Surface Area 0.040 0.040 0.080 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 28.72 28.72 57.44 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 13.68 24.41 38.09 c.m"
"      Maximum flow 0.009 0.024 0.029 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.029 0.053 0.046 0.000"
" 51 PIPE DESIGN"
"      0.053 Current peak flow c.m/sec"
"      0.013 Manning 'n'"
"      0.300 Diameter metre"
"      0.300 Gradient %"
"      Depth of flow 0.244 metre"
"      Velocity 0.854 m/sec"
"      Pipe capacity 0.053 c.m/sec"
"      Critical depth 0.178 metre"
" 53 ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      8.780 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.884 Beta weighting factor"
"      75.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.051 c.m/sec"
"      0.029 0.053 0.051 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.029 0.051 0.051 0.000"
" 52 CHANNEL DESIGN"
"      0.051 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.085 metre"

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"      Rainfall losses      37.254      6.084      24.786      mm"
"      Runoff depth         34.547      65.717      47.015      mm"
"      Runoff volume        91.20       115.66      206.87      c.m"
"      Maximum flow         0.033      0.087      0.100      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.100      0.119      0.051      0.051"
" 54  POND DESIGN"
"      0.119 Current peak flow      c.m/sec"
"      250.0 Hydrograph volume      c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level      c.m/sec"
"      0.750 Maximum water level      c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"          Level Discharge      Volume"
"          0.000      0.000      0.0"
"          0.300      0.001      0.1"
"          0.450      0.001      4.7"
"          0.600      0.001      37.1"
"          0.740      0.001      72.0"
"          0.750      0.096      75.0"
"      1. ORIFICES"
"          Orifice      Orifice      Orifice Number of"
"          invert coefficie      diameter orifices"
"          0.000      0.600      0.025      1.000"
"      Peak outflow      0.090      c.m/sec"
"      Maximum level      0.749      metre"
"      Maximum storage      74.802      c.m"
"      Centroidal lag      5.228      hours"
"          0.100      0.119      0.090      0.051 c.m/sec"
" 40  HYDROGRAPH Combine      14"
"      6 Combine "
"      14 Node #"
"          Maximum flow      0.138      c.m/sec"
"          Hydrograph volume      888.737      c.m"
"          0.100      0.119      0.090      0.138"
" 40  HYDROGRAPH Confluence      14"
"      7 Confluence "
"      14 Node #"
"          Maximum flow      0.138      c.m/sec"
"          Hydrograph volume      888.737      c.m"
"          0.100      0.138      0.090      0.000"
"=====
"                                CATCHMENT 33
"=====
" 33  CATCHMENT 33"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      33 ID number"
"      50.000 % Impervious"
"      0.070 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.035 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.035 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"          0.026      0.138      0.090      0.000 c.m/sec"
"      Catchment 33      Pervious      Impervious Total Area "
"      Surface Area      0.035      0.035      0.070      hectare"
"      Time of concentration      4.259      0.566      1.893      minutes"
"      Time to Centroid      94.699      81.236      86.073      minutes"
"      Rainfall depth      71.801      71.801      71.801      mm"
"      Rainfall volume      25.13      25.13      50.26      c.m"
"      Rainfall losses      37.589      10.785      24.187      mm"
"      Runoff depth      34.212      61.017      47.614      mm"
"      Runoff volume      11.97      21.36      33.33      c.m"
"      Maximum flow      0.008      0.021      0.026      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"          0.026      0.149      0.090      0.000"
" 51  PIPE DESIGN"
"      0.149 Current peak flow      c.m/sec"
"      0.015 Manning 'n'"
"      0.450 Diameter      metre"
"      0.500 Gradient      %"
"          Depth of flow      0.319      metre"
"          Velocity      1.234      m/sec"
"          Pipe capacity      0.175      c.m/sec"
"          Critical depth      0.270      metre"
" 53  ROUTE 10"
"      10.00 Reach length( metre)"
"      0.000 X-factor <= 0.5"
"      6.080 K-lag ( seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"

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"      Surface Area      0.264      0.176      0.440      hectare"
"      Time of concentration 17.393      2.312      8.961      minutes"
"      Time to Centroid 112.842      83.216      96.279      minutes"
"      Rainfall depth 71.801      71.801      71.801      mm"
"      Rainfall volume 189.55      126.37      315.92      c.m"
"      Rainfall losses 37.251      6.088      24.786      mm"
"      Runoff depth 34.550      65.713      47.015      mm"
"      Runoff volume 91.21      115.66      206.87      c.m"
"      Maximum flow 0.033      0.087      0.100      c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff " 0.100      0.119      0.139      0.139"
" 54 POND DESIGN"
"      0.119 Current peak flow c.m/sec"
"      250.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.740 0.001 72.0"
"      0.750 0.096 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.090 c.m/sec"
"      Maximum level 0.749 metre"
"      Maximum storage 74.799 c.m"
"      Centroidal lag 5.225 hours"
"      0.100 0.119 0.090 0.139 c.m/sec"
" 40 HYDROGRAPH Combine 15"
"      6 Combine "
"      15 Node #"
"      Maximum flow 0.229 c.m/sec"
"      Hydrograph volume 1150.034 c.m"
"      0.100 0.119 0.090 0.229"
" 40 HYDROGRAPH Confluence 15"
"      7 Confluence "
"      15 Node #"
"      Maximum flow 0.229 c.m/sec"
"      Hydrograph volume 1150.034 c.m"
"      0.100 0.229 0.090 0.000"
=====
CATCHMENT 36
=====
" 33 CATCHMENT 36"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      36 ID number"
"      50.000 % Impervious"
"      0.070 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.035 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.035 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.026 0.229 0.090 0.000 c.m/sec"
"      Catchment 36 Pervious Impervious Total Area "
"      Surface Area 0.035 0.035 0.070 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 25.13 25.13 50.26 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 11.97 21.36 33.33 c.m"
"      Maximum flow 0.008 0.021 0.026 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff " 0.026      0.240      0.090      0.000"
" 51 PIPE DESIGN"
"      0.240 Current peak flow c.m/sec"
"      0.015 Manning 'n'"
"      0.500 Diameter metre"
"      0.500 Gradient %"
"      Surcharged HGL 0.536 %"
"      Velocity 1.221 m/sec"
"      Pipe capacity 0.231 c.m/sec"
"      Critical depth 0.000 metre"
" 53 ROUTE 10"
"      10.00 Reach length( metre)"

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"      0.264 Pervious Area"
"      60.000 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"      60.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.100 0.019 0.208 0.208 c.m/sec"
"      Catchment 38 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"
"      Time of concentration 17.393 2.312 8.961 minutes"
"      Time to Centroid 112.842 83.216 96.279 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 189.55 126.37 315.92 c.m"
"      Rainfall losses 37.251 6.088 24.786 mm"
"      Runoff depth 34.550 65.713 47.015 mm"
"      Runoff volume 91.21 115.66 206.87 c.m"
"      Maximum flow 0.033 0.087 0.100 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.100 0.119 0.208 0.208"
" 54 POND DESIGN"
"      0.119 Current peak flow c.m/sec"
"      250.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.740 0.001 72.0"
"      0.750 0.096 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficient diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.090 c.m/sec"
"      Maximum level 0.749 metre"
"      Maximum storage 74.799 c.m"
"      Centroidal lag 5.225 hours"
"      0.100 0.119 0.090 0.208 c.m/sec"
" 40 HYDROGRAPH Combine 16"
"      6 Combine "
"      16 Node #"
"      Maximum flow 0.298 c.m/sec"
"      Hydrograph volume 1411.251 c.m"
"      0.100 0.119 0.090 0.298"
" 40 HYDROGRAPH Confluence 16"
"      7 Confluence "
"      16 Node #"
"      Maximum flow 0.298 c.m/sec"
"      Hydrograph volume 1411.251 c.m"
"      0.100 0.298 0.090 0.000"
"=====
" CATCHMENT 39
"=====
" 33 CATCHMENT 39"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      39 ID number"
"      50.000 % Impervious"
"      0.070 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.035 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.035 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.026 0.298 0.090 0.000 c.m/sec"
"      Catchment 39 Pervious Impervious Total Area "
"      Surface Area 0.035 0.035 0.070 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 25.13 25.13 50.26 c.m"

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"      Runoff depth      34.409      64.409      34.409      mm"
"      Runoff volume     34.41       0.00       34.41       c.m"
"      Maximum flow      0.019       0.000       0.019       c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "      0.019      0.284      0.284"
=====
CATCHMENT 41
=====
" 33 CATCHMENT 41"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      41 ID number"
"      40.000 % Impervious"
"      0.440 Total Area"
"      60.000 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"      60.000 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"      60.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.100      0.019      0.284      0.284 c.m/sec"
"      Catchment 41 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"
"      Time of concentration 17.393 2.312 8.961 minutes"
"      Time to Centroid 112.842 83.216 96.279 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 189.55 126.37 315.92 c.m"
"      Rainfall losses 37.251 6.088 24.786 mm"
"      Runoff depth 34.550 65.713 47.015 mm"
"      Runoff volume 91.21 115.66 206.87 c.m"
"      Maximum flow 0.033 0.087 0.100 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "      0.100      0.119      0.284      0.284"
" 54 POND DESIGN"
"      0.119 Current peak flow c.m/sec"
"      250.0 Hydrograph volume c.m/sec"
"      6. Number of stages"
"      0.000 Minimum water level c.m/sec"
"      0.750 Maximum water level c.m/sec"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.740 0.001 72.0"
"      0.750 0.096 75.0"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow 0.090 c.m/sec"
"      Maximum level 0.749 metre"
"      Maximum storage 74.799 c.m"
"      Centroidal lag 5.225 hours"
"      0.100 0.119 0.090 0.284 c.m/sec"
" 40 HYDROGRAPH Combine 17"
"      6 Combine "
"      17 Node #"
"      Maximum flow 0.372 c.m/sec"
"      Hydrograph volume 1672.472 c.m"
"      0.100 0.119 0.090 0.372"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.100 0.000 0.090 0.372"
=====
CATCHMENT 42
=====
" 33 CATCHMENT 42"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      42 ID number"
"      50.000 % Impervious"
"      0.110 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.055 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.055 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"

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```

"      43 ID number"
" 50.000 % Impervious"
" 0.110 Total Area"
" 5.750 Flow length"
" 2.000 Overland Slope"
" 0.055 Pervious Area"
" 5.750 Pervious length"
" 2.000 Pervious slope"
" 0.055 Impervious Area"
" 5.750 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.481 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.925 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
"      0.040 0.000 0.377 0.377 c.m/sec"
" Catchment 43 Pervious Impervious Total Area "
" Surface Area 0.055 0.055 0.110 hectare"
" Time of concentration 4.259 0.566 1.893 minutes"
" Time to Centroid 94.699 81.236 86.073 minutes"
" Rainfall depth 71.801 71.801 71.801 mm"
" Rainfall volume 39.49 39.49 78.98 c.m"
" Rainfall losses 37.589 10.785 24.187 mm"
" Runoff depth 34.212 61.017 47.614 mm"
" Runoff volume 18.82 33.56 52.38 c.m"
" Maximum flow 0.013 0.033 0.040 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"      0.040 0.040 0.377 0.377"
" 52 CHANNEL DESIGN"
" 0.040 Current peak flow c.m/sec"
" 0.035 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 1.500 Basewidth metre"
" 2.000 Left bank slope"
" 2.000 Right bank slope"
" 0.900 Channel depth metre"
" 3.000 Gradient %"
" Depth of flow 0.043 metre"
" Velocity 0.584 m/sec"
" Channel capacity 9.717 c.m/sec"
" Critical depth 0.041 metre"
" 53 ROUTE 93"
" 93.00 Reach length( metre)"
" 0.495 X-factor <= 0.5"
" 119.334 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.033 c.m/sec"
"      0.040 0.040 0.033 0.377 c.m/sec"
" 40 HYDROGRAPH Combine 18"
" 6 Combine "
" 18 Node #"
" Maximum flow 0.398 c.m/sec"
" Hydrograph volume 1777.156 c.m"
"      0.040 0.040 0.033 0.398"
" 40 HYDROGRAPH Confluence 18"
" 7 Confluence "
" 18 Node #"
" Maximum flow 0.398 c.m/sec"
" Hydrograph volume 1777.156 c.m"
"      0.040 0.398 0.033 0.000"
" 52 CHANNEL DESIGN"
" 0.398 Current peak flow c.m/sec"
" 0.035 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 1.500 Basewidth metre"
" 2.000 Left bank slope"
" 2.000 Right bank slope"
" 0.900 Channel depth metre"
" 0.600 Gradient %"
" Depth of flow 0.262 metre"
" Velocity 0.752 m/sec"
" Channel capacity 4.346 c.m/sec"
" Critical depth 0.177 metre"
" 53 ROUTE 16"
" 16.00 Reach length( metre)"
" 0.000 X-factor <= 0.5"
" 15.952 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.608 Beta weighting factor"
" 37.500 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.386 c.m/sec"
"      0.040 0.398 0.386 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
"      0.040 0.386 0.386 0.000"

```

```

"      1 SCS method"
"      22 ID number"
" 50.000 % Impervious"
"      0.090 Total Area"
"      5.750 Flow length"
"      2.000 Overland Slope"
"      0.045 Pervious Area"
"      5.750 Pervious length"
"      2.000 Pervious slope"
"      0.045 Impervious Area"
"      5.750 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.033 0.000 0.789 0.789 c.m/sec"
"      Catchment 22 Pervious Impervious Total Area "
"      Surface Area 0.045 0.045 0.090 hectare"
"      Time of concentration 4.259 0.566 1.893 minutes"
"      Time to Centroid 94.699 81.236 86.073 minutes"
"      Rainfall depth 71.801 71.801 71.801 mm"
"      Rainfall volume 32.31 32.31 64.62 c.m"
"      Rainfall losses 37.589 10.785 24.187 mm"
"      Runoff depth 34.212 61.017 47.614 mm"
"      Runoff volume 15.40 27.46 42.85 c.m"
"      Maximum flow 0.011 0.027 0.033 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.033 0.033 0.789 0.789"
" 52 CHANNEL DESIGN"
"      0.033 Current peak flow c.m/sec"
"      0.035 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      1.500 Basewidth metre"
"      2.000 Left bank slope"
"      2.000 Right bank slope"
"      0.900 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.065 metre"
"      Velocity 0.308 m/sec"
"      Channel capacity 3.967 c.m/sec"
"      Critical depth 0.036 metre"
" 53 ROUTE 32"
"      32.00 Reach length (metre)"
"      0.379 X-factor <= 0.5"
"      77.910 K-lag ( seconds)"
"      0.000 Default (0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag ( seconds)"
"      0.500 Beta weighting factor"
"      75.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.033 0.033 0.026 c.m/sec"
"      0.033 0.033 0.026 0.789 c.m/sec"
" 40 HYDROGRAPH Combine 19"
"      6 Combine "
"      19 Node #"
"      Maximum flow 0.799 c.m/sec"
"      Hydrograph volume 4131.400 c.m"
"      0.033 0.033 0.026 0.799"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.033 0.000 0.026 0.799"
=====
CATCHMENT 23
=====
" 33 CATCHMENT 23"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      23 ID number"
"      40.000 % Impervious"
"      0.440 Total Area"
"      56.300 Flow length"
"      2.000 Overland Slope"
"      0.264 Pervious Area"
"      56.300 Pervious length"
"      2.000 Pervious slope"
"      0.176 Impervious Area"
"      56.300 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.481 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.925 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.100 0.000 0.026 0.799 c.m/sec"
"      Catchment 23 Pervious Impervious Total Area "
"      Surface Area 0.264 0.176 0.440 hectare"

```

```

"          invert coefficie diameter orifices"
"          0.000      0.600      0.025      1.000"
"          Peak outflow              0.068      c.m/sec"
"          Maximum level              0.750      metre"
"          Maximum storage            74.979      c.m"
"          Centroidal lag             5.331      hours"
"          0.129      0.129      0.068      0.854 c.m/sec"
" 40      HYDROGRAPH Combine 20"
"          6 Combine "
"          20 Node #"
"          "
"          Maximum flow              0.068      c.m/sec"
"          Hydrograph volume          198.813      c.m"
"          0.129      0.129      0.068      0.068"
" 40      HYDROGRAPH Start - New Tributary"
"          2 Start - New Tributary"
"          0.129      0.000      0.068      0.068"
"=====
"                                CATCHMENT 46
"=====
" 33      CATCHMENT 46"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          46 ID number"
"          50.000 % Impervious"
"          0.110 Total Area"
"          5.750 Flow length"
"          2.000 Overland Slope"
"          0.055 Pervious Area"
"          5.750 Pervious length"
"          2.000 Pervious slope"
"          0.055 Impervious Area"
"          5.750 Impervious length"
"          2.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.481 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.015 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.925 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          0.040      0.000      0.068      0.068 c.m/sec"
"          Catchment 46 Pervious Impervious Total Area "
"          Surface Area      0.055      0.055      0.110      hectare"
"          Time of concentration 4.259      0.566      1.893      minutes"
"          Time to Centroid 94.699      81.236      86.073      minutes"
"          Rainfall depth 71.801      71.801      71.801      mm"
"          Rainfall volume 39.49      39.49      78.98      c.m"
"          Rainfall losses 37.589      10.785      24.187      mm"
"          Runoff depth 34.212      61.017      47.614      mm"
"          Runoff volume 18.82      33.56      52.38      c.m"
"          Maximum flow 0.013      0.033      0.040      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          0.040      0.040      0.068      0.068"
" 52      CHANNEL DESIGN"
"          0.040 Current peak flow c.m/sec"
"          0.035 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          1.500 Basewidth metre"
"          2.000 Left bank slope"
"          2.000 Right bank slope"
"          0.900 Channel depth metre"
"          0.500 Gradient %"
"          Depth of flow              0.074      metre"
"          Velocity                    0.331      m/sec"
"          Channel capacity            3.967      c.m/sec"
"          Critical depth              0.041      metre"
" 53      ROUTE 47"
"          47.00 Reach length( metre)"
"          0.408 X-factor <= 0.5"
"          106.467 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500 Beta weighting factor"
"          100.000 Routing time step ( seconds)"
"          1 No. of sub-reaches"
"          Peak outflow              0.032      c.m/sec"
"          0.040      0.040      0.032      0.068 c.m/sec"
" 40      HYDROGRAPH Combine 20"
"          6 Combine "
"          20 Node #"
"          "
"          Maximum flow              0.088      c.m/sec"
"          Hydrograph volume          251.188      c.m"
"          0.040      0.040      0.032      0.088"
" 40      HYDROGRAPH Confluence 20"
"          7 Confluence "
"          20 Node #"
"          "
"          Maximum flow              0.088      c.m/sec"
"          Hydrograph volume          251.188      c.m"
"          0.040      0.088      0.032      0.000"
" 52      CHANNEL DESIGN"
"          0.088 Current peak flow c.m/sec"
"          0.035 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"

```

```

"      Peak outflow      0.275 c.m/sec"
"      0.022 0.278 0.275 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.022 0.275 0.275 0.000"
" 52 CHANNEL DESIGN"
" 0.275 Current peak flow c.m/sec"
" 0.035 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 1.500 Basewidth metre"
" 2.000 Left bank slope"
" 2.000 Right bank slope"
" 0.900 Channel depth metre"
" 0.420 Gradient %"
"      Depth of flow      0.235 metre"
"      Velocity      0.594 m/sec"
"      Channel capacity      3.636 c.m/sec"
"      Critical depth      0.141 metre"
" 53 ROUTE 46"
" 46.10 Reach length( metre) "
" 0.160 X-factor <= 0.5"
" 58.209 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
"      1 No. of sub-reaches"
"      Peak outflow      0.273 c.m/sec"
"      0.022 0.275 0.273 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 8"
"      6 Combine "
"      8 Node #"
"      "
"      Maximum flow      0.273 c.m/sec"
"      Hydrograph volume      1638.487 c.m"
"      0.022 0.275 0.273 0.273"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.022 0.000 0.273 0.273"
"=====
" CATCHMENT 17
"=====
" 33 CATCHMENT 17"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      17 ID number"
" 40.000 % Impervious"
" 0.460 Total Area"
" 56.100 Flow length"
" 2.000 Overland Slope"
" 0.276 Pervious Area"
" 56.100 Pervious length"
" 2.000 Pervious slope"
" 0.184 Impervious Area"
" 56.100 Impervious length"
" 2.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.481 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.925 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
"      0.104 0.000 0.273 0.273 c.m/sec"
"      Catchment 17 Pervious Impervious Total Area "
"      Surface Area      0.276 0.184 0.460 hectare"
"      Time of concentration      16.705 2.221 8.601 minutes"
"      Time to Centroid      111.906 83.063 95.769 minutes"
"      Rainfall depth      71.801 71.801 71.801 mm"
"      Rainfall volume      198.17 132.11 330.29 c.m"
"      Rainfall losses      37.298 6.069 24.807 mm"
"      Runoff depth      34.503 65.732 46.994 mm"
"      Runoff volume      95.23 120.95 216.17 c.m"
"      Maximum flow      0.036 0.092 0.104 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.104 0.104 0.273 0.273"
" 54 POND DESIGN"
" 0.104 Current peak flow c.m/sec"
" 220.0 Hydrograph volume c.m/sec"
" 6. Number of stages"
" 0.000 Minimum water level c.m/sec"
" 0.750 Maximum water level c.m/sec"
" 0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.300 0.000 0.0"
"      0.300 0.001 0.1"
"      0.450 0.001 4.7"
"      0.600 0.001 37.1"
"      0.740 0.001 72.0"
"      0.750 0.076 75.0"
" 1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coefficie diameter orifices"
"      0.000 0.600 0.025 1.000"
"      Peak outflow      0.076 c.m/sec"
"      Maximum level      0.750 metre"

```

ROUTE

Last conduit

Channel simple

Channel depth 0.900 metre

Gradient 0.500

Manning n 0.025

Depth of flow 0.434 metre

Flow capacity 3.967 c.m/sec

Peak inflow 0.927 c.m/sec

Reach length 10 metre

X-factor <= 0.5

K lag 8.3 seconds

Peak outflow 0.923 c.m/sec

☐ Specify values for X and K

Route

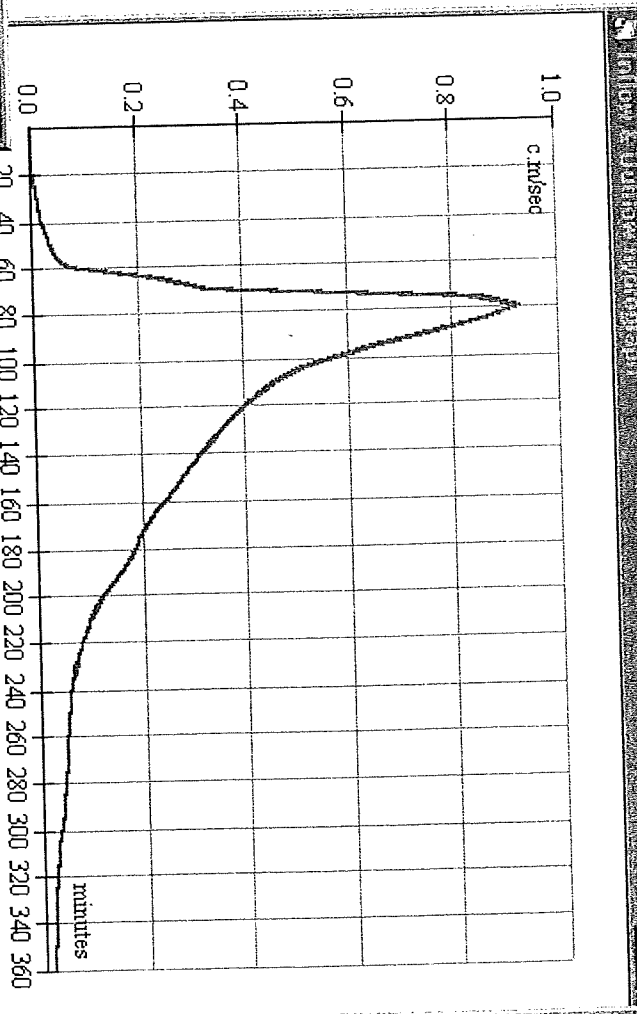
Undo

Cancel

Accept

Using 1 reaches of length 10.0 metre

Using 7 time steps of duration 12.9 seconds



Outflow Hydrograph

Total volume 4581.08 c.m Maximum flow 0.923 c.m/sec 300.0 minutes

	5.0	10.0	15.0	20.0	25.0	30.0	35.0	40.0	45.0	50.0
5.0	0.000	0.000	0.001	0.003	0.007	0.012	0.017	0.022	0.028	0.035
55.0	0.046	0.070	0.231	0.332	0.826	0.923	0.864	0.785	0.667	0.572
105.0	0.507	0.461	0.429	0.403	0.379	0.358	0.336	0.317	0.298	0.280
155.0	0.262	0.244	0.225	0.208	0.196	0.186	0.175	0.159	0.141	0.125
205.0	0.111	0.100	0.090	0.082	0.075	0.069	0.063	0.059	0.057	0.054
255.0	0.052	0.051	0.049	0.048	0.046	0.044	0.042	0.041	0.039	0.035
305.0	0.032	0.029	0.026	0.024	0.023	0.021	0.020	0.019	0.019	0.019
355.0	0.019	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018
405.0	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018
455.0	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018
505.0	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018
555.0	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.017	0.017
605.0	0.018	0.018	0.018	0.018	0.018	0.018	0.018	0.017	0.017	0.017
655.0	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017
705.0	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017	0.017
755.0	0.017	0.017	0.017	0.017	0.017	0.017	0.016	0.016	0.016	0.016
805.0	0.015	0.015	0.015	0.015	0.015	0.015	0.015	0.015	0.015	0.015

Appendix C

Geotechnical Report



RE: PRELIMINARY GEOTECHNICAL INVESTIGATION
PROPOSED INDUSTRIAL SUBDIVISION
1045 DONNYBROOK DRIVE
DORCHESTER, ONTARIO

FOR: Lantern Capital
2425 Matheson Boulevard East, 8th Floor
Mississauga, Ontario
L4W 5K4

ATTENTION: Mr. Bav Malhi

REPORT NO.: 2021-15454

DATE: June 15, 2021

DISTRIBUTION: PDF Copy: Lantern Capital
- Mr. Bav Malhi [bmalhi@lanterncapital.ca]
- Mr. Stephen Maycher [smaycher@lanterncapital.ca]

Original: (File No. 10826-S0456-GEO)



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June 15, 2021

REPORT NO.: 2021-15454

FILE NO.: 10826-S0456-GEO

1.0 INTRODUCTION

Sola Engineering Inc. (Sola) was retained by Lantern Capital (the Client) to carry out a preliminary geotechnical investigation for the proposed industrial subdivision located at 1045 Donnybrook Drive in Dorchester, Ontario (the subject site or site). Authorization to proceed with the investigation was received on April 26, 2021 through the acceptance of Sola's Proposal No. 2021-2716 dated April 21, 2021.

As per the scope of services detailed in Sola's proposal, the purpose of this investigation is to collect information on the soil and groundwater conditions at the subject site and, based on the investigation data to provide recommendations to assist with the preliminary design of the proposed industrial subdivision. It should be noted that a supplementary investigation will be required according to the building footprints for the detailed design.

This report presents the details of Sola's fieldwork and laboratory testing, outlines the soil and groundwater conditions at the site, and provides comments on the aforementioned items.

In this report, standard site investigation procedures have been adopted. The procedures including those developed by the Ontario Building Code (OBC), Canadian Foundation Engineering Manual (CFEM), American Society for Testing and Materials (ASTM), Ontario Ministry of Transportation (MTO) and Toronto Transit Commission (TTC), are considered by far the most accepted methods by the local geotechnical society for the general engineering purposes. Soil Classification Systems used for developing this report have been in general conformance with those outlined in the above-mentioned procedures, with modifications where appropriate. Where in doubt, this office must be contacted for further interpretation or clarification.

This report has been prepared for the Client, and their nominated engineers and designers. Third-party use or reproduction, in part or in full, of this report, is prohibited without written authorization from Sola. This report is also subject to the *Statement of Limitations* which forms an integral part of this document.

2.0 SITE SETTING

2.1 SITE LOCATION, DESCRIPTION AND PROPOSED DEVELOPMENT

The subject site is located at the open field at 1045 Donnybrook Drive in Dorchester, Ontario and is currently vacant. The site is bounded to the north by Donnybrook Drive and residential properties,



to the south by Highway 401, to the west by residential properties and to the east by farm land and tree covered areas.

The subject site is being considered for a industrial subdivision. It is understood that the Client is contemplating developing the site with single-storey slab-on-grade industrial buildings with office spaces.

2.2 PUBLISHED GEOLOGY

Based on a review of the existing geological publication for the site area, Ontario Geological Survey (OGS) Map P0606: *"Pleistocene Geology of the St. Thomas Area (East Half) (Southern Ontario)"*, the site surrounding area is underlain by Glacial Erie Lobe, comprising Port Stanley silty clay till and clayey silt till, in places covered by thin patches of lacustrine silt; ground moraine plains and end moraine ridges; slightly undulating microtopography. According to the OGS Map 2197: *"Ontario Geological Map – Southern Sheet"*, the surficial overburden is underlain by the bedrock of the Middle Devonian comprising Limestone, Dolostone, Shale and Gypsum.

3.0 GROUND INVESTIGATION

3.1 FIELD INVESTIGATION

3.1.1 Soil Investigation

Prior to undertaking field drilling, Sola obtained clearances of existing public utility services to the site from all applicable agencies and companies. In addition, private utility locates were also carried out.

The geotechnical field program was carried out on May 20, 2021 and comprised the drilling of four (4) boreholes (BH1 through BH4). The boreholes were advanced through the existing ground surface to the depth of approximately 6.6 m below the ground surface using a track-mounted drill rig equipped for split spoon sampling and standard penetration testing. The approximate locations of the boreholes are shown on **Enclosure 1**. Four (4) monitoring wells were installed at borehole locations BH1 through BH4.

All drilling equipment was supplied and operated by Terra Firma Environmental Services Ltd. of North York, Ontario, and the drilling works were completed under the full-time supervision of a qualified Sola Technician.

Standard Penetration Tests (SPTs) split spoon samples were collected in the drilled boreholes using a 50 mm outer diameter and 35 mm inner diameter split barrel sampler driven with a



63.5 kg automatic hammer dropping 760 mm. All soil samples were logged in the field and returned to Sola's laboratory in Vaughan for review and subsequent laboratory testing.

The logs of the boreholes completed are presented on **Enclosures 2 through 5**.

3.1.2 Groundwater Investigation

Groundwater level observations were made during drilling and in the open borehole upon completion of the drilling operations. Upon completion of each borehole, a monitoring well was installed to enable the a longer term monitoring of the groundwater at the site without interference from surface water. Details of groundwater observations for the boreholes are presented on the borehole logs on **Enclosures 2 through 5**. Further discussion on groundwater is provided in **Section 4.2** of this report.

3.2 GEOTECHNICAL LABORATORY TESTING

All soil samples were submitted to Sola's laboratory for natural moisture content determination. The results of the moisture content are presented on the borehole logs on **Enclosures 2 through 5**. In addition, two (2) representative soil samples were selected and submitted for testing of particle size distribution. The results of the laboratory tests are provided on **Enclosures 8 and 9**.

4.0 SUBSURFACE CONDITIONS

The detailed descriptions of the subsurface conditions encountered at each borehole location are given on the Borehole Logs on **Enclosures 2 through 5**.

The borehole data collected by Sola only represents the subsurface conditions at the borehole locations. It should be pointed out that the material boundaries indicated on the Borehole Logs are approximate and based on visual observations and interpolation between successive samples. These boundaries typically represent a transition from one material type to another and should not be regarded as an exact plane of geological change. It should also be noted that the subsurface conditions may vary across the site.

A summary of the characteristics for each unit of subsoil encountered within the borehole depths is given in the following paragraphs.

4.1 SOIL CHARACTERISATION

4.1.1 Topsoil

A layer of topsoil was encountered at all borehole locations. The thicknesses of topsoil was



measured to range from approximately 75 mm to 150 mm at the borehole locations.

It is important to note that topsoil thicknesses may vary throughout the site area, depending upon their location. As such, these findings should not be relied upon for any estimation of topsoil quantities to be stripped prior to construction.

4.1.2 Fill Materials (Including Probable Fill)

Fill materials were encountered at all borehole locations. The thicknesses of the fill materials at the borehole locations vary from approximately 0.7 m (BH1) to 1.4 m (BH2 and BH4). In BH1 underlying the fill, a 0.7 m thick layer of soil identified as Probable Fill was contacted. The fill (and probable fill) unit was found to extend to a depth of approximately 1.5 m in all boreholes.

Fill materials generally consisted of silty sand to sandy silt and clayey silt. The fill was generally brown in colour. In-situ resistance testing results ranged from 4 (BH2 and BH4) to 24 (BH1) blows per 300 mm of spoon penetration, indicating that the fill was not constructed under engineering control.

In the fill layer, the moisture content of the samples recovered ranged from 15.9% (BH3) to 21.3% (BH2), indicating a moist condition.

4.1.3 Clayey Silt

A clayey silt deposit was encountered below the fill in borehole BH3 at the depth of approximately 1.5 m and extended to the depth of approximately 2.3 m below the ground surface.

SPT “N” value for the clayey silt layer was recorded to be 11 blows per 300 mm of spoon penetration, indicating that the soil is in a stiff condition.

In the clayey silt soil layer, the moisture content of the sample recovered was approximately 14.4%, indicating a moist condition.

4.1.4 Glacial Till

Clayey silt till and silty clay till deposits were encountered below the fill materials or clayey silt deposit in all borehole locations, at the depth ranging from approximately 1.5 m (BH1, BH2 and BH4) to 2.3 m (BH3) below the ground surface. All boreholes were terminated in these deposits.



The composition of the till was found to change from primarily clayey silt with trace to some sand and gravel to a relatively more clayey till (i.e. silty clay till) with trace of sand and gravel at the depth of about 4.5 m to 6.6 m below the ground surface. Owing to their mode of deposition, the presence of cobbles and boulders should always be anticipated in the glacial till deposits.

SPT “N” values for the glacial till deposits were recorded from 12 (BH2 and BH4) to 36 (BH1) blows per 300 mm of spoon penetration, indicating that the deposits to be in a stiff to hard condition.

In the glacial till deposits, the moisture content of the samples recovered ranged from approximately 12.2% (BH3) to 18.3% (BH1), indicating a moist to very moist condition.

4.2 GROUNDWATER

The groundwater conditions encountered during drilling and cave in depths are presented on the borehole logs on **Enclosures 2 through 5** as well as in **Table 1**.

Table 1: Borehole Water Depth and Cave-in Upon Completion of Drilling

Borehole Number	Water Depth Upon Drilling Completion (mBGS)	Cave-in Depth Upon Drilling Completion (mBGS)	Groundwater Depth (mBGS) taken by Project Hydrogeologist on May 25, 2021
BH1	Dry	Open	4.80
BH2	Dry	Open	1.15
BH3	Dry	Open	4.15
BH4	Dry	Open	3.50

Note: mBGS = meters below ground surface

It should be noted that water levels can vary in response to seasonal fluctuations and major weather events. In addition, a perched water condition can occur due to the accumulation of surface water in the more pervious fill overlying less pervious deposits, especially during seasonally wetter periods.

Long-term “stabilized” groundwater level measurements should refer to the project hydrogeology study.

5.0 DISCUSSION AND RECOMMENDATIONS

The investigation and comments should be considered ongoing as new information about the underground conditions will continue to become available. When more specific information is available with respect to the



soil conditions, the interpretation and the recommendations of this report must therefore be checked through field inspections carried out by Sola to validate the information for use during construction.

For this preliminary investigation, the details of the proposed development have not been made available. It is understood that the Client is contemplating developing the site with single-storey slab-on-grade industrial buildings with office spaces. A supplementary investigation will be required according to the building footprints for the detailed design, when available. Based on the ground conditions found at the site, our recommendations are presented in the following sections.

5.1 FROST PROTECTION

All footings and structural elements exposed to seasonal freezing conditions must have at least 1.2 metres of permanent soil cover, or equivalent artificial insulation, for frost protection.

5.2 CONVENTIONAL SPREAD OR STRIP FOUNDATIONS

At the time of preparation of this report, design loading requirements have not been made available. The following discussions are provided to assist the preliminary design phase of the proposed industrial subdivision. For geotechnical design purposes, it is assumed that the footings will be positioned below the frost penetration depth, i.e., at least 1.2 m below the finished grade.

Based on borehole data, the proposed industrial development can be supported by spread and strip footings founded on undisturbed native soil and designed for geotechnical reactions at Serviceability Limit States (SLS) and factored geotechnical resistances at Ultimate Limit States (ULS) at the depths as outlined in **Table 2**.

Table 2: Bearing Resistances and Founding Depths

Borehole Number	SLS (kPa)	ULS (kPa)	Founding Depth (mBGS)	Founding Stratum
BH1	200	300	1.5	Clayey Silt Till
BH2	120	180	1.5	Clayey Silt Till
	160	240	2.3	Clayey Silt Till
BH3	100	150	1.5	Clayey Silt
	160	240	2.3	Clayey Silt Till
BH4	200	300	1.5	Clayey Silt Till

It is assumed that the dimensions of the footing units will not be greater than 3 x 3 m (square) or 1.0 m wide (strip). Larger footings may yield larger settlements and must be reviewed by the Geotechnical Engineer during the detailed structural design.



Alternatively, the footings can be founded on engineered fill. This would involve stripping of the existing fill to the surface of suitable native soils, inspecting and compacting from the surface, and backfilling in shallow layers of not more than 300 mm in thickness when first placed i.e., before applying compaction. Each layer would be compacted to not less than 100% of the Standard Proctor Maximum Dry Density (SPMDD). Imported granular fill would be utilized for this purpose. The entire process would be conducted under the supervision of geotechnical personnel from this office. An SLS value of 150 to 200 kPa and a ULS value of 225 to 300 kPa can be utilized depending on the property of the fill used and compaction procedures, including the degree of compaction. We will be pleased to provide more details of this procedure if it is to be considered.

Alternatively, a “trench-and-pour” construction technique can be utilized. In order to facilitate the construction, it is prudent to excavate a few test pits prior to construction in the general area to examine whether the trench walls can remain relatively stable for the proposed footing construction.

The design values provided above are based on the presumption that the bearing resistance at SLS is governed by total and differential settlements of 25 mm and 19 mm respectively, and the structure will tolerate an angular distortion of 1 in 300.

Where it is necessary to place footings on the soil at a different level, the upper footing must be founded below an imaginary 10 horizontal to 7 vertical line (10H:7V) drawn up from the base of the lower footing. The lower footing must be installed first to minimize the risk of undermining the upper footing.

Footings and any foundation wall should be reinforced as per the design to be provided by the Structural Engineer of the project.

The recommended bearing resistances and the corresponding founding elevations would need to be confirmed by geotechnical engineering staff at the site prior to pouring footing concrete.

It should be noted that the recommended bearing resistances have been calculated by Sola from the borehole information for the design stage only. Should higher bearing values be required, this office should be contacted to review this report.

Foundation walls and columns should be protected against heave due to adfreeze. Where construction is undertaken during winter conditions, footing subgrades should be protected from freezing.



5.3 EARTHQUAKE CONSIDERATIONS

Using the information provided by the site investigation, the general soil profile comprises “*Stiff Soil – Site Class D*” as defined by Table 4.1.8.4.A “*Site Classification for Seismic Site Response*” of the Ontario Building Code.

For industrial building construction, cost savings may be achieved if the Site Classification can be upgraded through shear wave velocity testing. This testing can be carried out by a specialist geophysics firm.

5.4 SLAB-ON-GRADE CONSTRUCTION

The existing topsoil and fill within the proposed building footprint should be removed to a depth of not less than 1.0 m below the existing ground surface. Depending on the design grade and loading conditions, some of the existing geotechnically and environmentally clean fill may be reused to raise the grade after striping to a depth of 0.5 m below the proposed floor slab, depending on the loading conditions. After striping, the exposed soil subgrade must be inspected, evaluated and approved. The approved subgrade should then be proof rolled to detect any soft or unstable areas, which must be removed and replaced with suitably compacted engineered fill, as defined in **Section 5.9** of this report. Once the required subgrade has been developed, Sola recommends that the exposed subgrade be inspected and approved by the Geotechnical Engineer before the placement of any granular fill or concrete.

For highly loaded floor areas (i.e., warehouses, etc.) sensitive to settlements, it is recommended that engineered fill be used. For this purpose, the site should be stripped of all the existing fill, and the subgrade should be approved by Sola. Upon approval, the on-site excavated clean selected material can be used to raise the grade to a depth of about 1.0 m below the bottom of the floor slab. We recommend that the remaining portion of the fill should consist of imported clean granular fill such as Granular ‘B’ material, type 2. Under light-loaded floor areas, which may not be sensitive to settlements, the existing fill can selectively be used to raise the grade to a depth of 0.5 m below the underside of the floor slab. For normal duty concrete floor-slab, it is recommended that an at least 200 mm thick layer of either OPSS Granular A or 20 mm Crusher-Run Limestone (to top over and above the Granular ‘B’) should be used and compacted to at least 100% SPMDD. For heavy-duty floor slabs, the granular thickness should be increased to 300 mm. These recommendations need to be adjusted when the details are known.

The minimum acceptable degree of compaction for the backfill typically ranges between 98% and 100% of the SPMDD depending on the details of the project.



It is considered by Sola that completed excavations for floor slabs should not be left open before pouring concrete for any period longer than 24 hours, particularly if the floor construction works are being completed during the winter months or wet weather periods. The base of any floor slab excavation that is to be left exposed for longer than 24 hours should be suitably covered and protected from water ponding, and/or protected to prevent degradation of the exposed founding stratum with the construction of a mud mat.

Prior to placing the stone bedding, the final subgrade should be proof-rolled and approved by a Geotechnical Engineer.

The design of the concrete slabs on improved fill may be made on the basis of a value of modulus of subgrade reaction which is 15 MPa/m on the surface of the granular moisture barrier.

The floor slab should be structurally independent from any load-bearing structural elements.

5.5 PERMANENT DRAINAGE CONSIDERATIONS

The finished exterior ground surface should be sloped away from the proposed industrial development area at a minimum cross-fall of 2%.

Perimeter drainage should be provided around all floor slab areas where water may accumulate. The perimeter drainage is not required if the interior finish floor elevation is at least 200 mm higher than the exterior elevation. If the interior finish floor elevation is less than 200 mm, this office should be contacted, and the drainage details can be provided. Based on the groundwater condition at the site, underfloor drains may not be required, however, the need for a subfloor drainage system should be determined by the designer in accordance with the latest Ontario Building Code requirements.

5.6 SITE PREPARATORY WORKS

The site preparation work may include stripping of the ground cover and existing fill in order to develop the required construction or engineered fill subgrades. Depending on the final grading plan, stripping depths will likely vary locally and should be adjusted to remove all unsuitable material.

It is recommended that the Geotechnical Engineer monitor the stripping operations to ensure that unsuitable materials have been fully removed prior to construction works or the placement of engineered fill. Unacceptable areas identified are to be remediated as soon as practicable and, the procedures would be dependent upon conditions encountered.



5.7 EXCAVATABILITY AND SITE EXCAVATIONS

It has been assumed that in general excavations for the building and utilities will be open cut. In order to enable entry into excavations during the construction process, all excavations must comply with the definitions prescribed by the *“Occupational Health and Safety Act”* (OHSA), Ontario Regulation 213/91 *“Construction Projects”*.

Unless properly tapered, the sides of the excavation will not remain stable for a prolonged period of time. The borehole data indicate that the native glacial till deposits can be classified as a Type 2 material as defined in the OHSA and Regulations for Construction Projects (Part III Excavations, Section 226); native clayey silt deposit and fill, Type 3 above groundwater and Type 4 below groundwater. Excavations in these materials should be constructed in conformance with the regulations. It is noted that the above classifications have been estimated based on small, discontinuous samples from boreholes. The excavation conditions must be confirmed and/or modified on the basis of field inspections during the construction stage when large-scale observations can be made with ease.

As defined by the OHSA, excavation walls within the Type 3 soils will require battering back at slopes no steeper than 1H (horizontal):1V (vertical) and flatter for Type 4 material. Within the fill materials, a flatter than 1:1 side slope may be required even above the water table. For Type 2 material, the bottom 1.2 m high of the trench wall can be vertical, for temporary conditions.

Depending on the construction feasibility the excavation walls can be supported by temporary shoring systems. During excavations, adjacent existing structures and public right of way, if present, must be protected by proper shoring or sloping.

Based on the findings of the investigation, it is considered that excavation of the overburden soils at the site can be carried out using a conventional backhoe excavator.

It is important to note that the above discussion about the excavation is for information purposes only. Contractor bidding on the projects must make their own assessment based on the real site conditions.

Cobbles and boulders were inferred in the boreholes and are expected to be in the glacial till deposits. The contractor carrying out the excavation work should account for removing cobbles and boulders in their site excavation work.

It is assumed that the groundwater will be lowered to 1.0 m below the required excavation depth to enable the construction to be carried out in the ‘dry’ condition. It is expected that the ‘perched water’



can be controlled by the conventional 'sump and pump' methodology. If more aggressive dewatering methods are required, a dewatering specialist should be consulted.

5.8 CONSTRUCTION DEWATERING

The borehole data have indicated that no unusual groundwater seepage problems should be expected during excavation and 'perched water' can be controlled by conventional sump pumping. However, the construction dewatering requirements should refer to the project hydrogeology study.

5.9 ENGINEERED FILL

On-site excavated, clean inorganic earth (native and/or fill) may selectively be reused as engineered fill material, provided that the moisture contents are strictly controlled.

If imported inorganic mineral soils are used for engineered fill construction, they must meet the applicable environmental guidelines, and their moisture contents should preferably be close to their respective optimum water content values.

The soil should be placed in thin lifts and suitable compaction equipment should be employed to achieve the specified degree of field density. The on site excavated clayey soils can be expected to require heavy sheepsfoot or padfoot type compacters to achieve a high degree of compaction. However, vibrations due to compaction may need to be reduced or curtailed to prevent damage to the existing structures and public right of way.

Consideration may also be given to backfilling excavations with a well-graded, compacted granular soil such as Granular B as it, if thoroughly compacted, would reduce the post-construction settlements to an acceptable level and may also expedite the compaction process.

Fill materials required for replacing locally softened soils or raising grades within the footprint of the structures and paved areas are to comprise suitably organic free materials approved for use by a Geotechnical Engineer. Fill materials are to be placed in lifts of a maximum thickness of 300 mm and compacted, using appropriate compaction equipment, to at least 98 % of its SPMDD.

Fill located in areas outside of the footprint of any proposed structure or paved areas should be compacted to at least 95 % of the material's SPMDD below 1.0 m of the subgrade level, and then to at least 98 % of its SPMDD up to the required grade. Imported granular fill used in confined areas should be compacted using only hand-held compaction equipment only.

Sola recommends that any and all engineered subgrades beneath proposed structures including



pavements be inspected and proof rolled prior to construction.

5.10 PAVEMENT

Pavement structure adjoining the proposed construction areas should be protected from damages resulting from construction activities. All heavy vehicles should be appropriately planned and re-routed to avoid such damages.

5.10.1 Pavement Thickness Design

For pavement construction, if contemplated, the existing subgrade soils, when compacted and proof rolled in the presence of Geotechnical personnel, can be expected to be competent to support a conventional pavement structural thickness. Any unsuitable soils, such as topsoil/organic mixed soil and other spongy materials, if found, should be sub-excavated and replaced with approved materials and the profiled subgrade compacted to not less than 98% of its SPMDD.

The pavement construction may consist of upfilling (if applicable) from the prepared subgrade surface to the underside of the granular base layer using a well-graded granular subbase material (OPSS Granular B-Type I) up to a maximum thickness of 500 mm. The material should be laid and compacted in thin lifts to at least 100% of their SPMDD. Per the County of Middlesex's Standard Details, we recommend the pavement design shown in **Table 3**. It is assumed that there will be only occasional delivery trucks allowed for light-duty areas. In the areas where fire routes and loading dock approaches, the heavy-duty pavement design should be implemented.

Table 3: Recommended Pavement Design

Pavement Component	Light Duty Thickness (mm)	Heavy-Duty Thickness (mm)	Compaction Requirements
Asphaltic Concrete Surface Course HL-3	40	40	Minimum of 92.0% of Maximum Relative Density (MRD)
Asphaltic Concrete Binder Course HL-8	50	80	
Granular Base (OPSS Granular 'A')	150	150	100% SPMDD
Granular Sub-Base (OPSS Granular 'B')	300	450	



The recommended granular base and sub-base materials shall meet the OPSS 1010 requirements. The granular base and subbase should be compacted to at least 100% of their SPMDD.

The asphaltic concrete courses are to be hot-mixed and hot-laid in accordance with current OPSS specifications and compacted to a minimum of 92% of Maximum Relative Density (MRD).

The pavement design as presented above in **Table 3** assumes that construction will be undertaken under dry weather conditions and that the subgrade is stable and not heaving under construction equipment traffic. However, if the construction conditions are non-ideal, with the final subgrade being wet and/or unstable, additional imported subbase material may become necessary.

The pavement make-up for the entrance driveways should match the respective road pavement design at the road/driveway interface. It may be preferable to use concrete pavements at loading docks.

Prior to placing the granular subbase, the final subgrade should be proof rolled to identify soft spots, if any, and rectified as required in consultation with a Geotechnical Engineer.

The recommended pavement structure should be considered for preliminary design purposes only. The functional design life of eight (8) to ten (10) years has been used to establish the pavement recommendations. This represents the number of years to the first rehabilitation, assuming regular maintenance is carried out. If required, a more refined pavement structure design can be performed based on specific design life requirements. Such further analysis will also involve specific laboratory tests to determine the frost susceptibility and strength characteristics of the subgrade soils, as well as specific traffic loading data input from the Client.

Pavement Drainage: The ability of the soils to provide adequate subgrade support is reduced if allowed to become too wet. Therefore, in order to intercept infiltrating water and provide drainage of the subgrade and pavement material, it is recommended that 100 mm diameter sub-drains, wrapped in filter cloth, be provided along both sides of the driveways; in addition, similar sub-drains should be installed in four (4) directions from the catch basins and at strategic locations under the parking lot pavement. Furthermore, the subgrade should be graded to promote the flow of water towards the subdrains.



5.10.2 Pavement Construction Considerations

For pavement construction, the subgrade must be compacted to at least 98% SPMDD, for at least the upper 300 mm, unless an alternative is approved by Sola.

The long-term performance of the pavement structure is highly dependent upon the subgrade support conditions. Stringent construction control procedures should be maintained to ensure uniform subgrade moisture and density conditions are achieved.

Additional comments on the construction of pavement areas are as follows:

- The subgrade preparation should include stripping of any objectionable materials, e.g., loose fill with organics. The subgrade surface should be properly shaped and thoroughly proof rolled using suitable equipment. Soft and/or unstable subgrade areas should be further sub-excavated and backfilled to the design subgrade level using an approved material, placed in thin lifts, and compacted to at least 98% of its SPMDD;
- The locations and extent of sub-drainage required within the paved areas should be reviewed by this office in conjunction with the proposed grading. Assuming that satisfactory crossfalls in the order of 3% have been provided, subdrains extending from and between catch basins may be satisfactory. In the event that flatter crossfalls are considered, a more extensive system of sub-drainage may be necessary and should be reviewed by Sola; and,
- The most severe loading conditions on the pavement areas and subgrade may occur during construction. Consequently, special provisions such as restricted access routes, half-loads during paving, etc., may be required, especially if construction is carried out during unfavourable weather.

It is recommended that Sola be retained to review the final pavement structure designs and drainage plans prior to construction to ensure that they are consistent with the recommendations in this report.

5.11 SERVICE INSTALLATION CONSIDERATIONS (WHERE APPLICABLE)

5.11.1 General

The materials found in the boreholes at the expected elevations of the proposed servicing trench generally consist of competent soils. In general, the native materials are suitable for pipeline support. Localized loose/soft subgrade conditions, if encountered during construction, should be sub excavated to a depth of at least 300 mm or to a firm base, if



shallower, and backfilled with clean, compactable materials and stabilized as per the project specifications. If the invert of the pipes falls within the fill soils, the fill should be removed and replaced with engineered fill, unless otherwise directed by the Geotechnical Engineer.

Prior to placement of bedding, the exposed subgrade at the bottom of each servicing trench excavation should be inspected by a Geotechnical Engineer to identify any soft, loose, or disturbed base conditions. All disturbed soils resulting from construction activities should be removed and replaced as noted above.

Design and construction considerations for both flexible (PVC) and rigid (concrete) pipes are included in the following sections.

5.11.2 Excavations and Health and Safety Considerations

The same recommendations as given in **Section 5.7** will generally apply to the excavations for laying of the underground services. The excavated soils should be placed not closer than the depth of the trenches from the trench edge.

5.11.3 Bedding

The improved fill materials and native subgrade in an undisturbed state will provide adequate support for the proposed service pipes and will allow the use of normal Class B type bedding. The bedding should conform to the current Ontario Provincial Standard Specifications (OPSS 1010) and/or the Middlesex County standards for bedding stone gradation requirements. The pipes should be placed with a minimum bedding thickness in conformance with Ontario Provincial Standard Drawing OPSD 802.010 (for flexible pipes) or OPSD 802.031 (for rigid pipes), though the bedding thickness will be subject to variation and ultimately be based on the proposed pipe diameter, bedding specifications used, etc. It is recommended that clear stone should not be used for bedding and as backfill above the obvert of the pipe, as soil fines from the silty subgrade may infiltrate into the voids of the clear stone, giving rise to settlements of the surface pipes and the trench surface, after the trenches are backfilled.

On completion of the servicing pipe installation, a granular surround of the same bedding material should be placed around the pipe to cover it to at least 300 mm above the pipe obvert.

The backfill above the bedding and cover materials may consist of clean, compactable fill. Based on the borehole data it is anticipated that some of the local soil material can selectively be reused as trench backfill, subject to approval by Geotechnical personnel. Some moisture



conditioning of the soil may be required to facilitate soil compaction. In the event that imported soil is used as a trench backfill, it must be ensured that the drainage properties of the subgrade are maintained and that there is no differential frost movement. Trench backfill should be compacted to at least 97% of the material's SPMDD, or Middlesex County standards, whichever is more stringent. Within the top one meter, the degree of compaction should be increased to at least 98% of the SPMDD of the material.

5.11.4 Trench Backfill

Backfilling During Dry-Weather Conditions

The excavated fill soils, if approved by the Geotechnical personnel at the time of construction, are considered suitable for re-use as fill to backfill service trenches, provided that suitable compaction equipment can be used to compact the fill material. However, the clayey soils will require heavy sheepsfoot or padfoot type compactors to achieve a high degree of compaction. The use of heavy compactors in the narrow confined service trenches may not be feasible. In confined areas, consideration may be also given to backfilling the areas with a well-graded, compacted granular soil such as Granular 'B' material. As such material, if thoroughly compacted, would reduce the post-construction settlements to an acceptable level and may also expedite the compaction process. However, proper tapering should be provided to prevent differential frost heave of the paved surface.

Each lift should be no greater than 300 mm thick when first placed and compacted using an appropriate heavy compaction machine to at least 95 % of the material's SPMDD to within 1 m of the top of the subgrade, and then to at least 98 % SPMDD up to the required grade.

Exposed, excavated soil stockpiles that are to be reused as fill on-site should be compacted at the surface or temporarily covered during wet weather to help maintain their original moisture content. Such stockpiles are prone to wet weather exposure and, as such, the increased moisture contents will make these materials too wet to achieve the required levels of compaction.

Conversely, if the excavated soils are too dry to achieve the required levels of compaction, some moisture addition/conditioning by means of water hosing or misting should be expected.

We recommend the subgrade be observed and approved by a Geotechnical Engineer prior to the placement of the bedding material to confirm that the subgrade conditions are consistent with the recommendations given in this report. Where unsuitable subgrade



conditions are observed, remedial procedures can be established in the field to avoid construction delays.

Backfilling During Winter Months

Should this project proceed during the winter months or when the ambient temperatures are below freezing, the following additional recommendations will apply in order to avoid any detrimental effects of frost.

In this situation, it is imperative that the excavation and backfilling operations follow simultaneously. This procedure is required to avoid time gaps between the two construction stages, as prolonged exposure to frost may lead to the inclusion of frozen material during backfilling. It is recommended that prior to resuming backfilling over the frozen surface, all frost should be removed to achieve a satisfactory bond between the current and previously laid fills. Also, this procedure would prevent leaving frozen layers of soils which could cause long-term settlements while undergoing slow thawing.

It is further recommended that any accumulation of water or ice in the small sheepsfoot compactor footprint overnight or weekends should be prevented by adequately shaping up and back blading the compacted grades prior to leaving the site.

In order to ensure that no frozen material is being backfilled in the trenches, it is recommended that the backfilling and compaction operations should be supervised and closely monitored by Sola on a continuous basis.

For the construction of the parking lot, the final subgrade should be prepared during 'dry weather' conditions so as to achieve a satisfactory end product.

5.12 CONSTRUCTION CONSIDERATIONS

Load-bearing soils are susceptible to disturbance from environmental factors (temperature, moisture change, etc.) and construction activity. Therefore, due care should be given to minimizing the trafficking of such areas during periods of excavation and the construction of the floor slab and footings to minimize the disturbance of the bearing soils.

Any excessive disturbances of the load-bearing and underlying soils affected during construction works could influence the long-term settlement of the structures and will therefore require further excavation and replacement of such impacted soils with suitable engineered fill.



During winter seasons, foundations and slab-on-grade construction should be carried out to avoid pouring concrete on frozen soil. Foundations must be adequately protected at all times from cold weather and freezing conditions.

A Geotechnical Engineer should evaluate all subgrade surfaces to confirm that the subgrade and founding conditions are consistent with the recommendations given by this report.

6.0 MATERIAL TESTING AND INSPECTION

It is recommended that Sola be appointed to carry out field inspection and materials testing during construction to ensure that the construction complies with the design recommendations.

7.0 DRAWING REVIEW

Once the final design drawings for this project are prepared, it is recommended that one (1) set of the drawings should be submitted to Sola for review and to make any amendments to our recommendations that may be required, prior to starting construction. Adequacy of the existing subgrade condition should be checked by Sola.

Sola should also be retained for a general review of the final design and specifications to verify that this report has been properly interpreted and implemented. If not accorded the privilege of making this review, Sola will assume no responsibility for the interpretation of the recommendations in this report.

The comments given in this report are preliminary and intended only for the guidance of design engineers. Contractors bidding on or undertaking the works should make their own interpretations of the factual borehole results, so that they may draw their own conclusions on how the subsurface conditions may affect them.

The information in this report in no way reflects on the environmental aspects of soil conditions at the site and has not been addressed in this report, since this aspect was beyond the scope and terms of reference.



8.0 CLOSURE

This report is subject to the Statement of Limitations which forms an integral part of this document. The Statement of Limitations is not intended to reduce the level of responsibility accepted by Sola, but rather to ensure that all parties who have been given reliance for this report are aware of the responsibilities each assumes in so doing.

We trust that this report meets your needs. Should you have any queries, please contact the Sola office.

Sincerely,

SOLA ENGINEERING INC.

George Hao P. Eng.



Bill Feng P. Eng.

Chief Engineer

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Enclosures



STATEMENT OF LIMITATIONS

Standard of Care and Basis of this Report

Sola Engineering Inc. ("Sola Engineering") has prepared this report in a manner consistent with generally accepted engineering and/or environmental practices in the jurisdiction in which the specified services were provided. The information and conclusions set out in this report reflects Sola Engineering's best professional judgment in light of the information available to Sola Engineering at the time of preparation. Sola Engineering disclaims any and all warranties, express or implied, including without limitation any warranty of merchantability and/or fitness for a particular purpose, and makes no representations concerning the legal effect, interpretation or significance of this report or the information, conclusions or recommendations contained in it.

The conclusions and recommendations provided in this report have been prepared in relation to the specified site (the "Site") and the proposed project (the "Project"), as described by the Client to Sola Engineering. Given the nature of the work undertaken by Sola Engineering as part of this report, the Client acknowledges that ground conditions may vary over distances and may change over time. Should there arise any changes to the conditions of the Site or the Project (as to purpose or design), Sola Engineering is to be notified within a reasonable period of time, and in any event within 24 hours of the Client's learning of such changes, so as to give Sola Engineering an opportunity to review and revise this report in light of such changes. Sola Engineering accepts no liability or responsibility for any use of this report or reliance on this report following any changes to the conditions of the Site or the Project.

The scope of professional services provided by Sola Engineering for the Project are as set out in this report. Should such services be limited to those of a geotechnical nature, Sola Engineering shall not be held liable or responsible for any environmental services that may be required, nor shall this report be interpreted to reflect any environmental aspects of the Project. Alternatively, should such services be limited to those of an environmental nature, Sola Engineering shall not be held liable or responsible for any geotechnical services that may be required, nor shall this report be interpreted to reflect any geotechnical aspects of the Project.

This report is not intended to provide recommendations for possible future conditions or use of the Site or adjoining properties. Should the need arise for such recommendations Sola Engineering may need to conduct further investigations.

Use of this Report

This report is intended to be read and used in its entirety. No reliance may be made upon any individual portion or section of this report without reference to the entire report as a whole. In preparing this report, Sola Engineering has relied on information, instructions and communications given by the Client to Sola Engineering, the applicability, truth and accuracy of which is the sole responsibility of the Client.

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Site Conditions

The material conditions, classifications, conclusions and recommendations contained in this report were based on the site conditions observed or tested by Sola Engineering or otherwise communicated to Sola Engineering by the Client. The description, identification and classification of soils, rocks, chemical contamination and other materials have been made based on limited investigations, sampling and testing of materials performed by Sola Engineering and its qualified representatives in reliance on the use of relevant or applicable equipment, all in accordance with commonly acceptable standards in the geotechnical and/or environmental disciplines. Accordingly, this report may include assumptions of conditions which are based on discrete sample locations and thus some conditions may not have been detected. The Client accepts all liability and risk for the use of this report and the information and data contained in it. Sola Engineering shall not be held liable or responsible for any conditions beyond the scope of tests conducted on samples of the subsurface and soil conditions of the subject property as set out in this report.

For clarity, the Client acknowledges and accepts that unique risks exist whenever engineering or related disciplines are applied to identify subsurface conditions and even a comprehensive sampling and testing program may fail to detect certain conditions. The environmental, geological, geotechnical, geochemical and hydrogeological conditions that Sola Engineering interprets to exist between sampling points may differ from those that actually exist. As a result, the Client acknowledges and accepts that because of the inherent uncertainties in subsurface evaluations, unanticipated underground conditions may occur or become known subsequent to Sola Engineering's investigation that could affect conclusions, recommendations, total Project cost and/or execution.

Indemnification of Risk

Though Sola Engineering adheres to the highest degree of integrity and employs due diligence in limiting the potential release of toxins and hazardous substances, the risk of accidental release of such substances is a possibility when providing geotechnical and environmental services.

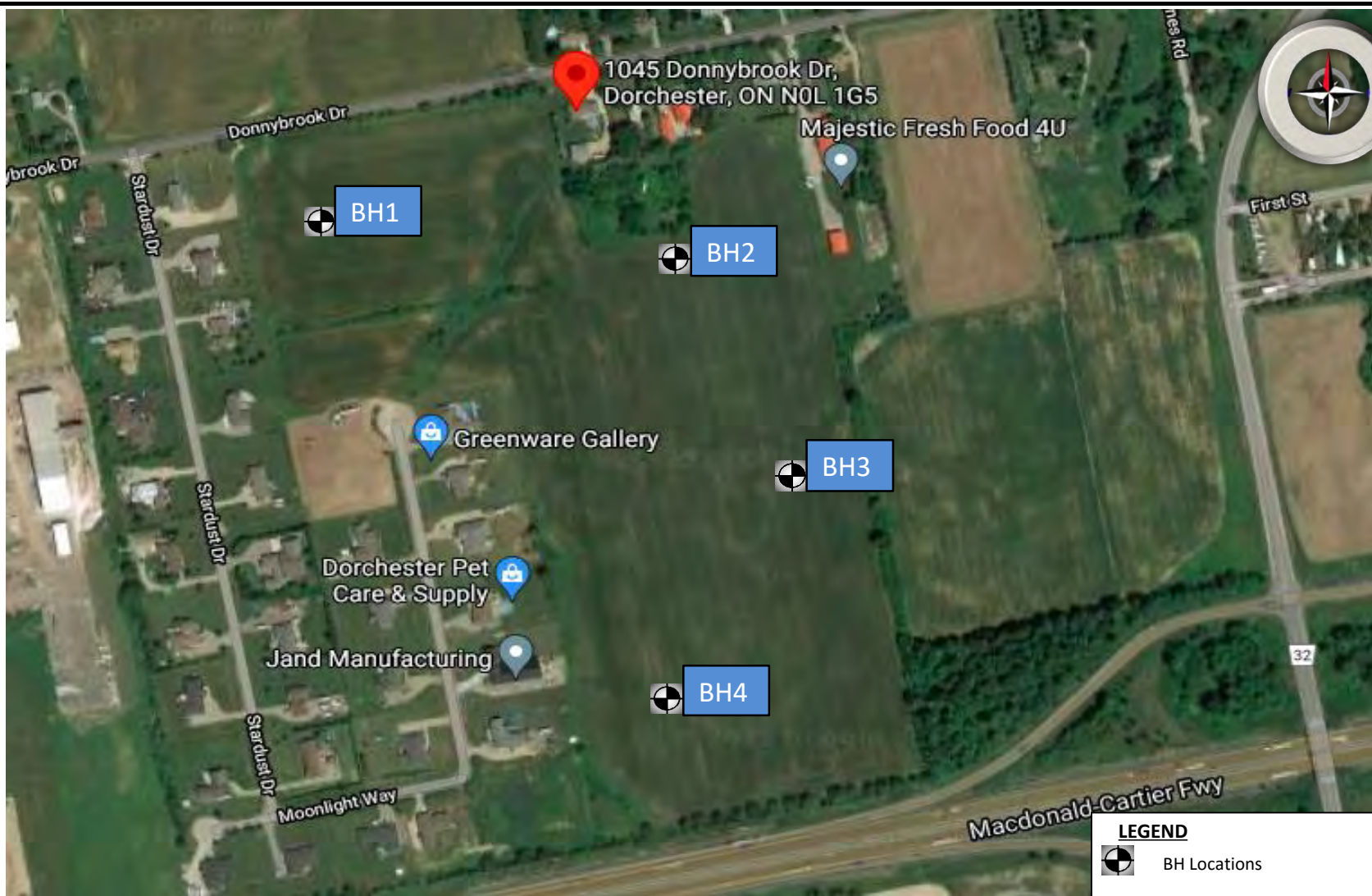
In consideration of the provision of services by Sola Engineering, the Client agrees to defend, indemnify and hold Sola Engineering and its employees and agents harmless from and against any and all claims, liabilities, damages, causes of action, judgments, costs or expenses (including reasonable legal fees and disbursements), resulting from or arising by reason of the death or bodily injury to persons, damage to property, or other loss, whether related to an accidental release of pollutants or hazardous substances occurring as a result of carrying out this Project or otherwise, and whether or not resulting from Sola Engineering's negligent actions or omissions. This indemnification shall include and extend to any and all third party claims brought or threatened against Sola Engineering under any federal or provincial law or statute as a result of Sola Engineering conducting work on the Project. In addition to and notwithstanding the foregoing, the Client further agrees to unconditionally and irrevocably release Sola Engineering from, and not to bring any claims against Sola Engineering in connection with, any of the aforementioned claims or causes.


Subconsultants and Contractor Services

In conjunction with the services provided by Sola Engineering's own employees, external services provided by other persons or entities that are specializing in services other than those offered by Sola Engineering, such as drilling, excavation and laboratory testing, are often employed in order to carry out the defined scope of work. If such external services have been employed for this Project, the Client acknowledges that Sola Engineering is not in any way liable or responsible for any costs, claims or damages in relation to the services rendered by such other persons or entities or payment therefor, nor shall Sola Engineering be liable or responsible for damages for errors, omissions or negligence caused by such other persons or entities while providing such external services.

Work and Job Site Safety

Sola Engineering shall be responsible only for its activities and that of its employees on the Site. Sola Engineering shall not direct any of the fieldwork nor the work of any other person or entity on the Project. The presence of Sola Engineering staff on the Site does not relieve the Client or any contractor on the Site from their responsibilities pertaining to site safety. The Client at all times retains any and all responsibility for the safety of those individuals present on the Site and/or working on the Project, including Sola Engineering's employees.



LEGEND
 BH Locations



File No.: 10826-S0456-GEO

Report Number: 2021-15454

Date: May 17, 2021

BH Location Plan

Proposed Industrial Subdivision

1045 Donnybrook Drive, Dorchester, Ontario

Lantern Capital

The figure provided is for the intended purpose of presenting the approximate borehole locations. This figure should not be used for any other purposes including construction, architecture or for accuracy of dimensions and orientation of objects.

Enclosure No.:

1

Not to Scale

RECORD OF BOREHOLE No. BH1

1 OF 1

METRIC

PROJECT NUMBER 10826 LOCATION 1045 Donnybrook Drive, Dorchester, Ontario ORIGINATED BY RS
DIST HWY BOREHOLE TYPE Solid Stem Augers COMPILED BY CC
DATUM DATE 2021.05.20 - 2021.05.20 LATITUDE LONGITUDE CHECKED BY GH

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)						
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									WATER CONTENT (%)			GR	SA	SI	CL
								○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	× LAB VANE												
0.0	Topsoil																						
0.1	TOPSOIL - 100 mm thick FILL - clayey silt, trace gravel, trace sand, brown, moist		1	SS	7																		
0.8	PROBABLE FILL - clayey silt, trace gravel, trace sand, brown, moist		2	SS	24																		
1.5	CLAYEY SILT TILL - trace gravel, trace sand, occasional inferred cobble and boulder, brown, very stiff to hard, moist		3	SS	32																		
			4	SS	36																		
			5	SS	28																		
			6	SS	21																		
6.1	SILTY CLAY TILL - trace gravel, grey, very stiff, moist		7	SS	16																		
6.6	End of Borehole at Targeted Depth; Borehole Was Open and Dry Upon Completion of Drilling; A Groundwater Measurement Was Taken By the Project Hydrogeology Team On May 25, 2021 and was Approximately 4.8 m Below Existing Ground Surface.																						

RECORD OF BOREHOLE No. BH2

1 OF 1

METRIC

PROJECT NUMBER 10826 LOCATION 1045 Donnybrook Drive, Dorchester, Ontario ORIGINATED BY RS
DIST HWY BOREHOLE TYPE Solid Stem Augers COMPILED BY CC
DATUM DATE 2021.05.20 - 2021.05.20 LATITUDE LONGITUDE CHECKED BY GH

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)						
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									WATER CONTENT (%)			GR	SA	SI	CL
								○ UNCONFINED	+	FIELD VANE	● QUICK TRIAXIAL	×					LAB VANE						
0.0	Topsoil																						
0.1	TOPSOIL - 100 mm thick FILL - clayey silt, trace gravel, trace sand, brown, moist		1	SS	6																		
			2	SS	4																		
1.5	CLAYEY SILT TILL - trace gravel, brown, stiff to very stiff, moist		3	SS	12																		
			4	SS	20																		
			5	SS	21																		
			6	SS	12																		
6.1	SILTY CLAY TILL - trace gravel, grey, stiff, moist		7	SS	14																		
6.6	End of Borehole at Targeted Depth; Borehole Was Open and Dry Upon Completion of Drilling; A Groundwater Measurement Was Taken By the Project Hydrogeology Team On May 25, 2021 and was Approximately 1.2 m Below Existing Ground Surface.																						

RECORD OF BOREHOLE No. BH3

1 OF 1

METRIC

PROJECT NUMBER 10826 LOCATION 1045 Donnybrook Drive, Dorchester, Ontario ORIGINATED BY RS
 DIST HWY BOREHOLE TYPE Solid Stem Augers COMPILED BY CC
 DATUM DATE 2021.05.20 - 2021.05.20 LATITUDE LONGITUDE CHECKED BY GH

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)						
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									WATER CONTENT (%)			GR	SA	SI	CL
								○ UNCONFINED	● QUICK TRIAXIAL	+ FIELD VANE	× LAB VANE												
0.0	Topsoil							20	40	60	80	100											
0.2	TOPSOIL - 150 mm thick		1	SS	5																		
0.8	FILL - silty sand, trace gravel, trace clay, brown, moist																						
			2	SS	10																		
1.5	CLAYEY SILT - trace gravel, brown, stiff, moist																						
			3	SS	11																		
2.3	CLAYEY SILT TILL - trace gravel, brown, stiff to very stiff, moist																						
			4	SS	14																		
			5	SS	20																		
4.6	SILTY CLAY TILL - trace gravel, brownish grey, very stiff, very moist																						
			6	SS	18																		
			7	SS	16																		
6.6	End of Borehole at Targeted Depth; Borehole Was Open and Dry Upon Completion of Drilling; A Groundwater Measurement Was Taken By the Project Hydrogeology Team On May 25, 2021 and was Approximately 4.2 m Below Existing Ground Surface.																						

RECORD OF BOREHOLE No. BH4

1 OF 1

METRIC

PROJECT NUMBER 10826 LOCATION 1045 Donnybrook Drive, Dorchester, Ontario ORIGINATED BY RS
DIST HWY BOREHOLE TYPE Solid Stem Augers COMPILED BY CC
DATUM DATE 2021.05.20 - 2021.05.20 LATITUDE LONGITUDE CHECKED BY GH

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)						
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									WATER CONTENT (%)			GR	SA	SI	CL
								○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	× LAB VANE												
0.0	Topsoil																						
0.1	TOPSOIL - 75 mm thick FILL - clayey silt, trace gravel, trace sand, brown, moist		1	SS	4																		
			2	SS	5																		
1.5	CLAYEY SILT TILL - trace gravel, trace sand, brown, very stiff, moist		3	SS	21																		
			4	SS	26																		
			5	SS	26																		
4.6	SILTY CLAY TILL - trace gravel, grey, stiff to very stiff, moist		6	SS	18																		
			7	SS	12																		
6.6	End of Borehole at Targeted Depth; Borehole Was Open and Dry Upon Completion of Drilling; A Groundwater Measurement Was Taken By the Project Hydrogeology Team On May 25, 2021 and was Approximately 3.5 m Below Existing Ground Surface.																						

PROJECT NUMBER _10826

LOCATION _1045 Donnybrook Drive, Dorchester, Ontario

PROJECT NAME _Proposed Industrial Subdivision

CLIENT _Lantern Capital

LITHOLOGIC SYMBOLS (Unified Soil Classification System)



CL-SL: clayey silt



CL-SL-TL: clayey silt till



FILL: TTC Fill (made ground)



SL-CL: silty clay



TOPSOIL: Topsoil/peat/organics

SAMPLER SYMBOLS



Split Spoon Sample

WELL CONSTRUCTION SYMBOLS



Bentonite Seal: 1 pipe group, 1 pipe



Concrete: 1 pipe group, 1 pipe



Filter Pack: 1 pipe group, 1 pipe



Slotted Pipe: 1 pipe group, 1 pipe



Slough at bottom of hole

Notes:

Terms describing RELATIVE DENSITY, based on Standard Penetration Test "N"-Value for COURSE GRAINED soils (major portion retained on No. 200 sieve):

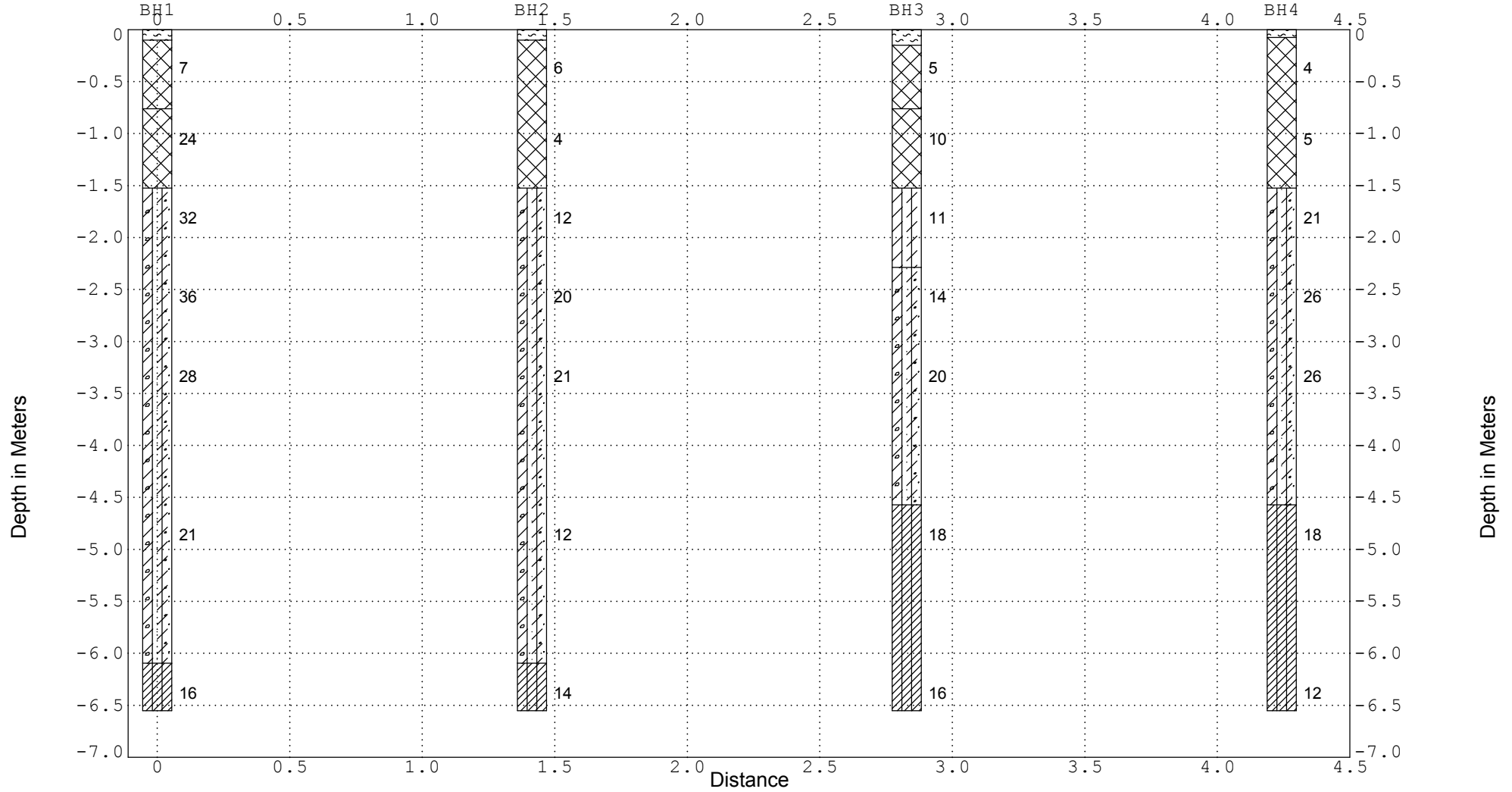
DESCRIPTIVE TERM ["N"-Value (blows/0.3m), Relative Density (%)]

- Very Loose [less than 4, less than 15]
- Loose [4 to 10, 15 to 35]
- Compact or Medium [10 to 30, 35 to 65]
- Dense [30 to 50, 65 to 85]
- Very Dense [greater than 50, greater than 85]

Terms describing CONSISTENCY, based on Standard Penetration Test "N"-Value for FINE GRAINED soils (major portion passing No. 200 sieve):

DESCRIPTIVE TERM [Unconfined Compressive Strength (kPa), "N"-Value (blows/0.3m)]

- Very Soft [less than 25, less than 2]
- Soft [25 to 50, 2 to 4]
- Firm [50 to 100, 4 to 8]
- Stiff [100 to 200, 8 to 15]
- Very Stiff [200 to 400, 15 to 30]
- Hard [greater than 400, greater than 30]



Plan View



SOLA ENGINEERING INC. CONCEPTUAL SOIL PROFILE

Horizontal Scale:

Drawn By:

Vertical Scale:

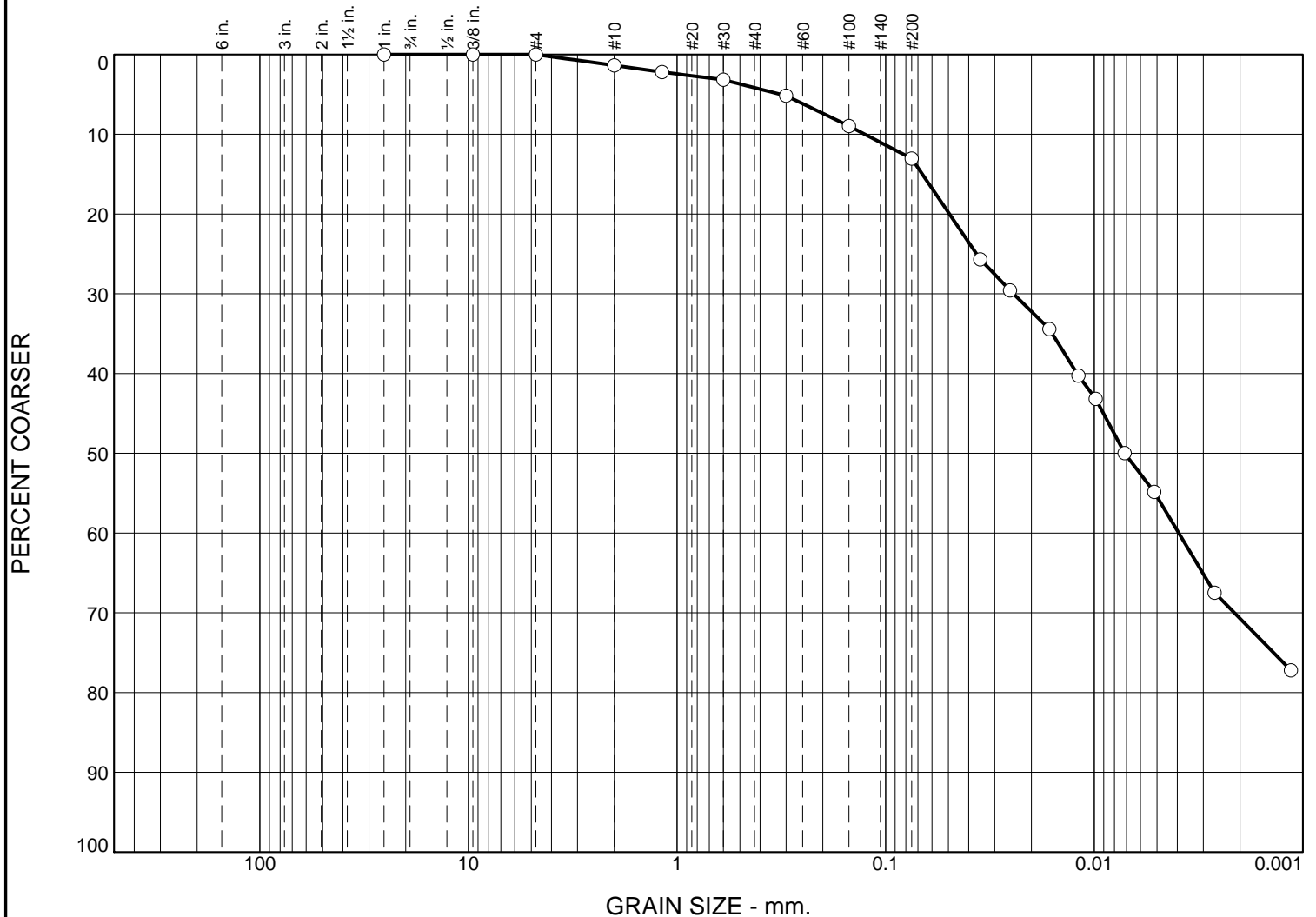
Approved By:

Proposed Industrial Subdivision
1045 Donnybrook Drive, Dorchester, Ontario

Project Number: 10826

Enclosure No.: 7

Particle Size Distribution Report

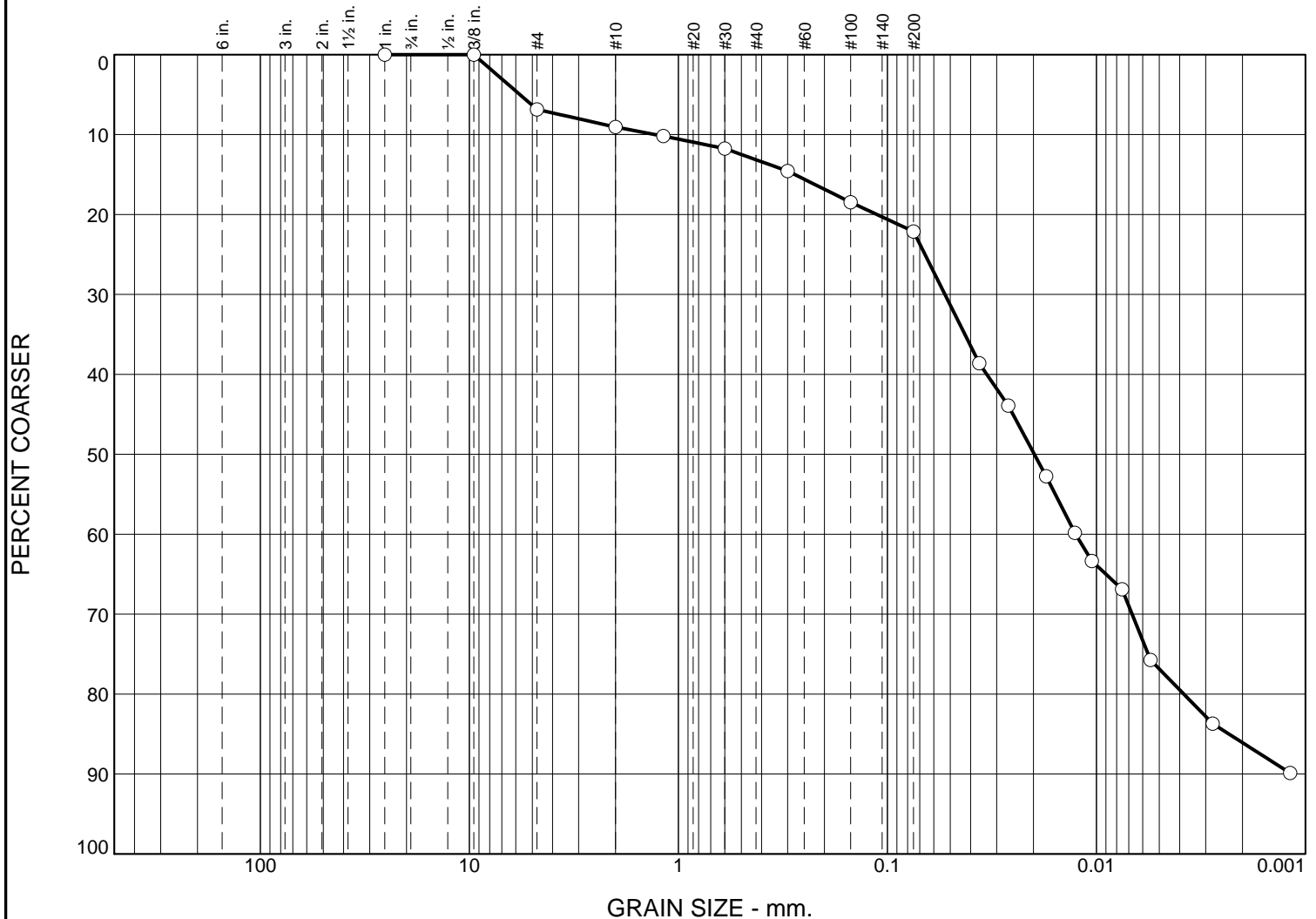


GRAIN SIZE - mm.											
% +3"		% Gravel		% Sand			% Fines				
		Coarse	Fine	Coarse	Medium	Fine					
○	0	0	0	1	3	9	87				
○											
×	Colloids	LL	PL	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
○				0.0667	0.0121	0.0071	0.0021				

Material Description									USCS	AASHTO
○ CLAYEY SILT TILL (VISUAL/MANUAL) CLAYEY SILT (LAB)										

Project No. 10826 Client: Lantern Capital Project: Proposed Industrial Subdivision Location: BH1 SS4 Sample Number: 21-204 Date: ○	Remarks: ○ Smapped By: Rattan Date: May 20, 2021 Note: Additional Information is available upon request
<div>SOLA ENGINEERING INC.</div>	

Particle Size Distribution Report



GRAIN SIZE - mm.											
% +3"		% Gravel		% Sand			% Fines				
		Coarse	Fine	Coarse	Medium	Fine					
0		0	7	2	4	9	78				
Colloids	LL	PL	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u	
			0.2777	0.0334	0.0198	0.0068	0.0023				

Material Description								USCS	AASHTO
CLAYEY SILT TILL (VISUAL/MANUAL) CLAYEY SILT WITH SAND (LAB)									

Project No. 10826 Client: Lantern Capital Project: Proposed Industrial Subdivision Location: BH4 SS5 Sample Number: 21-203 Date:	Remarks: Smapped By: Rattan Date: May 20, 2021 Note: Additional Information is available upon request
<div>SOLA ENGINEERING INC.</div>	

Appendix D

Pre-Development Conditions Hydrologic Modelling Output

=====

```

V   V   I   SSSSS U   U   A   L           (v 6. 2. 2006)
V   V   I   SS    U   U   A A   L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A   L
VV    I   SSSSS UUUUU A   A   LLLLL

```

```

000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM
0   0   T     T     H   H   Y Y   MM MM   0   0
0   0   T     T     H   H   Y   M   M   0   0
000   T     T     H   H   Y   M   M   000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\voir.n.dat

Output filename:

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Summary filename:

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DATE: 11/15/2021

TIME: 04:33:25

USER:

COMMENTS: Catchment Drains to Newton-Capstick Municipal Drain

```

*****
** SIMULATION : 100-year Storm **
*****

```

```

| CHI CAGO STORM |
| Ptotal = 79.37 mm |

```

IDF curve parameters: A=2619.363
 B= 10.500
 C= 0.884

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	3.30	1.08	23.09	2.08	12.82	3.08	4.80
0.17	3.56	1.17	38.91	2.17	11.32	3.17	4.56
0.25	3.86	1.25	92.77	2.25	10.11	3.25	4.34
0.33	4.23	1.33	232.24	2.33	9.13	3.33	4.14
0.42	4.67	1.42	118.26	2.42	8.32	3.42	3.95
0.50	5.21	1.50	67.39	2.50	7.63	3.50	3.79
0.58	5.89	1.58	45.00	2.58	7.04	3.58	3.63
0.67	6.78	1.67	32.92	2.67	6.54	3.67	3.49
0.75	7.96	1.75	25.56	2.75	6.10	3.75	3.36
0.83	9.61	1.83	20.68	2.83	5.71	3.83	3.24
0.92	12.05	1.92	17.26	2.92	5.37	3.92	3.13
1.00	15.97	2.00	14.74	3.00	5.07	4.00	3.02

```

-----
| CALIB |
| NASHYD ( 0001) | Area (ha)= 9.60 Curve Number (CN)= 83.0
| ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
-----
| U. H. Tp(hrs)= 0.69 |

```

Unit Hyd Qpeak (cms)= 0.531

PEAK FLOW (cms)= 0.658 (i)
 TIME TO PEAK (hrs)= 2.167
 RUNOFF VOLUME (mm)= 43.762
 TOTAL RAINFALL (mm)= 79.374
 RUNOFF COEFFICIENT = 0.551

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
=====
=====
V V I SSSSS U U A L (v 6.2.2006)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0

```

000 T T H H Y M M 000
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***** D E T A I L E D O U T P U T *****

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Summary filename:

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DATE: 11/15/2021

TIME: 04:33:25

USER:

COMMENTS: _____

```
*****
** SIMULATION : 10-year Storm                               **
*****
```

CHI CAGO STORM
Ptotal = 54.75 mm

IDF curve parameters: $A=1574.382$

B= 9.025

C= 0,860

used in: $INTENSITY = A / (t + B)^C$

Duration of storm = 4.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	2.53	1.08	15.60	2.08	8.95	3.08	3.58
0.17	2.71	1.17	25.83	2.17	7.96	3.17	3.41
0.25	2.93	1.25	61.71	2.25	7.17	3.25	3.26
0.33	3.19	1.33	162.47	2.33	6.51	3.33	3.12
0.42	3.49	1.42	79.04	2.42	5.97	3.42	2.99

0.50	3.87		1.50	44.47		2.50	5.51		3.50	2.88
0.58	4.34		1.58	29.77		2.58	5.12		3.58	2.77
0.67	4.94		1.67	21.95		2.67	4.77		3.67	2.67
0.75	5.73		1.75	17.20		2.75	4.47		3.75	2.57
0.83	6.83		1.83	14.05		2.83	4.21		3.83	2.49
0.92	8.44		1.92	11.83		2.92	3.98		3.92	2.41
1.00	11.00		2.00	10.20		3.00	3.77		4.00	2.33

```

-----
| CALIB |
| NASHYD ( 0001) |
| ID= 1 DT= 5.0 min |
-----
Area (ha)= 9.60 Curve Number (CN)= 83.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.69

```

Unit Hyd Qpeak (cms)= 0.531

PEAK FLOW (cms)= 0.351 (i)
 TIME TO PEAK (hrs)= 2.167
 RUNOFF VOLUME (mm)= 24.317
 TOTAL RAINFALL (mm)= 54.748
 RUNOFF COEFFICIENT = 0.444

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
=====
=====
V V I SSSSS U U A L (v 6.2.2006)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

```

```

000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0
000 T T H H Y M M 000

```

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***** D E T A I L E D O U T P U T *****

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Summary filename:

C: \Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\0
b10d70d-72d6-4d41-b175-c87fb115e121\

DATE: 11/15/2021

TIME: 04: 33: 25

USER:

COMMENTS: _____

** SIMULATION : 25-year Storm **

| CHICAGO STORM | IDF curve parameters: A=2019.372
| Ptotal = 64.46 mm | B= 9.824
C= 0.875

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	'	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.78	1.08	18.53	'	2.08	10.41	3.08	4.00
0.17	2.99	1.17	31.05	'	2.17	9.22	3.17	3.81
0.25	3.24	1.25	74.37	'	2.25	8.27	3.25	3.63
0.33	3.54	1.33	190.82	'	2.33	7.48	3.33	3.47
0.42	3.90	1.42	95.08	'	2.42	6.83	3.42	3.32
0.50	4.34	1.50	53.76	'	2.50	6.28	3.50	3.18
0.58	4.89	1.58	35.88	'	2.58	5.81	3.58	3.06
0.67	5.60	1.67	26.31	'	2.67	5.41	3.67	2.94
0.75	6.54	1.75	20.49	'	2.75	5.05	3.75	2.83
0.83	7.86	1.83	16.63	'	2.83	4.74	3.83	2.74
0.92	9.80	1.92	13.93	'	2.92	4.47	3.92	2.64
1.00	12.91	2.00	11.93	'	3.00	4.22	4.00	2.56

| CALIB |

NASHYD (0001)	Area (ha)=	9.60	Curve Number (CN)=	83.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res. (N)=	3.00
-----	U. H. Tp(hrs)=	0.69		

Unit Hyd Qpeak (cms)= 0.531

PEAK FLOW (cms)= 0.468 (i)
 TIME TO PEAK (hrs)= 2.167
 RUNOFF VOLUME (mm)= 31.715
 TOTAL RAINFALL (mm)= 64.464
 RUNOFF COEFFICIENT = 0.492

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 =====
 =====

V	V	I	SSSSS	U	U	A	L		(v 6.2.2006)
V	V	I	SS	U	U	A	A	L	
V	V	I	SS	U	U	AAAAA	L		
V	V	I	SS	U	U	A	A	L	
VV		I	SSSSS	UUUUU	A	A	LLLLL		

000	TTTTT	TTTTT	H	H	Y	Y	M	M	000	TM	
0	0	T	T	H	H	Y	Y	MM	MM	0	0
0	0	T	T	H	H	Y		M	M	0	0
000	T	T	H	H	Y		M	M	000		

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\vo in.dat

Output filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\0
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Summary filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\0
 d634577-eb90-4aa0-bdb9-11806d26dce1\

DATE: 11/15/2021

TIME: 04:33:25

USER:

COMMENTS: _____

** SIMULATION : 2-year **

| CHICAGO STORM |
Ptotal = 44.94 mm

IDF curve parameters: A=1290.000
B= 8.500
C= 0.860
used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	'	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.05	1.08	12.57		2.08	7.21	3.08	2.90
0.17	2.20	1.17	20.86		2.17	6.42	3.17	2.77
0.25	2.38	1.25	50.59		2.25	5.78	3.25	2.64
0.33	2.58	1.33	137.56		2.33	5.26	3.33	2.53
0.42	2.83	1.42	65.09		2.42	4.82	3.42	2.43
0.50	3.13	1.50	36.14		2.50	4.45	3.50	2.33
0.58	3.51	1.58	24.07		2.58	4.14	3.58	2.25
0.67	3.99	1.67	17.71		2.67	3.86	3.67	2.17
0.75	4.63	1.75	13.86		2.75	3.62	3.75	2.09
0.83	5.51	1.83	11.32		2.83	3.41	3.83	2.02
0.92	6.81	1.92	9.54		2.92	3.22	3.92	1.96
1.00	8.86	2.00	8.22		3.00	3.05	4.00	1.89

| CALIB |
| NASHYD (0001) |
ID= 1 DT= 5.0 min

Area (ha)= 9.60 Curve Number (CN)= 83.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.69

Unit Hyd Qpeak (cms)= 0.531

PEAK FLOW (cms)= 0.247 (i)
TIME TO PEAK (hrs)= 2.167
RUNOFF VOLUME (mm)= 17.346
TOTAL RAINFALL (mm)= 44.941
RUNOFF COEFFICIENT = 0.386

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
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V   V   I   SSSSS U   U   A   L           (v 6. 2. 2006)
V   V   I   SS   U   U   A A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
W   I   SSSSS UUUUU A   A   LLLLL
```

```
000  TTTTT  TTTTT  H   H   Y   Y   M   M   000  TM
0   0   T   T   H   H   Y   Y   MM  MM  0   0
0   0   T   T   H   H   Y   M   M   0   0
000  T   T   H   H   Y   M   M   000
```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6. 2\V02\voir.n.dat

Output filename:

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Summary filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\d9361e4-2d5a-44d1-b636-1968ca914566\

DATE: 11/15/2021

TIME: 04: 33: 25

USER:

COMMENTS: _____

```
-----
*****
** SIMULATION : 50-year Storm **
*****
```

| CHICAGO STORM | IDF curve parameters: A=2270.665

| Ptotal = 72.05 mm |

B= 9.984

C= 0.876

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	3.10	1.08	20.80	2.08	11.67	3.08	4.47
0.17	3.34	1.17	34.86	2.17	10.33	3.17	4.25
0.25	3.62	1.25	83.24	2.25	9.26	3.25	4.05
0.33	3.95	1.33	211.98	2.33	8.38	3.33	3.87
0.42	4.35	1.42	106.30	2.42	7.64	3.42	3.70
0.50	4.85	1.50	60.28	2.50	7.03	3.50	3.55
0.58	5.47	1.58	40.27	2.58	6.50	3.58	3.41
0.67	6.26	1.67	29.53	2.67	6.04	3.67	3.28
0.75	7.32	1.75	22.99	2.75	5.65	3.75	3.16
0.83	8.80	1.83	18.66	2.83	5.30	3.83	3.05
0.92	10.98	1.92	15.62	2.92	4.99	3.92	2.95
1.00	14.48	2.00	13.38	3.00	4.72	4.00	2.85

| CALIB
| NASHYD (0001)
| ID= 1 DT= 5.0 min |

Area (ha)= 9.60 Curve Number (CN)= 83.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.69

Unit Hyd Qpeak (cms)= 0.531

PEAK FLOW (cms)= 0.561 (i)

TIME TO PEAK (hrs)= 2.167

RUNOFF VOLUME (mm)= 37.752

TOTAL RAINFALL (mm)= 72.046

RUNOFF COEFFICIENT = 0.524

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

FINISH

V V I SSSSS U U A L

(v 6.2.2006)


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V   V   I   SS   U   U   A A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
  VV   I   SSSSS UUUUU A   A   LLLLL

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000   TTTTT TTTTT H   H   Y   Y   M   M   000   TM
0   0   T       T   H   H   Y Y   MM MM 0   0
0   0   T       T   H   H   Y   M   M   0   0
000   T       T   H   H   Y   M   M   000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\voir.n.dat

Output filename:

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 bb403bc-05bf-4e2d-8f62-3963bc29c549\

Summary filename:

C:\Users\dsredojev\c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
 bb403bc-05bf-4e2d-8f62-3963bc29c549\

DATE: 11/15/2021

TIME: 04: 33: 25

USER:

COMMENTS: _____

```

*****
** SIMULATION : 5-year Storm **
*****

```

```

-----
| CHICAGO STORM |
| Ptotal = 46.69 mm |
-----

```

IDF curve parameters: A=1183.740
 B= 7.641
 C= 0.838

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.36	1.08	13.04	2.08	7.70	3.08	3.27
0.17	2.52	1.17	21.19	2.17	6.90	3.17	3.12
0.25	2.71	1.25	50.66	2.25	6.25	3.25	2.99
0.33	2.93	1.33	141.24	2.33	5.72	3.33	2.87
0.42	3.19	1.42	65.17	2.42	5.27	3.42	2.76
0.50	3.51	1.50	36.21	2.50	4.89	3.50	2.66
0.58	3.91	1.58	24.34	2.58	4.56	3.58	2.56
0.67	4.41	1.67	18.09	2.67	4.27	3.67	2.48
0.75	5.07	1.75	14.31	2.75	4.02	3.75	2.40
0.83	5.98	1.83	11.80	2.83	3.80	3.83	2.32
0.92	7.29	1.92	10.03	2.92	3.60	3.92	2.25
1.00	9.36	2.00	8.71	3.00	3.43	4.00	2.18

CALIB			
NASHYD (0001)	Area (ha)=	9.60	Curve Number (CN)= 83.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res. (N)= 3.00
	U. H. Tp(hrs)=	0.69	

Unit Hyd Qpeak (cms)= 0.531

PEAK FLOW (cms)= 0.259 (i)

TIME TO PEAK (hrs)= 2.250

RUNOFF VOLUME (mm)= 18.549

TOTAL RAINFALL (mm)= 46.694

RUNOFF COEFFICIENT = 0.397

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

=====

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V   V   I   SSSSS U   U   A   L           (v 6. 2. 2006)
V   V   I   SS    U   U   A A   L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A   L
VV      I   SSSSS UUUUU A   A   LLLLL

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000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM
0   0   T     T     H   H   Y Y   MM MM   0   0
0   0   T     T     H   H   Y   M   M   0   0
000     T     T     H   H   Y   M   M   000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\voir.n.dat

Output filename:

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 a32d773-f0e7-41d2-8281-1cd184b1116f\

Summary filename:

C:\Users\dsredojev\c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\6
 a32d773-f0e7-41d2-8281-1cd184b1116f\

DATE: 11/15/2021

TIME: 04: 34: 44

USER:

COMMENTS: Catchment Drains to Rath Harris Municipal Drain

```

*****
** SIMULATION : 100-year Storm **
*****

```

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-----
| CHI CAGO STORM |
| Ptotal = 79.37 mm |
-----

```

IDF curve parameters: A=2619.363

B= 10.500

C= 0.884

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	3.30	1.08	23.09	2.08	12.82	3.08	4.80
0.17	3.56	1.17	38.91	2.17	11.32	3.17	4.56
0.25	3.86	1.25	92.77	2.25	10.11	3.25	4.34
0.33	4.23	1.33	232.24	2.33	9.13	3.33	4.14
0.42	4.67	1.42	118.26	2.42	8.32	3.42	3.95
0.50	5.21	1.50	67.39	2.50	7.63	3.50	3.79
0.58	5.89	1.58	45.00	2.58	7.04	3.58	3.63
0.67	6.78	1.67	32.92	2.67	6.54	3.67	3.49
0.75	7.96	1.75	25.56	2.75	6.10	3.75	3.36
0.83	9.61	1.83	20.68	2.83	5.71	3.83	3.24
0.92	12.05	1.92	17.26	2.92	5.37	3.92	3.13
1.00	15.97	2.00	14.74	3.00	5.07	4.00	3.02

```

-----
| CALIB |
| NASHYD ( 0001) | Area (ha)= 12.57 Curve Number (CN)= 83.0
| ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
-----
| U. H. Tp(hrs)= 0.70 |

```

Unit Hyd Qpeak (cms)= 0.686

PEAK FLOW (cms)= 0.852 (i)
TIME TO PEAK (hrs)= 2.167
RUNOFF VOLUME (mm)= 43.762
TOTAL RAINFALL (mm)= 79.374
RUNOFF COEFFICIENT = 0.551

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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=====
=====
V V I SSSSS U U A L (v 6.2.2006)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0

```

000 T T H H Y M M 000
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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\voir n.dat

Output filename:
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 Summary filename:
 C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\3
 c55f286-a31c-40a0-8d3e-3c872bd0c6b9\

DATE: 11/15/2021

TIME: 04:34:44

USER:

COMMENTS: _____

 ** SIMULATION : 10-year Storm **

 | CHI CAGO STORM |
Ptotal = 54.75 mm

IDF curve parameters: A=1574.382
 B= 9.025
 C= 0.860

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	2.53	1.08	15.60	2.08	8.95	3.08	3.58
0.17	2.71	1.17	25.83	2.17	7.96	3.17	3.41
0.25	2.93	1.25	61.71	2.25	7.17	3.25	3.26
0.33	3.19	1.33	162.47	2.33	6.51	3.33	3.12
0.42	3.49	1.42	79.04	2.42	5.97	3.42	2.99

0.50	3.87		1.50	44.47		2.50	5.51		3.50	2.88
0.58	4.34		1.58	29.77		2.58	5.12		3.58	2.77
0.67	4.94		1.67	21.95		2.67	4.77		3.67	2.67
0.75	5.73		1.75	17.20		2.75	4.47		3.75	2.57
0.83	6.83		1.83	14.05		2.83	4.21		3.83	2.49
0.92	8.44		1.92	11.83		2.92	3.98		3.92	2.41
1.00	11.00		2.00	10.20		3.00	3.77		4.00	2.33

```

-----
| CALIB |
| NASHYD ( 0001) |
| ID= 1 DT= 5.0 min |
-----
Area (ha)= 12.57 Curve Number (CN)= 83.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.70

```

Unit Hyd Qpeak (cms)= 0.686

PEAK FLOW (cms)= 0.454 (i)
 TIME TO PEAK (hrs)= 2.167
 RUNOFF VOLUME (mm)= 24.317
 TOTAL RAINFALL (mm)= 54.748
 RUNOFF COEFFICIENT = 0.444

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
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=====
V V I SSSSS U U A L (v 6.2.2006)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

```

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000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0
000 T T H H Y M M 000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\vo1n.dat

Output filename:

C: \Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
144cf04-12f5-49d8-acff-9bf35c710077\

Summary filename:

C: \Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
144cf04-12f5-49d8-acff-9bf35c710077\

DATE: 11/15/2021

TIME: 04: 34: 45

USER:

COMMENTS: _____

** SIMULATION : 25-year Storm **

| CHICAGO STORM | IDF curve parameters: A=2019.372
| Ptotal = 64.46 mm | B= 9.824
C= 0.875

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	'	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.78	1.08	18.53	'	2.08	10.41	3.08	4.00
0.17	2.99	1.17	31.05	'	2.17	9.22	3.17	3.81
0.25	3.24	1.25	74.37	'	2.25	8.27	3.25	3.63
0.33	3.54	1.33	190.82	'	2.33	7.48	3.33	3.47
0.42	3.90	1.42	95.08	'	2.42	6.83	3.42	3.32
0.50	4.34	1.50	53.76	'	2.50	6.28	3.50	3.18
0.58	4.89	1.58	35.88	'	2.58	5.81	3.58	3.06
0.67	5.60	1.67	26.31	'	2.67	5.41	3.67	2.94
0.75	6.54	1.75	20.49	'	2.75	5.05	3.75	2.83
0.83	7.86	1.83	16.63	'	2.83	4.74	3.83	2.74
0.92	9.80	1.92	13.93	'	2.92	4.47	3.92	2.64
1.00	12.91	2.00	11.93	'	3.00	4.22	4.00	2.56

| CALIB |

NASHYD (0001)	Area (ha)= 12.57	Curve Number (CN)= 83.0
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res. (N)= 3.00
-----	U. H. Tp(hrs)= 0.70	

Unit Hyd Qpeak (cms)= 0.686

PEAK FLOW (cms)= 0.607 (i)
 TIME TO PEAK (hrs)= 2.167
 RUNOFF VOLUME (mm)= 31.715
 TOTAL RAINFALL (mm)= 64.464
 RUNOFF COEFFICIENT = 0.492

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 =====
 =====

V	V	I	SSSSS	U	U	A	L	(v 6.2.2006)
V	V	I	SS	U	U	A	A	L
V	V	I	SS	U	U	AAAAA	L	
V	V	I	SS	U	U	A	A	L
VV		I	SSSSS	UUUUU	A	A	LLLLL	

000	TTTTT	TTTTT	H	H	Y	Y	M	M	000	TM	
0	0	T	T	H	H	Y	Y	MM	MM	0	0
0	0	T	T	H	H	Y		M	M	0	0
000	T	T	H	H	Y		M	M	000		

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\vo in.dat

Output filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
 e041554-c368-4169-9e63-a59621c3e529\

Summary filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
 e041554-c368-4169-9e63-a59621c3e529\

DATE: 11/15/2021

TIME: 04:34:45

USER:

COMMENTS: _____

** SIMULATION : 2-year **

| CHICAGO STORM |
Ptotal = 44.94 mm

IDF curve parameters: A=1290.000
B= 8.500
C= 0.860
used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	2.05	1.08	12.57	2.08	7.21	3.08	2.90
0.17	2.20	1.17	20.86	2.17	6.42	3.17	2.77
0.25	2.38	1.25	50.59	2.25	5.78	3.25	2.64
0.33	2.58	1.33	137.56	2.33	5.26	3.33	2.53
0.42	2.83	1.42	65.09	2.42	4.82	3.42	2.43
0.50	3.13	1.50	36.14	2.50	4.45	3.50	2.33
0.58	3.51	1.58	24.07	2.58	4.14	3.58	2.25
0.67	3.99	1.67	17.71	2.67	3.86	3.67	2.17
0.75	4.63	1.75	13.86	2.75	3.62	3.75	2.09
0.83	5.51	1.83	11.32	2.83	3.41	3.83	2.02
0.92	6.81	1.92	9.54	2.92	3.22	3.92	1.96
1.00	8.86	2.00	8.22	3.00	3.05	4.00	1.89

| CALIB |
| NASHYD (0001) |
ID= 1 DT= 5.0 min

Area (ha)= 12.57 Curve Number (CN)= 83.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.70

Unit Hyd Qpeak (cms)= 0.686

PEAK FLOW (cms)= 0.321 (i)
TIME TO PEAK (hrs)= 2.250
RUNOFF VOLUME (mm)= 17.346
TOTAL RAINFALL (mm)= 44.941
RUNOFF COEFFICIENT = 0.386

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

FINISH
=====

=====

V	V	I	SSSSS	U	U	A	L		(v 6. 2. 2006)
V	V	I	SS	U	U	A	A	L	
V	V	I	SS	U	U	AAAAA	L		
V	V	I	SS	U	U	A	A	L	
VV		I	SSSSS	UUUUU	A	A	LLLLL		

000	TTTT	TTTT	H	H	Y	Y	M	M	000	TM	
0	0	T	T	H	H	Y	Y	MM	MM	0	0
0	0	T	T	H	H	Y		M	M	0	0
000	T	T	H	H	Y		M	M	000		

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Vi sua l OTTHYM0 6. 2\V02\voi n. dat

Output filename:

C:\Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\9
8ebb25a-b2dd-408b-b2d9-9a993c03e5b8\

Summary filename:

C:\Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\9
8ebb25a-b2dd-408b-b2d9-9a993c03e5b8\

DATE: 11/15/2021

TIME: 04: 34: 45

USER:

COMMENTS: _____

** SIMULATION : 50-year Storm **

 | CHICAGO STORM |
Ptotal = 72.05 mm

IDF curve parameters: A=2270.665
 B= 9.984
 C= 0.876
 used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	3.10	1.08	20.80	2.08	11.67	3.08	4.47
0.17	3.34	1.17	34.86	2.17	10.33	3.17	4.25
0.25	3.62	1.25	83.24	2.25	9.26	3.25	4.05
0.33	3.95	1.33	211.98	2.33	8.38	3.33	3.87
0.42	4.35	1.42	106.30	2.42	7.64	3.42	3.70
0.50	4.85	1.50	60.28	2.50	7.03	3.50	3.55
0.58	5.47	1.58	40.27	2.58	6.50	3.58	3.41
0.67	6.26	1.67	29.53	2.67	6.04	3.67	3.28
0.75	7.32	1.75	22.99	2.75	5.65	3.75	3.16
0.83	8.80	1.83	18.66	2.83	5.30	3.83	3.05
0.92	10.98	1.92	15.62	2.92	4.99	3.92	2.95
1.00	14.48	2.00	13.38	3.00	4.72	4.00	2.85

 | CALIB |
 | NASHYD (0001) |
ID= 1 DT= 5.0 min

Area (ha)= 12.57 Curve Number (CN)= 83.0
 Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
 U. H. Tp(hrs)= 0.70

Unit Hyd Qpeak (cms)= 0.686

PEAK FLOW (cms)= 0.727 (i)
 TIME TO PEAK (hrs)= 2.167
 RUNOFF VOLUME (mm)= 37.752
 TOTAL RAINFALL (mm)= 72.046
 RUNOFF COEFFICIENT = 0.524

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

V   V   I   SS   U   U   A A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
  VV   I   SSSSS UUUUU A   A   LLLLL

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000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM
0   0   T       T   H   H   Y Y   MM MM   0   0
0   0   T       T   H   H   Y   M   M   0   0
000   T       T   H   H   Y   M   M   000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\vo1n.dat

Output filename:

C:\Users\dsredojev\c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\1
 b577058-7d3f-49c1-87b7-1dcb0c25077\

Summary filename:

C:\Users\dsredojev\c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\1
 b577058-7d3f-49c1-87b7-1dcb0c25077\

DATE: 11/15/2021

TIME: 04: 34: 44

USER:

COMMENTS: _____

```

*****
** SIMULATION : 5-year Storm **
*****

```

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-----
| CHICAGO STORM |
| Ptotal = 46.69 mm |
-----

```

IDF curve parameters: A=1183.740
 B= 7.641
 C= 0.838

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.36	1.08	13.04	2.08	7.70	3.08	3.27
0.17	2.52	1.17	21.19	2.17	6.90	3.17	3.12
0.25	2.71	1.25	50.66	2.25	6.25	3.25	2.99
0.33	2.93	1.33	141.24	2.33	5.72	3.33	2.87
0.42	3.19	1.42	65.17	2.42	5.27	3.42	2.76
0.50	3.51	1.50	36.21	2.50	4.89	3.50	2.66
0.58	3.91	1.58	24.34	2.58	4.56	3.58	2.56
0.67	4.41	1.67	18.09	2.67	4.27	3.67	2.48
0.75	5.07	1.75	14.31	2.75	4.02	3.75	2.40
0.83	5.98	1.83	11.80	2.83	3.80	3.83	2.32
0.92	7.29	1.92	10.03	2.92	3.60	3.92	2.25
1.00	9.36	2.00	8.71	3.00	3.43	4.00	2.18

CALIB			
NASHYD (0001)	Area (ha)= 12.57	Curve Number (CN)= 83.0	
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res. (N)= 3.00	
	U. H. Tp(hrs)= 0.70		

Unit Hyd Qpeak (cms)= 0.686

PEAK FLOW (cms)= 0.336 (i)

TIME TO PEAK (hrs)= 2.250

RUNOFF VOLUME (mm)= 18.549

TOTAL RAINFALL (mm)= 46.694

RUNOFF COEFFICIENT = 0.397

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Appendix E

Post-Development Conditions Hydrologic Modelling Output

=====

```

V   V   I   SSSSS U   U   A   L           (v 6. 2. 2006)
V   V   I   SS    U   U   A A   L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A   L
VV      I   SSSSS UUUUU A   A   LLLLL

```

```

000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM
0   0   T     T     H   H   Y Y   MM MM   0   0
0   0   T     T     H   H   Y   M   M   0   0
000     T     T     H   H   Y   M   M   000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\vo1n.dat

Output filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\01aa7571-04a3-4e5b-b591-c4765341a3ee\

Summary filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\01aa7571-04a3-4e5b-b591-c4765341a3ee\

DATE: 11/18/2021

TIME: 10: 54: 39

USER:

COMMENTS: _____

```

*****
** SIMULATION : 100-year Storm **
*****

```

```

-----
| CHI CAGO STORM |
| Ptotal = 79.37 mm |
-----

```

IDF curve parameters: A=2619.363
 B= 10.500
 C= 0.884

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	3.30	1.08	23.09	2.08	12.82	3.08	4.80
0.17	3.56	1.17	38.91	2.17	11.32	3.17	4.56
0.25	3.86	1.25	92.77	2.25	10.11	3.25	4.34
0.33	4.23	1.33	232.24	2.33	9.13	3.33	4.14
0.42	4.67	1.42	118.26	2.42	8.32	3.42	3.95
0.50	5.21	1.50	67.39	2.50	7.63	3.50	3.79
0.58	5.89	1.58	45.00	2.58	7.04	3.58	3.63
0.67	6.78	1.67	32.92	2.67	6.54	3.67	3.49
0.75	7.96	1.75	25.56	2.75	6.10	3.75	3.36
0.83	9.61	1.83	20.68	2.83	5.71	3.83	3.24
0.92	12.05	1.92	17.26	2.92	5.37	3.92	3.13
1.00	15.97	2.00	14.74	3.00	5.07	4.00	3.02

CALIB			
NASHYD (0002)	Area (ha)=	1.50	Curve Number (CN)= 88.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res. (N)= 3.00
	U. H. Tp(hrs)=	0.12	

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.371 (i)
TIME TO PEAK (hrs)= 1.417
RUNOFF VOLUME (mm)= 50.065
TOTAL RAINFALL (mm)= 79.374
RUNOFF COEFFICIENT = 0.631

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0001)	Area (ha)=	20.71	
ID= 1 DT= 3.0 min	Total Imp(%)=	85.00	Dir. Conn. (%)= 75.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	17.60	3.11
Dep. Storage (mm)=	2.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	371.57	40.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.050	3.30	1.050	23.09	2.050	12.82	3.05	4.80
0.100	3.38	1.100	28.36	2.100	12.32	3.10	4.72
0.150	3.56	1.150	38.91	2.150	11.32	3.15	4.56
0.200	3.76	1.200	74.81	2.200	10.52	3.20	4.41
0.250	3.86	1.250	92.77	2.250	10.11	3.25	4.34
0.300	4.23	1.300	232.24	2.300	9.13	3.30	4.14
0.350	4.38	1.350	194.25	2.350	8.86	3.35	4.07
0.400	4.67	1.400	118.26	2.400	8.32	3.40	3.95
0.450	5.03	1.450	84.35	2.450	7.86	3.45	3.84
0.500	5.21	1.500	67.39	2.500	7.63	3.50	3.79
0.550	5.89	1.550	45.00	2.550	7.04	3.55	3.63
0.600	6.19	1.600	40.98	2.600	6.87	3.60	3.59
0.650	6.78	1.650	32.92	2.650	6.54	3.65	3.49
0.700	7.56	1.700	28.01	2.700	6.24	3.70	3.40
0.750	7.96	1.750	25.56	2.750	6.10	3.75	3.36
0.800	9.61	1.800	20.68	2.800	5.71	3.80	3.24
0.850	10.42	1.850	19.54	2.850	5.60	3.85	3.20
0.900	12.05	1.900	17.26	2.900	5.37	3.90	3.13
0.950	14.66	1.950	15.58	2.950	5.17	3.95	3.06
1.000	15.97	2.000	14.74	3.000	5.07	4.00	3.02

Max. Eff. Inten. (mm/hr)=	213.25	*****	
over (min)	6.00	9.00	
Storage Coeff. (min)=	4.15 (ii)	6.89 (ii)	
Unit Hyd. Tpeak (min)=	6.00	9.00	
Unit Hyd. peak (cms)=	0.23	0.15	
			TOTALS
PEAK FLOW (cms)=	7.06	1.10	8.038 (iii)
TIME TO PEAK (hrs)=	1.40	1.45	1.40
RUNOFF VOLUME (mm)=	77.37	44.90	69.25
TOTAL RAINFALL (mm)=	79.37	79.37	79.37
RUNOFF COEFFICIENT =	0.97	0.57	0.87

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
CN* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0006)	AREA	QPEAK	TPEAK	R. V.
1 + 2 = 3				

	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0001):	20.71	8.038	1.40	69.25
+ ID2= 2 (0002):	1.50	0.371	1.42	50.07
=====				
ID = 3 (0006):	22.21	8.390	1.40	67.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR(0004)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha. m.)	(cms)	(ha. m.)
	0.0000	0.0000	0.6190	1.0474
	0.0480	0.2326	0.6740	1.1492
	0.0780	0.4844	0.8160	1.4686
	0.4080	0.7558	0.8580	1.5800

	AREA	QPEAK	TPEAK	R. V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0006)	22.210	8.390	1.40	67.95
OUTFLOW: ID= 1 (0004)	22.210	0.656	2.25	67.90

PEAK FLOW REDUCTION [Qout/Qin] (%)= 7.82
 TIME SHIFT OF PEAK FLOW (min)= 51.00
 MAXIMUM STORAGE USED (ha. m.)= 1.1166

```

V   V   I   SSSSS U   U   A   L           (v 6.2.2006)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
  VV    I   SSSSS UUUUU A   A  LLLLL

```

```

000  TTTT  TTTT  H   H   Y   Y   M   M   000  TM
0 0  T    T    H   H   Y Y  MM MM 0 0
0 0  T    T    H   H   Y   M   M 0 0
000  T    T    H   H   Y   M   M 000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\voir.n.dat

Output filename:
C: \Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\196b6fc-a518-4982-a948-7646f04b0aa7\
Summary filename:
C: \Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\196b6fc-a518-4982-a948-7646f04b0aa7\

DATE: 11/18/2021 TIME: 10: 54: 40

USER:

COMMENTS: _____

** SIMULATION : 100-year-24 hours **

| CHICAGO STORM |
Ptotal=100.84 mm

IDF curve parameters: A=2619.363
B= 10.500
C= 0.884

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 24.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	'	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	'	hrs	mm/hr	hrs	mm/hr
0.08	0.52	6.08	2.08		12.08	1.93	18.08	0.79
0.17	0.52	6.17	2.18		12.17	1.89	18.17	0.79
0.25	0.53	6.25	2.29		12.25	1.86	18.25	0.78
0.33	0.54	6.33	2.41		12.33	1.82	18.33	0.78
0.42	0.54	6.42	2.55		12.42	1.78	18.42	0.77
0.50	0.55	6.50	2.70		12.50	1.75	18.50	0.76
0.58	0.55	6.58	2.87		12.58	1.72	18.58	0.76
0.67	0.56	6.67	3.07		12.67	1.69	18.67	0.75
0.75	0.56	6.75	3.30		12.75	1.66	18.75	0.75
0.83	0.57	6.83	3.56		12.83	1.63	18.83	0.74
0.92	0.58	6.92	3.86		12.92	1.60	18.92	0.74
1.00	0.58	7.00	4.23		13.00	1.57	19.00	0.73
1.08	0.59	7.08	4.67		13.08	1.55	19.08	0.73
1.17	0.60	7.17	5.21		13.17	1.52	19.17	0.72
1.25	0.60	7.25	5.89		13.25	1.50	19.25	0.72
1.33	0.61	7.33	6.78		13.33	1.48	19.33	0.71

1.42	0.62	7.42	7.96	13.42	1.45	19.42	0.71
1.50	0.63	7.50	9.61	13.50	1.43	19.50	0.70
1.58	0.63	7.58	12.05	13.58	1.41	19.58	0.70
1.67	0.64	7.67	15.97	13.67	1.39	19.67	0.69
1.75	0.65	7.75	23.09	13.75	1.37	19.75	0.69
1.83	0.66	7.83	38.91	13.83	1.35	19.83	0.68
1.92	0.67	7.92	92.77	13.92	1.33	19.92	0.68
2.00	0.67	8.00	232.24	14.00	1.31	20.00	0.67
2.08	0.68	8.08	118.26	14.08	1.29	20.08	0.67
2.17	0.69	8.17	67.39	14.17	1.28	20.17	0.66
2.25	0.70	8.25	45.00	14.25	1.26	20.25	0.66
2.33	0.71	8.33	32.92	14.33	1.24	20.33	0.66
2.42	0.72	8.42	25.56	14.42	1.23	20.42	0.65
2.50	0.73	8.50	20.68	14.50	1.21	20.50	0.65
2.58	0.74	8.58	17.26	14.58	1.20	20.58	0.64
2.67	0.75	8.67	14.74	14.67	1.18	20.67	0.64
2.75	0.77	8.75	12.82	14.75	1.17	20.75	0.64
2.83	0.78	8.83	11.32	14.83	1.15	20.83	0.63
2.92	0.79	8.92	10.11	14.92	1.14	20.92	0.63
3.00	0.80	9.00	9.13	15.00	1.13	21.00	0.62
3.08	0.81	9.08	8.32	15.08	1.11	21.08	0.62
3.17	0.83	9.17	7.63	15.17	1.10	21.17	0.62
3.25	0.84	9.25	7.04	15.25	1.09	21.25	0.61
3.33	0.86	9.33	6.54	15.33	1.08	21.33	0.61
3.42	0.87	9.42	6.10	15.42	1.07	21.42	0.61
3.50	0.89	9.50	5.71	15.50	1.05	21.50	0.60
3.58	0.90	9.58	5.37	15.58	1.04	21.58	0.60
3.67	0.92	9.67	5.07	15.67	1.03	21.67	0.60
3.75	0.94	9.75	4.80	15.75	1.02	21.75	0.59
3.83	0.96	9.83	4.56	15.83	1.01	21.83	0.59
3.92	0.97	9.92	4.34	15.92	1.00	21.92	0.59
4.00	0.99	10.00	4.14	16.00	0.99	22.00	0.58
4.08	1.01	10.08	3.95	16.08	0.98	22.08	0.58
4.17	1.04	10.17	3.79	16.17	0.97	22.17	0.58
4.25	1.06	10.25	3.63	16.25	0.96	22.25	0.57
4.33	1.08	10.33	3.49	16.33	0.95	22.33	0.57
4.42	1.11	10.42	3.36	16.42	0.94	22.42	0.57
4.50	1.13	10.50	3.24	16.50	0.93	22.50	0.56
4.58	1.16	10.58	3.13	16.58	0.93	22.58	0.56
4.67	1.19	10.67	3.02	16.67	0.92	22.67	0.56
4.75	1.22	10.75	2.92	16.75	0.91	22.75	0.55
4.83	1.25	10.83	2.83	16.83	0.90	22.83	0.55
4.92	1.28	10.92	2.75	16.92	0.89	22.92	0.55
5.00	1.32	11.00	2.67	17.00	0.88	23.00	0.55
5.08	1.36	11.08	2.59	17.08	0.88	23.08	0.54
5.17	1.40	11.17	2.52	17.17	0.87	23.17	0.54
5.25	1.44	11.25	2.45	17.25	0.86	23.25	0.54
5.33	1.48	11.33	2.39	17.33	0.85	23.33	0.53
5.42	1.53	11.42	2.32	17.42	0.85	23.42	0.53
5.50	1.58	11.50	2.27	17.50	0.84	23.50	0.53
5.58	1.64	11.58	2.21	17.58	0.83	23.58	0.53

5.67	1.70	11.67	2.16	17.67	0.83	23.67	0.52
5.75	1.76	11.75	2.11	17.75	0.82	23.75	0.52
5.83	1.83	11.83	2.06	17.83	0.81	23.83	0.52
5.92	1.91	11.92	2.02	17.92	0.81	23.92	0.52
6.00	1.99	12.00	1.97	18.00	0.80	24.00	0.51

 | CALIB |
 | NASHYD (0002) | Area (ha)= 1.50 Curve Number (CN)= 88.0
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res. (N)= 3.00

 U. H. Tp(hrs)= 0.12

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.416 (i)
 TIME TO PEAK (hrs)= 8.083
 RUNOFF VOLUME (mm)= 69.456
 TOTAL RAINFALL (mm)= 100.838
 RUNOFF COEFFICIENT = 0.689

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | STANDHYD (0001) | Area (ha)= 20.71
 | ID= 1 DT= 3.0 min | Total Imp(%)= 85.00 Di r. Conn. (%)= 75.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	17.60	3.11
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.00	2.00
Length	(m)=	371.57	40.00
Mannings n	=	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.050	0.52	6.050	2.08	12.050	1.93	18.05	0.79
0.100	0.52	6.100	2.12	12.100	1.92	18.10	0.79
0.150	0.52	6.150	2.18	12.150	1.89	18.15	0.79
0.200	0.53	6.200	2.26	12.200	1.87	18.20	0.78
0.250	0.53	6.250	2.29	12.250	1.86	18.25	0.78
0.300	0.54	6.300	2.41	12.300	1.82	18.30	0.78
0.350	0.54	6.350	2.46	12.350	1.81	18.35	0.77
0.400	0.54	6.400	2.55	12.400	1.78	18.40	0.77

0.450	0.54	6.450	2.65	12.450	1.76	18.45	0.77
0.500	0.55	6.500	2.70	12.500	1.75	18.50	0.76
0.550	0.55	6.550	2.87	12.550	1.72	18.55	0.76
0.600	0.55	6.600	2.94	12.600	1.71	18.60	0.76
0.650	0.56	6.650	3.07	12.650	1.69	18.65	0.75
0.700	0.56	6.700	3.22	12.700	1.67	18.70	0.75
0.750	0.56	6.750	3.30	12.750	1.66	18.75	0.75
0.800	0.57	6.800	3.56	12.800	1.63	18.80	0.74
0.850	0.57	6.850	3.66	12.850	1.62	18.85	0.74
0.900	0.58	6.900	3.86	12.900	1.60	18.90	0.74
0.950	0.58	6.950	4.11	12.950	1.58	18.95	0.73
1.000	0.58	7.000	4.23	13.000	1.57	19.00	0.73
1.050	0.59	7.050	4.67	13.050	1.55	19.05	0.73
1.100	0.59	7.100	4.85	13.100	1.54	19.10	0.72
1.150	0.60	7.150	5.21	13.150	1.52	19.15	0.72
1.200	0.60	7.200	5.67	13.200	1.51	19.20	0.72
1.250	0.60	7.250	5.89	13.250	1.50	19.25	0.72
1.300	0.61	7.300	6.78	13.300	1.48	19.30	0.71
1.350	0.61	7.350	7.17	13.350	1.47	19.35	0.71
1.400	0.62	7.400	7.96	13.400	1.45	19.40	0.71
1.450	0.62	7.450	9.06	13.450	1.44	19.45	0.70
1.500	0.63	7.500	9.61	13.500	1.43	19.50	0.70
1.550	0.63	7.550	12.05	13.550	1.41	19.55	0.70
1.600	0.64	7.600	13.36	13.600	1.40	19.60	0.69
1.650	0.64	7.650	15.97	13.650	1.39	19.65	0.69
1.700	0.65	7.700	20.72	13.700	1.38	19.70	0.69
1.750	0.65	7.750	23.09	13.750	1.37	19.75	0.69
1.800	0.66	7.800	38.91	13.800	1.35	19.80	0.68
1.850	0.66	7.850	56.87	13.850	1.34	19.85	0.68
1.900	0.67	7.900	92.77	13.900	1.33	19.90	0.68
1.950	0.67	7.950	185.78	13.950	1.32	19.95	0.67
2.000	0.67	8.000	232.22	14.000	1.31	20.00	0.67
2.050	0.68	8.050	118.26	14.050	1.29	20.05	0.67
2.100	0.69	8.100	101.29	14.100	1.29	20.10	0.67
2.150	0.69	8.150	67.39	14.150	1.28	20.15	0.66
2.200	0.70	8.200	52.46	14.200	1.27	20.20	0.66
2.250	0.70	8.250	45.00	14.250	1.26	20.25	0.66
2.300	0.71	8.300	32.92	14.300	1.24	20.30	0.66
2.350	0.71	8.350	30.47	14.350	1.24	20.35	0.65
2.400	0.72	8.400	25.56	14.400	1.23	20.40	0.65
2.450	0.73	8.450	22.31	14.450	1.22	20.45	0.65
2.500	0.73	8.500	20.68	14.500	1.21	20.50	0.65
2.550	0.74	8.550	17.26	14.550	1.20	20.55	0.64
2.600	0.75	8.600	16.42	14.600	1.19	20.60	0.64
2.650	0.75	8.650	14.74	14.650	1.18	20.65	0.64
2.700	0.76	8.700	13.46	14.700	1.17	20.70	0.64
2.750	0.77	8.750	12.82	14.750	1.17	20.75	0.64
2.800	0.78	8.800	11.32	14.800	1.15	20.80	0.63
2.850	0.78	8.850	10.92	14.850	1.15	20.85	0.63
2.900	0.79	8.900	10.11	14.900	1.14	20.90	0.63
2.950	0.80	8.950	9.46	14.950	1.13	20.95	0.63

3. 000	0. 80	9. 000	9. 13	15. 000	1. 13	21. 00	0. 62
3. 050	0. 81	9. 050	8. 32	15. 050	1. 11	21. 05	0. 62
3. 100	0. 82	9. 100	8. 09	15. 100	1. 11	21. 10	0. 62
3. 150	0. 83	9. 150	7. 63	15. 150	1. 10	21. 15	0. 62
3. 200	0. 84	9. 200	7. 24	15. 200	1. 09	21. 20	0. 61
3. 250	0. 84	9. 250	7. 04	15. 250	1. 09	21. 25	0. 61
3. 300	0. 86	9. 300	6. 54	15. 300	1. 08	21. 30	0. 61
3. 350	0. 86	9. 350	6. 39	15. 350	1. 07	21. 35	0. 61
3. 400	0. 87	9. 400	6. 10	15. 400	1. 07	21. 40	0. 61
3. 450	0. 88	9. 450	5. 84	15. 450	1. 06	21. 45	0. 60
3. 500	0. 89	9. 500	5. 71	15. 500	1. 05	21. 50	0. 60
3. 550	0. 90	9. 550	5. 37	15. 550	1. 04	21. 55	0. 60
3. 600	0. 91	9. 600	5. 27	15. 600	1. 04	21. 60	0. 60
3. 650	0. 92	9. 650	5. 07	15. 650	1. 03	21. 65	0. 60
3. 700	0. 93	9. 700	4. 89	15. 700	1. 02	21. 70	0. 59
3. 750	0. 94	9. 750	4. 80	15. 750	1. 02	21. 75	0. 59
3. 800	0. 96	9. 800	4. 56	15. 800	1. 01	21. 80	0. 59
3. 850	0. 96	9. 850	4. 48	15. 850	1. 01	21. 85	0. 59
3. 900	0. 97	9. 900	4. 34	15. 900	1. 00	21. 90	0. 59
3. 950	0. 99	9. 950	4. 20	15. 950	0. 99	21. 95	0. 58
4. 000	0. 99	10. 000	4. 14	16. 000	0. 99	22. 00	0. 58
4. 050	1. 01	10. 050	3. 95	16. 050	0. 98	22. 05	0. 58
4. 100	1. 02	10. 100	3. 90	16. 100	0. 98	22. 10	0. 58
4. 150	1. 04	10. 150	3. 79	16. 150	0. 97	22. 15	0. 58
4. 200	1. 05	10. 200	3. 68	16. 200	0. 96	22. 20	0. 57
4. 250	1. 06	10. 250	3. 63	16. 250	0. 96	22. 25	0. 57
4. 300	1. 08	10. 300	3. 49	16. 300	0. 95	22. 30	0. 57
4. 350	1. 09	10. 350	3. 45	16. 350	0. 95	22. 35	0. 57
4. 400	1. 11	10. 400	3. 36	16. 400	0. 94	22. 40	0. 57
4. 450	1. 12	10. 450	3. 28	16. 450	0. 94	22. 45	0. 56
4. 500	1. 13	10. 500	3. 24	16. 500	0. 93	22. 50	0. 56
4. 550	1. 16	10. 550	3. 13	16. 550	0. 93	22. 55	0. 56
4. 600	1. 17	10. 600	3. 09	16. 600	0. 92	22. 60	0. 56
4. 650	1. 19	10. 650	3. 02	16. 650	0. 92	22. 65	0. 56
4. 700	1. 21	10. 700	2. 96	16. 700	0. 91	22. 70	0. 56
4. 750	1. 22	10. 750	2. 92	16. 750	0. 91	22. 75	0. 55
4. 800	1. 25	10. 800	2. 83	16. 800	0. 90	22. 80	0. 55
4. 850	1. 26	10. 850	2. 80	16. 850	0. 90	22. 85	0. 55
4. 900	1. 28	10. 900	2. 75	16. 900	0. 89	22. 90	0. 55
4. 950	1. 31	10. 950	2. 69	16. 950	0. 89	22. 95	0. 55
5. 000	1. 32	11. 000	2. 67	17. 000	0. 88	23. 00	0. 55
5. 050	1. 36	11. 050	2. 59	17. 050	0. 88	23. 05	0. 54
5. 100	1. 37	11. 100	2. 57	17. 100	0. 87	23. 10	0. 54
5. 150	1. 40	11. 150	2. 52	17. 150	0. 87	23. 15	0. 54
5. 200	1. 43	11. 200	2. 47	17. 200	0. 86	23. 20	0. 54
5. 250	1. 44	11. 250	2. 45	17. 250	0. 86	23. 25	0. 54
5. 300	1. 48	11. 300	2. 39	17. 300	0. 85	23. 30	0. 53
5. 350	1. 50	11. 350	2. 37	17. 350	0. 85	23. 35	0. 53
5. 400	1. 53	11. 400	2. 32	17. 400	0. 85	23. 40	0. 53
5. 450	1. 57	11. 450	2. 29	17. 450	0. 84	23. 45	0. 53
5. 500	1. 58	11. 500	2. 27	17. 500	0. 84	23. 50	0. 53

5.550	1.64	11.550	2.21	17.550	0.83	23.55	0.53
5.600	1.66	11.600	2.19	17.600	0.83	23.60	0.53
5.650	1.70	11.650	2.16	17.650	0.83	23.65	0.52
5.700	1.74	11.700	2.13	17.700	0.82	23.70	0.52
5.750	1.76	11.750	2.11	17.750	0.82	23.75	0.52
5.800	1.83	11.800	2.06	17.800	0.81	23.80	0.52
5.850	1.86	11.850	2.05	17.850	0.81	23.85	0.52
5.900	1.91	11.900	2.02	17.900	0.81	23.90	0.52
5.950	1.97	11.950	1.99	17.950	0.80	23.95	0.51
6.000	1.99	12.000	1.97	18.000	0.80	24.00	0.51

Max. Eff. Inten. (mm/hr)=	209.00	*****	
over (min)	6.00	9.00	
Storage Coeff. (min)=	4.18 (ii)	6.94 (ii)	
Unit Hyd. Tpeak (min)=	6.00	9.00	
Unit Hyd. peak (cms)=	0.23	0.15	
			TOTALS
PEAK FLOW (cms)=	7.28	1.23	8.322 (iii)
TIME TO PEAK (hrs)=	8.05	8.10	8.05
RUNOFF VOLUME (mm)=	98.84	63.23	89.94
TOTAL RAINFALL (mm)=	100.84	100.84	100.84
RUNOFF COEFFICIENT =	0.98	0.63	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0006)				
1 + 2 = 3				
ID1= 1 (0001):	20.71	8.322	8.05	89.94
+ ID2= 2 (0002):	1.50	0.416	8.08	69.46
=====				
ID = 3 (0006):	22.21	8.702	8.05	88.56

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR(0004)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha. m.)	(cms)	(ha. m.)
	0.0000	0.0000	0.6190	1.0474
	0.0480	0.2326	0.6740	1.1492
	0.0780	0.4844	0.8160	1.4686

	0. 4080	0. 7558		0. 8580	1. 5800
	AREA	QPEAK		TPEAK	R. V.
	(ha)	(cms)		(hrs)	(mm)
INFLOW : ID= 2 (0006)	22. 210	8. 702		8. 05	88. 56
OUTFLOW: ID= 1 (0004)	22. 210	0. 709		8. 90	88. 49

PEAK FLOW REDUCTION [Qout/Qi n](%)= 8. 15
 TIME SHIFT OF PEAK FLOW (mi n)= 51. 00
 MAXIMUM STORAGE USED (ha. m.)= 1. 2290

FINISH

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V   V   I   SSSSS U   U   A   L           (v 6. 2. 2006)
V   V   I   SS    U   U   A A   L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A   L
WV    I   SSSSS UUUUU A   A   LLLLL
  
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000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM
0   0   T     T   H   H   Y   Y   MM  MM  0   0
0   0   T     T   H   H   Y     M   M   0   0
000   T     T   H   H   Y     M   M   000
  
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***** D E T A I L E D O U T P U T *****

Input fi le name: C: \Program Fi les (x86)\Vi sua l OTTHYM0 6. 2\V02\voi n. dat

Output fi le name:

C: \Users\dsredoj evi c\AppData\Local \Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\d
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Summary fi le name:

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1016303-091c-4cc3-92bc-b5c22df0a432\

DATE: 11/18/2021

TIME: 10: 54: 40

USER:

COMMENTS: _____

** SIMULATION : 10-year Storm **

| CHICAGO STORM |
Ptotal = 54.75 mm

IDF curve parameters: A=1574.382
B= 9.025
C= 0.860
used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	2.53	1.08	15.60	2.08	8.95	3.08	3.58
0.17	2.71	1.17	25.83	2.17	7.96	3.17	3.41
0.25	2.93	1.25	61.71	2.25	7.17	3.25	3.26
0.33	3.19	1.33	162.47	2.33	6.51	3.33	3.12
0.42	3.49	1.42	79.04	2.42	5.97	3.42	2.99
0.50	3.87	1.50	44.47	2.50	5.51	3.50	2.88
0.58	4.34	1.58	29.77	2.58	5.12	3.58	2.77
0.67	4.94	1.67	21.95	2.67	4.77	3.67	2.67
0.75	5.73	1.75	17.20	2.75	4.47	3.75	2.57
0.83	6.83	1.83	14.05	2.83	4.21	3.83	2.49
0.92	8.44	1.92	11.83	2.92	3.98	3.92	2.41
1.00	11.00	2.00	10.20	3.00	3.77	4.00	2.33

| CALIB |
| NASHYD (0002) |
ID= 1 DT= 5.0 min

Area (ha)= 1.50 Curve Number (CN)= 88.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.12

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.203 (i)
TIME TO PEAK (hrs)= 1.417
RUNOFF VOLUME (mm)= 28.937
TOTAL RAINFALL (mm)= 54.748

RUNOFF COEFFICIENT = 0.529

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD (0001)	Area (ha)= 20.71
ID= 1 DT= 3.0 min	Total Imp(%)= 85.00 Dir. Conn. (%)= 75.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	17.60	3.11
Dep. Storage (mm)=	2.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	371.57	40.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.050	2.53	1.050	15.60	2.050	8.95	3.05	3.58
0.100	2.59	1.100	19.01	2.100	8.62	3.10	3.53
0.150	2.71	1.150	25.83	2.150	7.96	3.15	3.41
0.200	2.86	1.200	49.75	2.200	7.43	3.20	3.31
0.250	2.93	1.250	61.71	2.250	7.17	3.25	3.26
0.300	3.19	1.300	162.47	2.300	6.51	3.30	3.12
0.350	3.29	1.350	134.66	2.350	6.33	3.35	3.08
0.400	3.49	1.400	79.04	2.400	5.97	3.40	2.99
0.450	3.74	1.450	55.99	2.450	5.66	3.45	2.91
0.500	3.87	1.500	44.47	2.500	5.51	3.50	2.88
0.550	4.34	1.550	29.77	2.550	5.12	3.55	2.77
0.600	4.54	1.600	27.16	2.600	5.00	3.60	2.73
0.650	4.94	1.650	21.95	2.650	4.77	3.65	2.67
0.700	5.47	1.700	18.78	2.700	4.57	3.70	2.61
0.750	5.73	1.750	17.20	2.750	4.47	3.75	2.57
0.800	6.83	1.800	14.05	2.800	4.21	3.80	2.49
0.850	7.37	1.850	13.31	2.850	4.13	3.85	2.46
0.900	8.44	1.900	11.83	2.900	3.98	3.90	2.41
0.950	10.15	1.950	10.74	2.950	3.84	3.95	2.36
1.000	11.00	2.000	10.20	3.000	3.77	4.00	2.33

Max. Eff. Inten. (mm/hr)=	148.56	*****
over (min)	6.00	9.00
Storage Coeff. (min)=	4.79 (i i)	7.96 (i i)
Unit Hyd. Tpeak (min)=	6.00	9.00
Unit Hyd. peak (cms)=	0.21	0.14

PEAK FLOW (cms)= 4.72 0.56 *TOTALS* 5.200 (i i i)

TIME TO PEAK	(hrs)=	1.40	1.45	1.40
RUNOFF VOLUME	(mm)=	52.75	25.43	45.92
TOTAL RAINFALL	(mm)=	54.75	54.75	54.75
RUNOFF COEFFICIENT	=	0.96	0.46	0.84

(i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:

CN* = 74.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0006) |
| 1 + 2 = 3 |
-----
      AREA      QPEAK      TPEAK      R. V.
      (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0001):  20.71  5.200  1.40  45.92
+ ID2= 2 ( 0002):  1.50  0.203  1.42  28.94
=====
ID = 3 ( 0006):  22.21  5.391  1.40  44.77

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR( 0004) |
| IN= 2---> OUT= 1 |
| DT= 5.0 mi n |
-----
      OVERFLOW IS OFF
      OUTFLOW      STORAGE      |      OUTFLOW      STORAGE
      (cms)      (ha. m. )      |      (cms)      (ha. m. )
      0.0000      0.0000      |      0.6190      1.0474
      0.0480      0.2326      |      0.6740      1.1492
      0.0780      0.4844      |      0.8160      1.4686
      0.4080      0.7558      |      0.8580      1.5800

```

	AREA	QPEAK	TPEAK	R. V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0006)	22.210	5.391	1.40	44.77
OUTFLOW: ID= 1 (0004)	22.210	0.399	2.35	44.71

PEAK FLOW REDUCTION [Qout/Qi n](%)= 7.40

TIME SHIFT OF PEAK FLOW (mi n)= 57.00

MAXIMUM STORAGE USED (ha. m.)= 0.7485

```

V   V   I   SSSSS   U   U   A   L
V   V   I   SS      U   U   A A  L
V   V   I   SS      U   U   AAAAA L

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(v 6.2.2006)

V V I SS U U A A L
 W W I SSSSS UUUUU A A LLLLL

000 TTTT TTTT H H Y Y M M 000 TM
 0 0 T T H H Y Y MM MM 0 0
 0 0 T T H H Y M M 0 0
 000 T T H H Y M M 000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\vojn.dat

Output filename:

C:\Users\dsredojevic\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
 7481a96-b45c-4563-9e30-1166dbf638d0\

Summary filename:

C:\Users\dsredojevic\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\b
 7481a96-b45c-4563-9e30-1166dbf638d0\

DATE: 11/18/2021

TIME: 10:54:40

USER:

COMMENTS: _____

 ** SIMULATION : 25mm Storm **

 | CHICAGO STORM |
Ptotal = 25.05 mm

IDF curve parameters: A= 538.850
 B= 6.331
 C= 0.809
 used in: INTENSITY = A / (t + B)^C
 Duration of storm = 4.00 hrs
 Storm time step = 5.00 min
 Time to peak ratio = 0.33

TIME RAIN | TIME RAIN |' TIME RAIN | TIME RAIN

hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	1.42	1.08	6.93	2.08	4.25	3.08	1.92
0.17	1.51	1.17	10.96	2.17	3.84	3.17	1.84
0.25	1.61	1.25	25.75	2.25	3.51	3.25	1.77
0.33	1.74	1.33	75.61	2.33	3.23	3.33	1.71
0.42	1.88	1.42	33.15	2.42	2.99	3.42	1.64
0.50	2.06	1.50	18.38	2.50	2.79	3.50	1.59
0.58	2.27	1.58	12.51	2.58	2.62	3.58	1.53
0.67	2.54	1.67	9.43	2.67	2.47	3.67	1.49
0.75	2.89	1.75	7.56	2.75	2.33	3.75	1.44
0.83	3.36	1.83	6.32	2.83	2.21	3.83	1.40
0.92	4.04	1.92	5.43	2.92	2.11	3.92	1.36
1.00	5.09	2.00	4.76	3.00	2.01	4.00	1.32

CALIB			
NASHYD (0002)	Area (ha)=	1.50	Curve Number (CN)= 88.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res. (N)= 3.00
	U. H. Tp(hrs)=	0.12	

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.040 (i)
TIME TO PEAK (hrs)= 1.500
RUNOFF VOLUME (mm)= 7.251
TOTAL RAINFALL (mm)= 25.047
RUNOFF COEFFICIENT = 0.289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0001)	Area (ha)=	20.71	
ID= 1 DT= 3.0 min	Total Imp(%)=	85.00	Dir. Conn. (%)= 75.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	17.60	3.11
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.00	2.00
Length	(m)=	371.57	40.00
Mannings n	=	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr

0.050	1.42	1.050	6.93	2.050	4.25	3.05	1.92
0.100	1.45	1.100	8.27	2.100	4.11	3.10	1.90
0.150	1.51	1.150	10.96	2.150	3.84	3.15	1.84
0.200	1.58	1.200	20.82	2.200	3.62	3.20	1.80
0.250	1.61	1.250	25.75	2.250	3.51	3.25	1.77
0.300	1.74	1.300	75.61	2.300	3.23	3.30	1.71
0.350	1.78	1.350	61.45	2.350	3.15	3.35	1.68
0.400	1.88	1.400	33.15	2.400	2.99	3.40	1.64
0.450	2.00	1.450	23.30	2.450	2.86	3.45	1.61
0.500	2.06	1.500	18.38	2.500	2.79	3.50	1.59
0.550	2.27	1.550	12.51	2.550	2.62	3.55	1.53
0.600	2.36	1.600	11.48	2.600	2.57	3.60	1.52
0.650	2.54	1.650	9.43	2.650	2.47	3.65	1.49
0.700	2.77	1.700	8.19	2.700	2.38	3.70	1.46
0.750	2.89	1.750	7.56	2.750	2.33	3.75	1.44
0.800	3.36	1.800	6.32	2.800	2.21	3.80	1.40
0.850	3.59	1.850	6.02	2.850	2.18	3.85	1.38
0.900	4.04	1.900	5.43	2.900	2.11	3.90	1.36
0.950	4.74	1.950	4.99	2.950	2.04	3.95	1.33
1.000	5.09	2.000	4.76	3.000	2.01	4.00	1.32

Max. Eff. Inten. (mm/hr)= 56.74 *****
over (min) 6.00 12.00
Storage Coeff. (min)= 7.04 (ii) 11.36 (ii)
Unit Hyd. Tpeak (min)= 6.00 12.00
Unit Hyd. peak (cms)= 0.17 0.10

TOTALS

PEAK FLOW (cms)= 1.89 0.10 1.946 (iii)
TIME TO PEAK (hrs)= 1.40 1.55 1.40
RUNOFF VOLUME (mm)= 23.05 6.43 18.89
TOTAL RAINFALL (mm)= 25.05 25.05 25.05
RUNOFF COEFFICIENT = 0.92 0.26 0.75

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 74.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0006)				
1 + 2 = 3				

ID1= 1 (0001):	AREA	QPEAK	TPEAK	R. V.
	(ha)	(cms)	(hrs)	(mm)
+ ID2= 2 (0002):	20.71	1.946	1.40	18.89
	1.50	0.040	1.50	7.25
=====				
ID = 3 (0006):	22.21	1.981	1.40	18.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR( 0004) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----

```

OUTFLOW (cms)	STORAGE (ha. m.)	OUTFLOW (cms)	STORAGE (ha. m.)
0.0000	0.0000	0.6190	1.0474
0.0480	0.2326	0.6740	1.1492
0.0780	0.4844	0.8160	1.4686
0.4080	0.7558	0.8580	1.5800

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R. V. (mm)
INFLOW : ID= 2 (0006)	22.210	1.981	1.40	18.11
OUTFLOW: ID= 1 (0004)	22.210	0.061	4.05	18.05


```

PEAK FLOW REDUCTION [Qout/Qi n](%)= 3.10
TIME SHIFT OF PEAK FLOW (min)=159.00
MAXIMUM STORAGE USED (ha. m. )= 0.3445

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=====
=====
V   V   I   SSSSS U   U   A   L           (v 6.2.2006)
V   V   I   SS   U   U   A A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
VV      I   SSSSS UUUUU A   A   LLLLL

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000   TTTTT TTTTT H   H   Y   Y   M   M   000   TM
0   0   T     T   H   H   Y   Y   MM  MM  0   0
0   0   T     T   H   H   Y     M   M   0   0
000     T     T   H   H   Y     M   M   000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6.2\V02\voir n. dat

Output filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\543c73d1-c34d-4726-8f8a-4355dcd19201\

Summary filename:

C:\Users\dsredoj evi c\AppData\Local\Ci vi ca\XH5\551ceb7e-af91-4608-b756-d808521cc3ad\543c73d1-c34d-4726-8f8a-4355dcd19201\

DATE: 11/18/2021

TIME: 10:54:39

USER:

COMMENTS: _____

** SIMULATION : 25-year Storm **

| CHICAGO STORM | IDF curve parameters: A=2019.372
| Ptotal = 64.46 mm | B= 9.824
C= 0.875

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.08	2.78	1.08	18.53	2.08	10.41	3.08	4.00
0.17	2.99	1.17	31.05	2.17	9.22	3.17	3.81
0.25	3.24	1.25	74.37	2.25	8.27	3.25	3.63
0.33	3.54	1.33	190.82	2.33	7.48	3.33	3.47
0.42	3.90	1.42	95.08	2.42	6.83	3.42	3.32
0.50	4.34	1.50	53.76	2.50	6.28	3.50	3.18
0.58	4.89	1.58	35.88	2.58	5.81	3.58	3.06
0.67	5.60	1.67	26.31	2.67	5.41	3.67	2.94
0.75	6.54	1.75	20.49	2.75	5.05	3.75	2.83
0.83	7.86	1.83	16.63	2.83	4.74	3.83	2.74
0.92	9.80	1.92	13.93	2.92	4.47	3.92	2.64
1.00	12.91	2.00	11.93	3.00	4.22	4.00	2.56

| CALIB |
| NASHYD (0002) | Area (ha)= 1.50 Curve Number (CN)= 88.0
| ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res. (N)= 3.00

U. H. Tp(hrs)= 0.12

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.269 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 37.074
 TOTAL RAINFALL (mm)= 64.464
 RUNOFF COEFFICIENT = 0.575

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | STANDHYD (0001) | Area (ha)= 20.71
 | ID= 1 DT= 3.0 min | Total Imp(%)= 85.00 Dir. Conn. (%)= 75.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	17.60	3.11
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.00	2.00
Length	(m)=	371.57	40.00
Mannings n	=	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.050	2.78	1.050	18.53	2.050	10.41	3.05	4.00
0.100	2.85	1.100	22.71	2.100	10.02	3.10	3.94
0.150	2.99	1.150	31.05	2.150	9.22	3.15	3.81
0.200	3.16	1.200	59.93	2.200	8.58	3.20	3.69
0.250	3.24	1.250	74.37	2.250	8.27	3.25	3.63
0.300	3.54	1.300	190.82	2.300	7.48	3.30	3.47
0.350	3.66	1.350	158.90	2.350	7.26	3.35	3.42
0.400	3.90	1.400	95.08	2.400	6.83	3.40	3.32
0.450	4.19	1.450	67.53	2.450	6.46	3.45	3.23
0.500	4.34	1.500	53.76	2.500	6.28	3.50	3.18
0.550	4.89	1.550	35.88	2.550	5.81	3.55	3.06
0.600	5.13	1.600	32.69	2.600	5.68	3.60	3.02
0.650	5.60	1.650	26.31	2.650	5.41	3.65	2.94
0.700	6.23	1.700	22.43	2.700	5.17	3.70	2.87
0.750	6.54	1.750	20.49	2.750	5.05	3.75	2.83
0.800	7.86	1.800	16.63	2.800	4.74	3.80	2.74
0.850	8.51	1.850	15.73	2.850	4.65	3.85	2.70
0.900	9.80	1.900	13.93	2.900	4.47	3.90	2.64
0.950	11.87	1.950	12.60	2.950	4.31	3.95	2.59
1.000	12.91	2.000	11.93	3.000	4.22	4.00	2.56

Max. Eff. Inten. (mm/hr)= 174.86
 over (min) 6.00

9.00

Storage Coeff. (min)=	4.49 (ii)	7.46 (ii)	
Unit Hyd. Tpeak (min)=	6.00	9.00	
Unit Hyd. peak (cms)=	0.22	0.14	
			TOTALS
PEAK FLOW (cms)=	5.67	0.76	6.335 (iii)
TIME TO PEAK (hrs)=	1.40	1.45	1.40
RUNOFF VOLUME (mm)=	62.46	32.85	55.06
TOTAL RAINFALL (mm)=	64.46	64.46	64.46
RUNOFF COEFFICIENT =	0.97	0.51	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0006)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R. V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0001):	20.71	6.335	1.40	55.06
+ ID2= 2 (0002):	1.50	0.269	1.42	37.07
=====				
ID = 3 (0006):	22.21	6.588	1.40	53.84

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR(0004)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha. m.)	(cms)	(ha. m.)
	0.0000	0.0000	0.6190	1.0474
	0.0480	0.2326	0.6740	1.1492
	0.0780	0.4844	0.8160	1.4686
	0.4080	0.7558	0.8580	1.5800
	AREA	QPEAK	TPEAK	R. V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0006)	22.210	6.588	1.40	53.84
OUTFLOW: ID= 1 (0004)	22.210	0.505	2.30	53.78

PEAK FLOW REDUCTION [Qout/Qin] (%) = 7.67
TIME SHIFT OF PEAK FLOW (min) = 54.00
MAXIMUM STORAGE USED (ha. m.) = 0.8905

=====

V V I SSSSS U U A L (v 6. 2. 2006)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTT TTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0
000 T T H H Y M M 000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYM0 6. 2\V02\vo i n. dat

Output filename:

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aad263c-bddf-47e9-ba49-bdb3eabe07cc\

Summary filename:

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aad263c-bddf-47e9-ba49-bdb3eabe07cc\

DATE: 11/18/2021

TIME: 10: 54: 40

USER:

COMMENTS: _____

** SIMULATION : 2-year **

| CHI CAGO STORM |
Ptotal = 44. 94 mm

IDF curve parameters: A=1290. 000
B= 8. 500
C= 0. 860

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.05	1.08	12.57	2.08	7.21	3.08	2.90
0.17	2.20	1.17	20.86	2.17	6.42	3.17	2.77
0.25	2.38	1.25	50.59	2.25	5.78	3.25	2.64
0.33	2.58	1.33	137.56	2.33	5.26	3.33	2.53
0.42	2.83	1.42	65.09	2.42	4.82	3.42	2.43
0.50	3.13	1.50	36.14	2.50	4.45	3.50	2.33
0.58	3.51	1.58	24.07	2.58	4.14	3.58	2.25
0.67	3.99	1.67	17.71	2.67	3.86	3.67	2.17
0.75	4.63	1.75	13.86	2.75	3.62	3.75	2.09
0.83	5.51	1.83	11.32	2.83	3.41	3.83	2.02
0.92	6.81	1.92	9.54	2.92	3.22	3.92	1.96
1.00	8.86	2.00	8.22	3.00	3.05	4.00	1.89

CALIB			
NASHYD (0002)	Area (ha)=	1.50	Curve Number (CN)= 88.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res. (N)= 3.00
	U. H. Tp(hrs)=	0.12	

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.145 (i)
TIME TO PEAK (hrs)= 1.417
RUNOFF VOLUME (mm)= 21.105
TOTAL RAINFALL (mm)= 44.941
RUNOFF COEFFICIENT = 0.470

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD (0001)	Area (ha)=	20.71	
ID= 1 DT= 3.0 min	Total Imp(%)=	85.00	Dir. Conn. (%)= 75.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	17.60	3.11
Dep. Storage (mm)=	2.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	371.57	40.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.050	2.05	1.050	12.57	2.050	7.21	3.05	2.90
0.100	2.10	1.100	15.34	2.100	6.95	3.10	2.86
0.150	2.20	1.150	20.86	2.150	6.42	3.15	2.77
0.200	2.32	1.200	40.68	2.200	6.00	3.20	2.69
0.250	2.38	1.250	50.59	2.250	5.78	3.25	2.64
0.300	2.58	1.300	137.56	2.300	5.26	3.30	2.53
0.350	2.67	1.350	113.41	2.350	5.11	3.35	2.50
0.400	2.83	1.400	65.09	2.400	4.82	3.40	2.43
0.450	3.03	1.450	45.79	2.450	4.58	3.45	2.36
0.500	3.13	1.500	36.14	2.500	4.45	3.50	2.33
0.550	3.51	1.550	24.07	2.550	4.14	3.55	2.25
0.600	3.67	1.600	21.95	2.600	4.04	3.60	2.22
0.650	3.99	1.650	17.71	2.650	3.86	3.65	2.17
0.700	4.42	1.700	15.14	2.700	3.70	3.70	2.12
0.750	4.63	1.750	13.86	2.750	3.62	3.75	2.09
0.800	5.51	1.800	11.32	2.800	3.41	3.80	2.02
0.850	5.94	1.850	10.73	2.850	3.35	3.85	2.00
0.900	6.81	1.900	9.54	2.900	3.22	3.90	1.96
0.950	8.18	1.950	8.66	2.950	3.11	3.95	1.92
1.000	8.86	2.000	8.22	3.000	3.05	4.00	1.89

Max. Eff. Inten. (mm/hr)= 125.49 *****
over (min) 6.00 9.00
Storage Coeff. (min)= 5.13 (ii) 8.51 (ii)
Unit Hyd. Tpeak (min)= 6.00 9.00
Unit Hyd. peak (cms)= 0.21 0.13

TOTALS

PEAK FLOW (cms)= 3.89 0.39 4.220 (iii)
TIME TO PEAK (hrs)= 1.40 1.45 1.40
RUNOFF VOLUME (mm)= 42.94 18.42 36.81
TOTAL RAINFALL (mm)= 44.94 44.94 44.94
RUNOFF COEFFICIENT = 0.96 0.41 0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 74.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0006) |
1 + 2 = 3

AREA QPEAK TPEAK R. V.
(ha) (cms) (hrs) (mm)

ID1= 1 (0001):	20.71	4.220	1.40	36.81
+ ID2= 2 (0002):	1.50	0.145	1.42	21.10
=====				
ID = 3 (0006):	22.21	4.356	1.40	35.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR( 0004) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----

```

OVERFLOW IS OFF

OUTFLOW (cms)	STORAGE (ha. m.)	OUTFLOW (cms)	STORAGE (ha. m.)
0.0000	0.0000	0.6190	1.0474
0.0480	0.2326	0.6740	1.1492
0.0780	0.4844	0.8160	1.4686
0.4080	0.7558	0.8580	1.5800

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R. V. (mm)
INFLOW : ID= 2 (0006)	22.210	4.356	1.40	35.75
OUTFLOW: ID= 1 (0004)	22.210	0.250	2.60	35.69

PEAK FLOW REDUCTION [Qout/Qin] (%) = 5.73
 TIME SHIFT OF PEAK FLOW (min) = 72.00
 MAXIMUM STORAGE USED (ha. m.) = 0.6256

```

V   V   I   SSSSS U   U   A   L           (v 6.2.2006)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
VV    I   SSSSS UUUUU A   A  LLLLL

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000  TTTT  TTTT  H  H  Y  Y  M  M  000  TM
0 0  T    T    H  H  Y Y  MM MM 0 0
0 0  T    T    H  H  Y   M  M 0 0
000  T    T    H  H  Y   M  M 000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\vo1n.dat

Output filename:

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Summary filename:

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DATE: 11/18/2021

TIME: 10: 54: 39

USER:

COMMENTS: _____

** SIMULATION : 50-year Storm **

| CHICAGO STORM | IDF curve parameters: A=2270.665
| Ptotal = 72.05 mm | B= 9.984
C= 0.876

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	'	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	3.10	1.08	20.80		2.08	11.67	3.08	4.47
0.17	3.34	1.17	34.86		2.17	10.33	3.17	4.25
0.25	3.62	1.25	83.24		2.25	9.26	3.25	4.05
0.33	3.95	1.33	211.98		2.33	8.38	3.33	3.87
0.42	4.35	1.42	106.30		2.42	7.64	3.42	3.70
0.50	4.85	1.50	60.28		2.50	7.03	3.50	3.55
0.58	5.47	1.58	40.27		2.58	6.50	3.58	3.41
0.67	6.26	1.67	29.53		2.67	6.04	3.67	3.28
0.75	7.32	1.75	22.99		2.75	5.65	3.75	3.16
0.83	8.80	1.83	18.66		2.83	5.30	3.83	3.05
0.92	10.98	1.92	15.62		2.92	4.99	3.92	2.95
1.00	14.48	2.00	13.38		3.00	4.72	4.00	2.85

| CALIB |

NASHYD (0002)	Area (ha)= 1.50	Curve Number (CN)= 88.0
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res. (N)= 3.00
	U. H. Tp(hrs)= 0.12	

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.319 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 43.618
 TOTAL RAINFALL (mm)= 72.046
 RUNOFF COEFFICIENT = 0.605

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 20.71	
STANDHYD (0001)	Total Imp(%)= 85.00	Dir. Conn. (%)= 75.00
ID= 1 DT= 3.0 min		

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	17.60	3.11
Dep. Storage (mm)=	2.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	371.57	40.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.050	3.10	1.050	20.80	2.050	11.67	3.05	4.47
0.100	3.18	1.100	25.48	2.100	11.23	3.10	4.40
0.150	3.34	1.150	34.86	2.150	10.33	3.15	4.25
0.200	3.53	1.200	67.11	2.200	9.62	3.20	4.12
0.250	3.62	1.250	83.24	2.250	9.26	3.25	4.05
0.300	3.95	1.300	211.98	2.300	8.38	3.30	3.87
0.350	4.09	1.350	176.76	2.350	8.13	3.35	3.81
0.400	4.35	1.400	106.30	2.400	7.64	3.40	3.70
0.450	4.68	1.450	75.62	2.450	7.23	3.45	3.60
0.500	4.85	1.500	60.28	2.500	7.03	3.50	3.55
0.550	5.47	1.550	40.27	2.550	6.50	3.55	3.41
0.600	5.73	1.600	36.69	2.600	6.35	3.60	3.37
0.650	6.26	1.650	29.53	2.650	6.04	3.65	3.28
0.700	6.97	1.700	25.17	2.700	5.78	3.70	3.20
0.750	7.32	1.750	22.99	2.750	5.65	3.75	3.16
0.800	8.80	1.800	18.66	2.800	5.30	3.80	3.05
0.850	9.53	1.850	17.65	2.850	5.20	3.85	3.02
0.900	10.98	1.900	15.62	2.900	4.99	3.90	2.95

0.950	13.31		1.950	14.13		2.950	4.81		3.95	2.88
1.000	14.48		2.000	13.38		3.000	4.72		4.00	2.85

Max. Eff. Inten. (mm/hr)=	194.37	*****	
over (min)	6.00	9.00	
Storage Coeff. (min)=	4.30 (ii)	7.15 (ii)	
Unit Hyd. Tpeak (min)=	6.00	9.00	
Unit Hyd. peak (cms)=	0.23	0.14	
			TOTALS
PEAK FLOW (cms)=	6.37	0.93	7.185 (iii)
TIME TO PEAK (hrs)=	1.40	1.45	1.40
RUNOFF VOLUME (mm)=	70.05	38.89	62.26
TOTAL RAINFALL (mm)=	72.05	72.05	72.05
RUNOFF COEFFICIENT =	0.97	0.54	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0006)				
1 + 2 = 3				
ID1= 1 (0001):	20.71	7.185	1.40	62.26
+ ID2= 2 (0002):	1.50	0.319	1.42	43.62
=====				
ID = 3 (0006):	22.21	7.487	1.40	60.99

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR(0004)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha. m.)	(cms)	(ha. m.)
	0.0000	0.0000	0.6190	1.0474
	0.0480	0.2326	0.6740	1.1492
	0.0780	0.4844	0.8160	1.4686
	0.4080	0.7558	0.8580	1.5800
	AREA	QPEAK	TPEAK	R. V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0006)	22.210	7.487	1.40	60.99
OUTFLOW: ID= 1 (0004)	22.210	0.586	2.30	60.94

PEAK FLOW REDUCTION [Qout/Qin] (%)= 7.83

TIME SHIFT OF PEAK FLOW
MAXIMUM STORAGE USED

(min)= 54.00
(ha. m.)= 1.0020

V V I SSSSS U U A L (v 6. 2. 2006)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0
000 T T H H Y M M 000

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***** D E T A I L E D O U T P U T *****

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DATE: 11/18/2021

TIME: 10:54:39

USER:

COMMENTS: _____

** SIMULATION : 5-year Storm **

CHICAGO STORM
Ptotal = 46.69 mm

IDF curve parameters: A=1183.740
B= 7.641
C= 0.838

used in: INTENSITY = $A / (t + B)^C$

Duration of storm = 4.00 hrs
Storm time step = 5.00 min
Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.08	2.36	1.08	13.04	2.08	7.70	3.08	3.27
0.17	2.52	1.17	21.19	2.17	6.90	3.17	3.12
0.25	2.71	1.25	50.66	2.25	6.25	3.25	2.99
0.33	2.93	1.33	141.24	2.33	5.72	3.33	2.87
0.42	3.19	1.42	65.17	2.42	5.27	3.42	2.76
0.50	3.51	1.50	36.21	2.50	4.89	3.50	2.66
0.58	3.91	1.58	24.34	2.58	4.56	3.58	2.56
0.67	4.41	1.67	18.09	2.67	4.27	3.67	2.48
0.75	5.07	1.75	14.31	2.75	4.02	3.75	2.40
0.83	5.98	1.83	11.80	2.83	3.80	3.83	2.32
0.92	7.29	1.92	10.03	2.92	3.60	3.92	2.25
1.00	9.36	2.00	8.71	3.00	3.43	4.00	2.18

CALIB
NASHYD (0002)
ID= 1 DT= 5.0 min

Area (ha)= 1.50 Curve Number (CN)= 88.0
Ia (mm)= 5.00 # of Linear Res. (N)= 3.00
U. H. Tp(hrs)= 0.12

Unit Hyd Qpeak (cms)= 0.477

PEAK FLOW (cms)= 0.152 (i)
TIME TO PEAK (hrs)= 1.417
RUNOFF VOLUME (mm)= 22.470
TOTAL RAINFALL (mm)= 46.694
RUNOFF COEFFICIENT = 0.481

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
STANDHYD (0001)
ID= 1 DT= 3.0 min

Area (ha)= 20.71
Total Imp(%)= 85.00 Dir. Conn. (%)= 75.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	17.60	3.11
Dep. Storage (mm)=	2.00	5.00

Average Slope (%) = 1.00 2.00
 Length (m) = 371.57 40.00
 Mannings n = 0.013 0.250

NOTE: RAINFALL WAS TRANSFORMED TO 3.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.050	2.36	1.050	13.04	2.050	7.70	3.05	3.27
0.100	2.41	1.100	15.76	2.100	7.44	3.10	3.22
0.150	2.52	1.150	21.19	2.150	6.90	3.15	3.12
0.200	2.64	1.200	40.84	2.200	6.47	3.20	3.04
0.250	2.71	1.250	50.66	2.250	6.25	3.25	2.99
0.300	2.93	1.300	141.24	2.300	5.72	3.30	2.87
0.350	3.02	1.350	115.89	2.350	5.57	3.35	2.83
0.400	3.19	1.400	65.17	2.400	5.27	3.40	2.76
0.450	3.40	1.450	45.87	2.450	5.02	3.45	2.69
0.500	3.51	1.500	36.21	2.500	4.89	3.50	2.66
0.550	3.91	1.550	24.34	2.550	4.56	3.55	2.56
0.600	4.08	1.600	22.26	2.600	4.47	3.60	2.54
0.650	4.41	1.650	18.09	2.650	4.27	3.65	2.48
0.700	4.85	1.700	15.57	2.700	4.11	3.70	2.42
0.750	5.07	1.750	14.31	2.750	4.02	3.75	2.40
0.800	5.98	1.800	11.80	2.800	3.80	3.80	2.32
0.850	6.42	1.850	11.21	2.850	3.74	3.85	2.30
0.900	7.29	1.900	10.03	2.900	3.60	3.90	2.25
0.950	8.67	1.950	9.15	2.950	3.49	3.95	2.21
1.000	9.36	2.000	8.71	3.000	3.43	4.00	2.18

Max. Eff. Inten. (mm/hr) = 128.56 *****
 over (min) 6.00 9.00
 Storage Coeff. (min) = 5.08 (ii) 8.43 (ii)
 Unit Hyd. Tpeak (min) = 6.00 9.00
 Unit Hyd. peak (cms) = 0.21 0.13

TOTALS

PEAK FLOW (cms) = 3.98 0.41 4.324 (iii)
 TIME TO PEAK (hrs) = 1.40 1.45 1.40
 RUNOFF VOLUME (mm) = 44.69 19.63 38.43
 TOTAL RAINFALL (mm) = 46.69 46.69 46.69
 RUNOFF COEFFICIENT = 0.96 0.42 0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 74.0 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0006)				
1 + 2 = 3				
ID1= 1 (0001):	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R. V. (mm)
+ ID2= 2 (0002):	20. 71	4. 324	1. 40	38. 43
	1. 50	0. 152	1. 42	22. 47
ID = 3 (0006):	22. 21	4. 467	1. 40	37. 35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR(0004)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5. 0 mi n	OUTFLOW (cms)	STORAGE (ha. m.)	OUTFLOW (cms)	STORAGE (ha. m.)
	0. 0000	0. 0000	0. 6190	1. 0474
	0. 0480	0. 2326	0. 6740	1. 1492
	0. 0780	0. 4844	0. 8160	1. 4686
	0. 4080	0. 7558	0. 8580	1. 5800
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R. V. (mm)
INFLOW : ID= 2 (0006)	22. 210	4. 467	1. 40	37. 35
OUTFLOW: ID= 1 (0004)	22. 210	0. 271	2. 60	37. 29
PEAK FLOW REDUCTION [Qout/Qi n] (%)= 6. 06				
TIME SHIFT OF PEAK FLOW (mi n)= 72. 00				
MAXIMUM STORAGE USED (ha. m.)= 0. 6428				

Appendix F

Stage-Storage-Discharge Relationship and Drawdown Calculations

PROJECT- 49549-100 (Dorchester , ON)

Name: PRELIMINARY WET POND

Date : December, 2021

POND STORAGE AND DISCHARGE

Orifice #1(Plate)	
Orifice Invert Elevation	276.00m
Diameter of Orifice	225mm
Orifice Constant	0.63

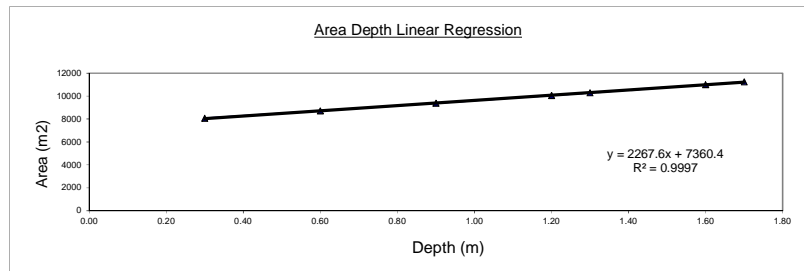
Orifice #2(Pipe)	
Orifice Invert Elevation	276.43m
Diameter of Orifice	575mm
Orifice Constant	0.63

Orifice #3(Pipe)	
Orifice Invert Elevation	0.00m
Diameter of Orifice	0mm
Orifice Constant	0.63

Weir(Trapezoidal)	
Weir Invert Elevation	196.50m
Bottom Length	10.00m
Side Slope (X:1)	13:1

Elevation (m)	Area (m ²)	Volume (m ³)	Cum.Storage Volume (m ³)	Depth over Orifice (m)	Depth to Center of Orifice (m)	Infiltration m3/sec	Flow (m ³ /sec)	Depth over Orifice (m)	Depth to Center of Orifice (m)	Flow (m ³ /sec)	Depth over Orifice (m)	Depth to Center of Orifice (m)	Flow (m ³ /sec)	Depth over Weir (m)	Weir Flow (m ³ /sec)	Total Flow m ³
PERMANENT POOL																
275	5475	0	0													
276	7440	6458	6458													
ACTIVE STORAGE																
276	7440	0	0	0.00	-0.11	0	-									
276.30	8068	2326	2326	0.30	0.19	0.000	0.048	-	-		-	-	-			0.0481
276.60	8715	2517	4844	0.60	0.49	0.000	0.078	0.17	-0.12	0.000						0.0775
276.90	9379	2714	7558	0.90	0.79	0.000	0.099	0.47	0.18	0.310						0.4082
277.20	10062	2916	10474	1.20	1.09	0.000	0.116	0.77	0.48	0.504						0.6193
277.30	10293	1018	11492	1.30	1.19	0.000	0.121	0.87	0.58	0.553						0.6742
277.60	11000	3194	14686	1.60	1.49	0.000	0.135	1.17	0.88	0.681						0.8164
277.70	11239	1112	15798	1.70	1.59	0.000	0.140	1.27	0.98	0.719						0.8584

VO2 Rating Table Input	
Q(m ³ /s)	Store(ha.m)
0	0
0.048	0.2326
0.078	0.4844
0.408	0.7558
0.619	1.0474
0.674	1.1492
0.816	1.4686
0.858	1.5798



EXTENDED DETENTION ONLY			
Intercept of Regression, C3			7371.00
Slope of Regression, C2			2252.700
Extended Det. Ponding Elevation (O1)			276.43 m
Depth over Orifice			0.430 m
Orifice Area			0.0398 m ²
Drawdown Time	=		92.244 sec
	=		25.62 hr

[Drawdown time Equation is Eqn 4.11 Stormwater Management Planning and Design Manual MOE, March 2003]